

ADDENDUM NO. 1

BID PACKAGE NUMBERS: All Bidders

PROJECT : ***Bay District Schools
Mosley Softball Field House***

This Addendum is a part of the Contract Documents.

This Addendum #01 consists of Items 1.1 through 1.6:

- Item 1.1 - JRA Addendum #1 dated April 10, 2026, which includes civil plan modifications.
- Item 1.2 - JRA Addendum #2 dated April 17, 2026, which includes clarifications for spray foam insulation on exterior CMU, Geotechnical Report and plumbing revisions.
- Item 1.3 - JRA Addendum #3 dated April 23, 2026, which includes clarifications for dryer exhaust, condensate drain routing and updates to the architectural site plan and floor plan.
- Item 1.4 - Prebid RFI Responses (#1- #18) are being included.
- Item 1.5 - Bidders Scope Checklist (**Please note that these are to be in your bid folders as part of your bid package**)
- Item 1.6 - Bid date remains Tuesday, May 12, 2026, at 2:00pm CDT at the Bay District Schools.

**End of Addendum #01
Dated This 23rd Day of April, 2026**





Addendum #1

Mosley Softball Fieldhouse

JRA Commission. 25871 CA/BC

Bay District Schools
1311 Balboa Avenue
Panama City, Florida 32401

JRA Architects, Inc.
2211 Navy Blvd- Suite 100
Panama City, Florida 32408

Date of Issue of addendum: **April 10, 2026**

The changes herewith form part of the Construction Documents and modify the original “Construction Documents” dated April 3, 2026.

This Addendum consists of **1** page(s), **0** attachment(s) and **2** revised plan sheet(s) attached and as referenced herein.

ITEM 1.1

Drawings:

Replace existing drawing sheets C1.1, C1.2, C1.3, C1.4, C1.5, C1.6, C1.7, C1.8, C1.9, and C1.10 with **Attached Revised Drawing Sheets C1.1, C1.2, C1.3, C1.4, C1.5, C1.5A, C1.6, C2.1, C2.2, C2.3, and C2.4.** (Note revised sheets contain an additive alternate)

END OF ADDENDUM #1

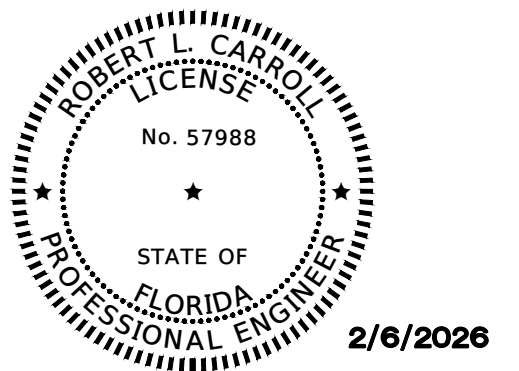
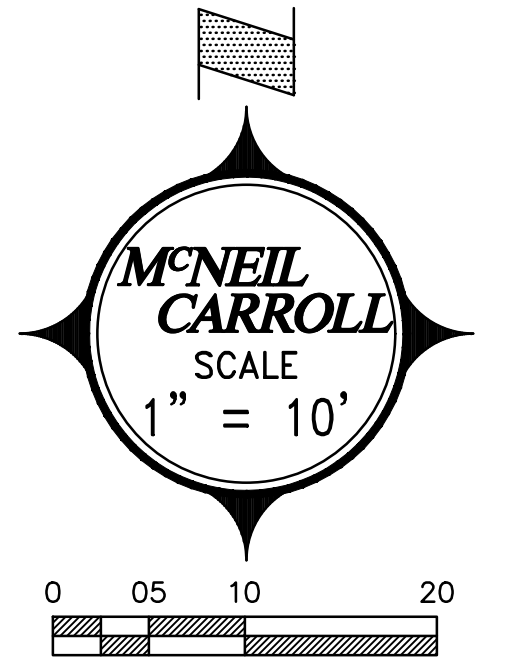


SITE DEMOLITION DRAWING NOTES:

1. SEE SYMBOL LEGEND ON THIS SHEET FOR SYMBOL INFORMATION AND REFERENCED DETAILS.
2. ALL DEMOLISHED MATERIALS (i.e., SIGNS, CONCRETE, ASPHALT, ETC...) TO BE REMOVED AND DISPOSED OF IN A LEGAL MANNER.
3. ALTHOUGH EVERY ATTEMPT TO LOCATE UNDERGROUND UTILITIES HAS BEEN MADE, THERE IS THE POSSIBILITY OF UNDERGROUND GAS, ELECTRICAL, WATER SEWER, ETC... THAT HAS NOT BEEN LOCATED. THE CONTRACTOR SHALL FIELD VERIFY THE LOCATION OF ALL UNDERGROUND UTILITIES PRIOR TO CONSTRUCTION.
4. THE DEVELOPER AND/OR CONTRACTOR IS RESPONSIBLE FOR FOLLOWING REQUIRED WASTE MANAGEMENT PRACTICES AS DEFINED IN THE LYNN HAVEN MUNICIPAL CODE SECTION 54-32 "BUILDING CONSTRUCTION WASTES", WHICH MAKES IT UNLAWFUL FOR ANY PERSON TO DUMP, LEAVE OR BURY ANY SOLID WASTE ON PUBLIC OR PRIVATE PROPERTY.
5. IT IS THE CONTRACTORS RESPONSIBILITY TO CALL SUNSHINE ONE AT 811 FOR UTILITY LOCATES PRIOR TO CONSTRUCTION.
6. REMOVE AND RELOCATE CLAY PILE PER BAY DISTRICT SCHOOL INSTRUCTIONS.

SYMBOL LEGEND

- N1 (SEE NOTE i.e., #1 - SEE NOTES ON THIS SHEET)
- RM (REMOVE EXISTING MATERIALS)



Robert L. Carroll, P.E.
PROFESSIONAL ENGINEER
FL LIC # 57988

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| CONSTRUCTION DOCUMENTS | MAY | SLB | 4/3/26 |

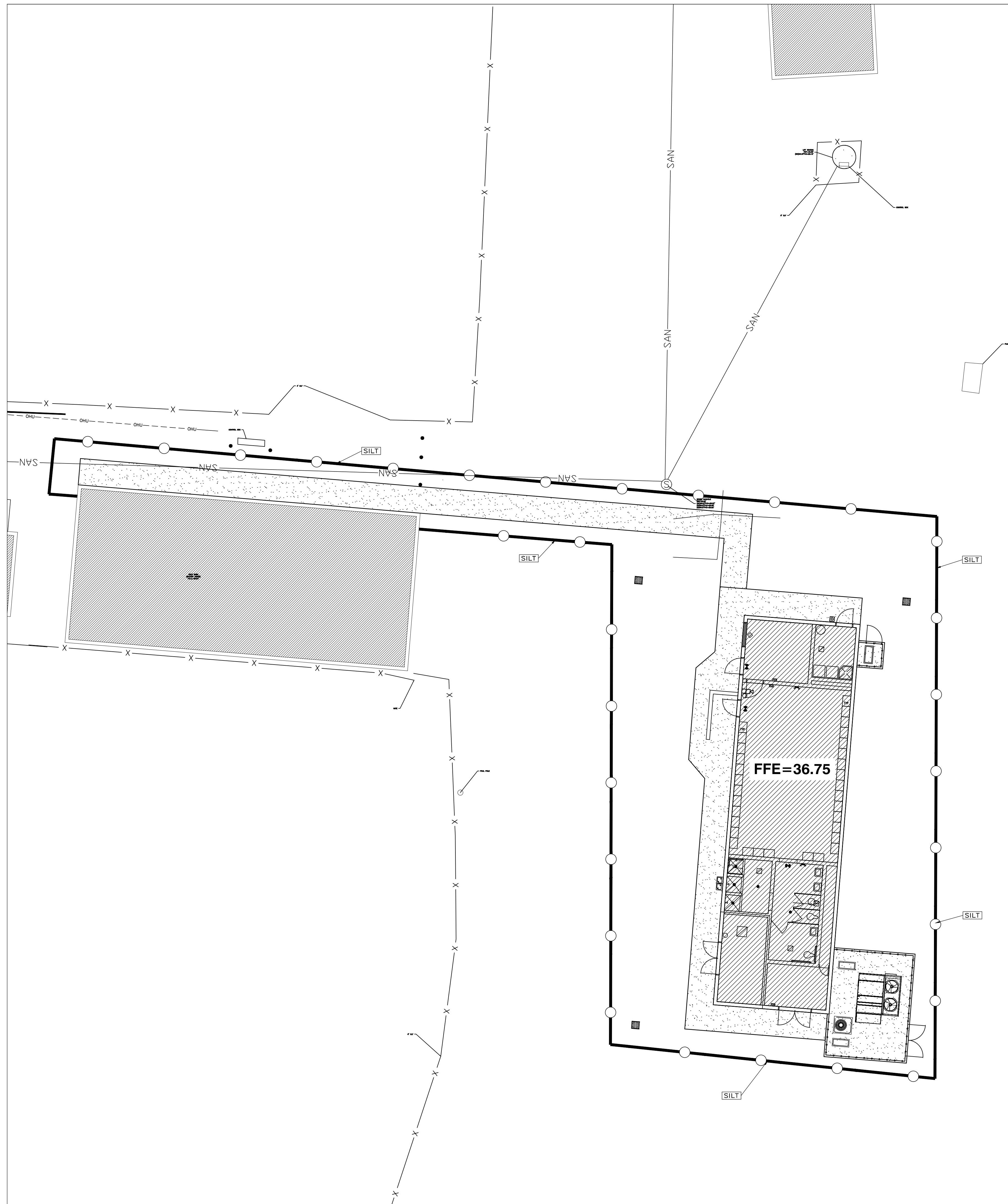
JRA ARCHITECTS 2211 NAVY BLVD., STE 100
PANAMA CITY BEACH, FL
PHONE: (850) 236-9832
Commission Number: 25871

CONSULTANTS:

PROJECT:
BAY DISTRICT SCHOOLS
NEW SOFTBALL FIELD
HOUSE
MOSLEY HIGH SCHOOL
LYNN HAVEN, FLORIDA

SITE DEMOLITION CONTROL PLAN

SHEET NUMBER: **C1.1**



SITE EROSION CONTROL DRAWING NOTES:

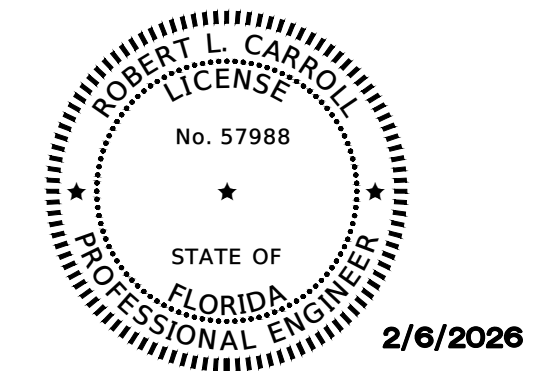
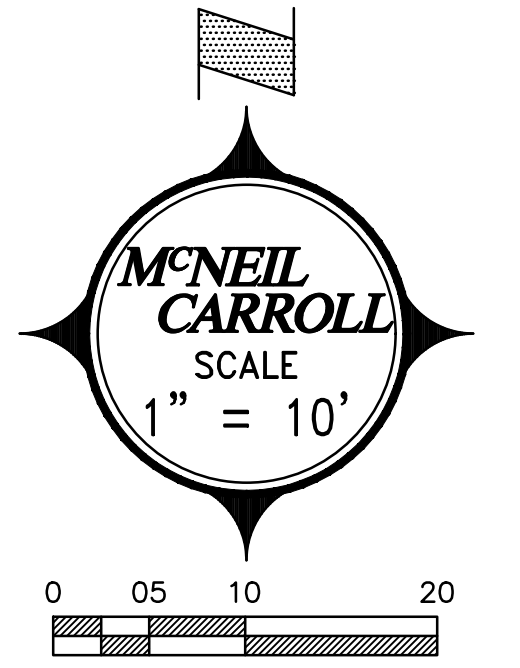
1. EROSION CONTROL SHALL BE MAINTAINED FOR THE DURATION FOR THE PROJECT.
2. ALL CONSTRUCTION OUTSIDE OF PROPERTY LINES IS SHOWN IN DETAIL ON PERMIT DRAWINGS. (SEE GENERAL NOTES.)
3. SEE SYMBOL LEGEND ON THIS SHEET FOR SYMBOL INFORMATION AND REFERENCED DETAILS.
4. SEE SECTIONS IN CONSTRUCTION DETAILS.
5. SILT FENCE TO BE INSTALLED AT PERIMETER OF SITE DURING CONSTRUCTION. EROSION CONTROL MEASURES WILL BE UTILIZED THROUGHOUT THE CONSTRUCTION PHASE OF THIS PROJECT TO RESTRICT ANY TURBID RUNOFF FROM LEAVING THE CONSTRUCTION SITE.
6. CONTROL OF SEDIMENT-LADEN RUNOFF SHALL BE PROVIDED WITH HAY BALES AND/OR GEOTECH STYLE FABRICS. ALL CONTROL MEASURES SHALL BE PROPERLY LOCATED AND CONSTRUCTED TO PREVENT SEDIMENT TRANSPORT. THE MEANS FOR RETAINING THE SEDIMENTS WILL BE MAINTAINED BY THE CONTRACTOR UNTIL PERMANENT IMPROVEMENTS ARE COMPLETE.
7. THE CONTRACTOR IS RESPONSIBLE FOR TREATING ALL ONSITE STORMWATER DRAINAGE AS REQUIRED TO MEET THE CRITERIA OF 62-3 FLORIDA ADMINISTRATIVE CODE, F.A.C. PRIOR TO DISCHARGE.
8. ALL CATCH BASINS, INLETS AND ACCESSSES TO UNDERGROUND STORMWATER SYSTEMS SHALL BE PROTECTED IN ACCORDANCE WITH THE ATTACHED DETAILS.
9. THE CONTRACTOR IS RESPONSIBLE FOR COMPLYING WITH THE TERMS AND CONDITIONS OF ANY STORMWATER PERMITS THAT MAY APPLY (FLORIDA DEPARTMENT OF ENVIRONMENTAL PROTECTION, FLORIDA DEPARTMENT OF TRANSPORTATION, CITY OF LYNN HAVEN, WATER MANAGEMENT DISTRICT, ETC.).
10. CONSTRUCTION DRIVES SHALL SLOPE AWAY FROM THE ROADWAY AT A MINIMUM SLOPE OF 2.00% TO DISTANCE OF NOT LESS THAN 15 FEET FROM THE EDGE OF PAVEMENT. THE MAXIMUM WIDTH OF THE DRIVE SHALL BE 30 FEET WITH #57 GRAVEL SURFACE 6 INCHES THICK. SIGNS SHALL BE PLACED (IN ACCORDANCE WITH CITY AND STATE REQUIREMENTS) TO WARN APPROACHING DRIVERS AND PEDESTRIANS.
11. THE DEVELOPER AND/OR CONTRACTOR IS RESPONSIBLE FOR FOLLOWING REQUIRED WASTE MANAGEMENT PRACTICES AS DEFINED IN THE LYNN HAVEN MUNICIPAL CODE SECTION 54-32 "BUILDING CONSTRUCTION WASTE", WHICH MAKES IT UNLAWFUL FOR ANY PERSON TO DUMP, LEAVE OR BURY ANY SOLID WASTE ON PUBLIC OR PRIVATE PROPERTY.
12. THE DEVELOPER AND/OR CONTRACTOR IS RESPONSIBLE FOR OBTAINING COVERAGE UNDER THE FDEP GENERIC PERMIT FOR STORMWATER DISCHARGE FROM LARGE AND SMALL CONSTRUCTION ACTIVITIES PRIOR TO START OF CONSTRUCTION OR ANY DISTURBANCE OF LAND GREATER THAN 1 ACRE. THE DEVELOPER/CONTRACTOR WILL FORWARD A COPY OF THE PERMIT AND WILL PROVIDE 48 HOUR NOTIFICATION TO THE APPROPRIATE AGENCIES PRIOR TO COMMENCEMENT OF CONSTRUCTION. ALL REQUIRED ELEMENTS OF THE SWPP MUST BE IN PLACE PRIOR TO COMMENCEMENT OF CONSTRUCTION. FAILURE TO COMPLY COULD RESULT IN CODE ENFORCEMENT ACTION AND FINES.
13. QUALIFIED PERSONNEL SHALL INSPECT THE FOLLOWING ITEMS AT LEAST ONCE EVERY SEVEN (7) CALENDAR DAYS AND/OR WITHIN 24 HOURS OF THE END OF A STORM EVENT (RAINFALL) THAT IS A 1/2 INCH OR GREATER.
 - A. POINTS OF DISCHARGE TO WATERS OF THE UNITED STATES.
 - B. POINTS OF DISCHARGE TO MUNICIPAL SEPARATE STORM WATER SYSTEMS.
 - C. DISTURBED AREAS OF THE SITE THAT HAVE NOT BEEN FINALLY STABILIZED.
 - D. AREAS USED FOR STORAGE OF MATERIALS THAT ARE EXPOSED TO PRECIPITATION.
 - E. STRUCTURAL CONTROLS.
 - F. LOCATIONS WHERE VEHICLES ENTER OR EXIT THE SITE.
14. THE CONTRACTOR SHALL INITIATE REPAIRS WITHIN 24 HOURS OF INSPECTION THAT INDICATE ITEMS ARE NOT IN GOOD WORKING ORDER. TO COMPLY, THE CONTRACTOR SHALL INSTALL AND MAINTAIN RAIN GAGES AND DAILY RAINFALL RECORDS. WHERE SITES HAVE BEEN PERMANENTLY STABILIZED, INSPECTIONS SHALL BE CONDUCTED AT LEAST ONCE EVERY MONTH. THE CONTRACTOR SHALL ALSO INSPECT AND CERTIFY THAT CONTROLS INSTALLED IN THE FIELD AGREE WITH THE LATEST STORMWATER POLLUTION PREVENTION PLAN.
15. IF INSPECTIONS INDICATE THAT THE INSTALLED STABILIZATION AND STRUCTURAL PRACTICES ARE NOT SUFFICIENT TO MINIMIZE EROSION, RETAIN SEDIMENT, AND PREVENT DISCHARGING POLLUTANTS, THE CONTRACTOR SHALL PROVIDE ADDITIONAL MEASURES, WHERE SITES HAVE BEEN PERMANENTLY STABILIZED, INSPECTIONS SHALL BE CONDUCTED AT LEAST ONCE EVERY MONTH, AS NEEDED.
16. RECORDS OF THE INSPECTIONS AND THE CONSTRUCTION PERMIT MUST BE MAINTAINED AT THE CONSTRUCTION SITE AND BE READILY AVAILABLE FOR INSPECTION.
17. ALL STORMWATER MANAGEMENT FACILITIES AND EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO COMMENCEMENT OF ANY CONSTRUCTION, DEMOLITION OR OTHER DISTURBANCE TO THE SUBJECT SITE.

CONSTRUCTION SEQUENCE AND BMP'S NWFWD

18. THE INITIAL PART OF THE CONSTRUCTION PROCESS SHALL BE THE INSTALLATION OF SILT FENCE AROUND THE PERIMETER OF THE AREA THAT IS TO BE DISTURBED TO ENSURE NO TURBID RUNOFF LEAVES THE CONSTRUCTION SITE. THE SILT FENCE SHALL BE INSTALLED PER THE CONSTRUCTION DETAILS. IF THERE IS A POSSIBILITY OF RUNOFF TO A WATER BODY, TURBIDITY CURTAIN SHALL BE INSTALLED PER THE CONSTRUCTION DETAILS. THE SECOND STEP SHALL BE THE INSTALLATION OF THE CONSTRUCTION ENTRANCE AND DEMOLITION OF ANY EXISTING IMPROVEMENTS AS NEEDED (SEE DEMOLITION PLAN). THE THIRD STEP SHALL BE TO CLEAR AND GRUB AREAS WHERE IMPROVEMENTS ARE TO BE INSTALLED. AS FILL IS BROUGHT INTO THE SITE, THE STORMWATER BASIN SHOULD BE CREATED TO CAPTURE ANY OVERLAND FLOW AND ACT AS A SEDIMENT TRAP. IT IS RECOMMENDED THAT THE BASIN BE CONSTRUCTED APPROXIMATELY 1/2' HIGHER THAN DESIGN AT THIS POINT TO ENSURE ALL SILTS AND FINES ARE REMOVED AT THE TIME OF FINAL GRADING OF THE STORMWATER BASIN.
19. TYPICALLY, THE SANITARY SEWER, STORM SEWER, AND WATER MAINS ARE INSTALLED RESPECTIVELY. UPON INSTALLATION OF THE STORM SEWER, HAY BALES AND FILTER FABRICS SHALL BE USED AT ALL INLET OPENINGS PER THE CONSTRUCTION DETAILS TO KEEP THE SYSTEM FREE OF SEDIMENTS DURING THE CONSTRUCTION PHASE. DEPENDING ON SITE CONDITIONS AND SIZE, SEDIMENT TRAPS SHALL BE UTILIZED TO PREVENT TURBID RUNOFF FROM LEAVING THE SITE (SEE EROSION CONTROL PLAN).
20. SITE STABILIZATION SHALL BE PROVIDED AS SOON AS THE GRADING WILL ALLOW IN ORDER TO STOP EROSION AND REDUCE TURBID RUNOFF. SEEDING, SODDING, OR HYDROSEEDING SHALL BE USED WHEN FINAL GRADES ARE ESTABLISHED.
21. EROSION CONTROL MEASURES SHALL BE UTILIZED THROUGHOUT THE CONSTRUCTION PHASE OF THIS PROJECT AND BE MANAGED IN ACCORDANCE WITH THE STATE NPDES PROGRAM.
22. THE DESIGN OF THE STORMWATER MANAGEMENT SYSTEM FOR THIS PROJECT COMPLIES WITH THE REQUIREMENTS OF THE FLORIDA DEPARTMENT OF ENVIRONMENTAL PROTECTION AND THE NORTHWEST FLORIDA WATER MANAGEMENT DISTRICT.
23. THE ENGINEER OF RECORD IS RESPONSIBLE FOR MONITORING CONSTRUCTION OF THE STORMWATER MANAGEMENT FACILITY AND SUBMITTING TO THE APPROPRIATE AGENCY NOTICE OF COMMENCEMENT AND AS-BUILT CERTIFICATIONS FOR THE PROJECT WHEN COMPLETED.

SYMBOL LEGEND

- (STORMWATER SURFACE FLOW)
- [ISB] (INLET SEDIMENT BARRIER - SEE CONSTRUCTION DETAILS)
- [SILT] (SILT FENCE - SEE CONSTRUCTION DETAILS)
- [PVI] (24" WIDE x 50" DEEP FDOT #1 OR #2 GRAVEL CONSTRUCTION ENTRANCE 6" THICK)



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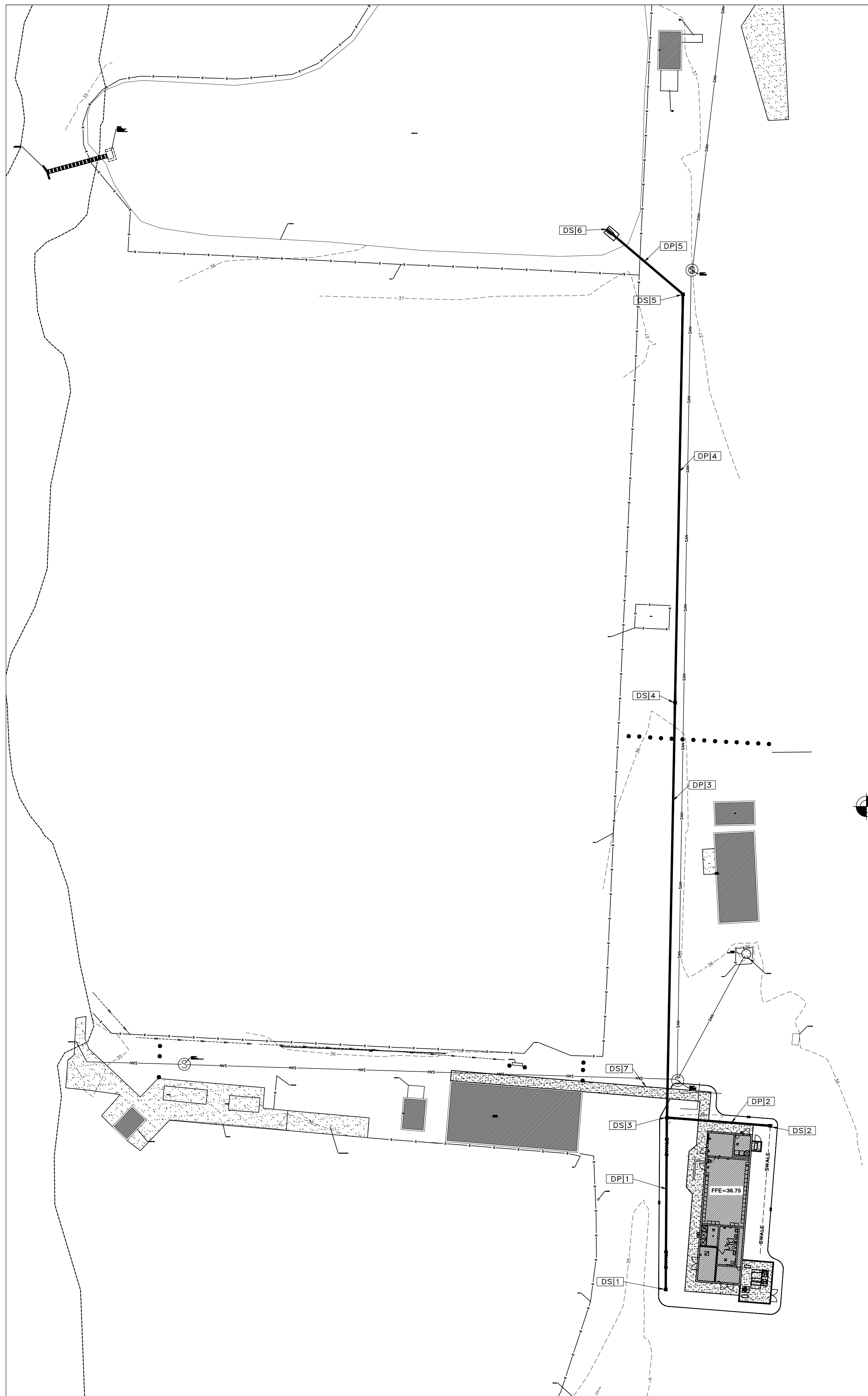
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CONSULTANTS:

PROJECT:
 BAY DISTRICT SCHOOLS
 NEW SOFTBALL FIELD
 HOUSE
 MOSLEY HIGH SCHOOL
 LYNN HAVEN, FLORIDA

SITE EROSION CONTROL PLAN

SHEET NUMBER: **C1.2**



SITE GRADING AND DRAINAGE DRAWING NOTES:

1. SEE SYMBOL LEGEND ON THIS SHEET FOR SYMBOL INFORMATION AND REFERENCED DETAILS.
2. ALL DEMOLISHED MATERIALS (i.e., SIGNS, CONCRETE, ASPHALT, ETC...) TO BE REMOVED AND DISPOSED OF IN A LEGAL MANNER. ALL EXISTING MONITORING WELLS ARE NOT TO BE REMOVED. WELLS IN PAVEMENT SHALL HAVE A MANHOLE LID INSTALLED.
3. SEE SECTIONS IN CONSTRUCTION DETAILS.
4. ALL DRAINAGE PIPES TO BE DEDICATED TO THE CITY OF LYNN HAVEN SHALL BE VIDEO RECORDED AND PLACED ON A DIGITAL MEDIA (NO TAPES). VIDEO MUST BE REVIEWED AND APPROVED BY THE CITY.
5. PROPOSED FINISHED FLOORS SHALL BE 1 FOOT (MIN.) ABOVE ROADWAY CENTERLINE.
6. CONTRACTOR SHALL PROVIDE McNEIL CARROLL ENGINEERING, INC. FIVE (5) SETS AND ONE (1) DIGITAL COPY (AUTOCAD FORMAT) OF AS-BUILT DRAWINGS OF THE COMPLETED PROJECT. DRAWINGS SHALL BE PREPARED AND SIGNED & SEALED BY A FLORIDA REGISTERED SURVEYOR.
7. IT IS THE CONTRACTORS RESPONSIBILITY TO CALL SUNSHINE ONE AT 811 FOR UTILITY LOCATES PRIOR TO CONSTRUCTION.
8. ALL DISTURBED AREAS SHALL BE RESTORED TO ORIGINAL CONDITION AND SODDED PER FDOT INDEX 570-010.

SYMBOL LEGEND

- 34.60 (EXISTING SPOT ELEVATION)
- 36- (EXISTING CONTOUR)
- +12.50 (PROPOSED FINISHED GRADE)
- (STORMWATER SURFACE FLOW)
- CSW (CONCRETE SIDEWALK - SEE CONSTRUCTION DETAILS)
- DP16 (SEE DRAINAGE PIPE SCHEDULE THIS SHEET i.e.#16)
- DS12 (SEE DRAINAGE STRUCTURE SCHEDULE THIS SHEET i.e.#12)
- FC (CHAINLINK FENCE - SEE CONSTRUCTION DETAILS)
- N11 (SEE NOTE i.e.#1 - SEE NOTES THIS SHEET)
- SA (SEE ARCHITECTURAL PLANS)

| DRAINAGE PIPE SCHEDULE | | | | |
|------------------------|------|-----|------|-------|
| NO. | SIZE | LF | TYPE | SLOPE |
| DP1 | 12" | 83 | ADS | 0.50% |
| DP2 | 12" | 50 | ADS | 0.80% |
| DP3 | 12" | 202 | ADS | 0.50% |
| DP4 | 12" | 199 | ADS | 0.50% |
| DP5 | 12" | 49 | ADS | 0.50% |

ALL ADS PIPE SHALL BE AS SHOWN OR EQUAL
 ALL PERFORATED PIPE SHALL HAVE A GRAVEL PACK
 ALL ADS PIPE SHALL BE RATED N-12
 SEE CONSTRUCTION DETAILS.

| DRAINAGE STRUCTURE SCHEDULE | | | | |
|-----------------------------|---|---------------------|-------------|-------------|
| NO. | TYPE STRUCTURE | TOP OF GRATE | PIPE INVERT | SLOT INVERT |
| DS1 | 15" ADS INLET | EL. 35.50 | EL. 33.50 | EL. |
| DS2 | 15" ADS INLET | EL. 35.50 | EL. 33.50 | EL. |
| DS3 | 15" ADS INLET | EL. 35.50 | EL. 33.50 | EL. |
| DS4 | 15" ADS INLET WITH SOLID LID | EL. 36.20 | EL. 32.08 | EL. |
| DS5 | 15" ADS INLET WITH SOLID LID | EL. 37.35 | EL. 31.88 | EL. |
| DS6 | 15" CONCRETE WITHEDED END | EL. | EL. 30.83 | EL. |
| DS7 | 5 LF TRENCH DRAIN EVERGRATE T-14C CONTINUUM | EL. N 35.65 S 35.63 | EL. | EL. |

SEE CONSTRUCTION DETAILS.
 2' SLUMP UNLESS OTHERWISE NOTED.

STORMWATER OPERATION AND MAINTENANCE SCHEDULE

AFTER EACH RAINFALL EVENT

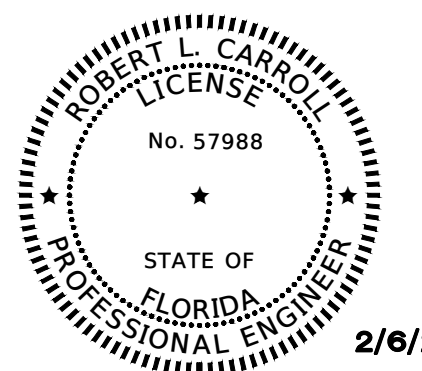
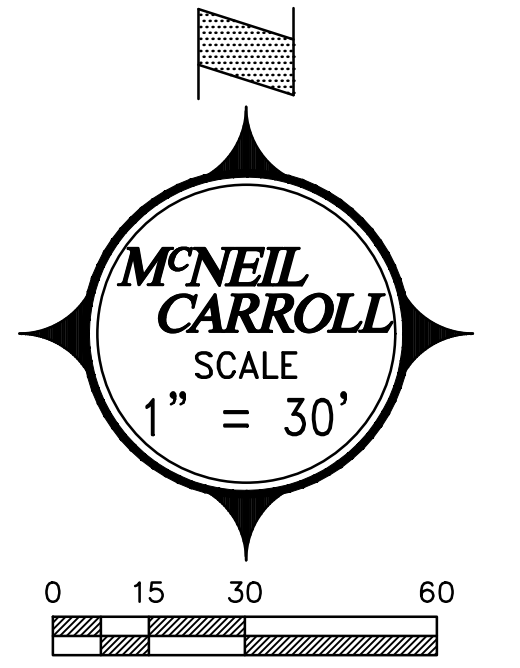
1. PAVEMENT AREAS: CLEAN/SWEEP DEBRIS AND DIRT FROM PAVEMENT AREAS.
2. SEDIMENTS IN RETENTION/DETENTION AREAS: REMOVE IMMEDIATELY.
3. DEBRIS IN RETENTION/DETENTION AREAS: ALL DEBRIS AND FOREIGN MATERIAL SHALL BE REMOVED IMMEDIATELY.
4. YARD INLETS, CATCH BASINS, ETC.: ALL DEBRIS AND FOREIGN MATERIALS SHALL BE REMOVED IMMEDIATELY.

PERIODIC POND/SYSTEM MAINTENANCE

1. CLEANING/ SWEEPING OF PAVEMENT AREAS SHALL BE ACCOMPLISHED WEEKLY OR AS REQUIRED.
2. INSPECT POND AT LEAST TWICE A MONTH FOR ACCUMULATION OF TRASH AND DEBRIS AND REMOVE UPON DISCOVERY. UPON ANY DISCOVERY OF TRASH AND DEBRIS ACCUMULATION, REMOVE AT ONCE.
3. MOWING AND LANDSCAPING MAINTENANCE SHOULD BE DONE ON A MONTHLY BASIS DURING THE ACTIVE GROWING SEASON FOR THIS AREA. INSPECT AND MAINTAIN AS REQUIRED DURING THE GROWING SEASON.
4. WEEDS OR UNDESIRABLE GROWTH SHALL BE REMOVED UPON DISCOVERY.
5. ALL STORMWATER STRUCTURES AND PIPES BASINS SHALL BE FLUSHED AS NECESSARY.
6. THE OWNER SHALL RE-GRADE AND RE-STABILIZE SWALE/ RETENTION/ DETENTION AREAS AS REQUIRED TO MAINTAIN THE APPROVED DESIGN, CROSS-SECTIONS, GRADES, ETC.
7. REMOVE SEDIMENT FROM POND WHEN ACCUMULATION REACHES TWO (2) INCHES. MEASUREMENTS FOR ACCUMULATION SHALL BE PERFORMED EVERY SIX MONTHS AND AFTER EACH MAJOR STORM EVENT.

INSPECTIONS

1. A MAINTENANCE INSPECTION SHALL BE PERFORMED AT MINIMUM EVERY FIFTH YEAR BY A REGISTERED PROFESSIONAL. THE INSPECTOR SHALL BE WORKING UNDER THE CHARGE OF A LICENSED PROFESSIONAL ENGINEER.
2. THE MAINTENANCE INSPECTION SHALL BE DOCUMENTED ON THE FDEP AND/OR NWFWM STANDARD INSPECTION FORM 62-330-311(1).
3. THE INSPECTION SHALL BE SIGNED, SEALED AND DATED BY THE REGISTERED PROFESSIONAL AND SUBMITTED TO EITHER THE FDEP OR NWFWM WITHIN 30 DAYS OF THE INSPECTION.
4. THE INSPECTION MUST BE CONDUCTED USING THE PLANS, CALCULATIONS AND SPECIFICATIONS APPROVED BY THE FDEP AND/OR NWFWM.
5. THERE MUST BE AN INSPECTION COMPLETED BY A REGISTERED PROFESSIONAL ONE YEAR AFTER THE CONVERSION INTO OPERATION.



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BAY DISTRICT SCHOOLS
 NEW SOFTBALL FIELD
 HOUSE
 MOSLEY HIGH SCHOOL
 LYNN HAVEN, FLORIDA

SHEET TITLE:

**SITE DRAINAGE
 PLAN**

SHEET NUMBER:

C1.5

SITE DRAINAGE

ALL OFF-SITE AND ON-SITE WORK INCLUDED CONSISTS OF BUT IS NOT LIMITED TO THE FOLLOWING:
EXCAVATION, BEDDING, FILTER MATERIAL AND BACKFILL FOR ALL STORM SEWER, SUBSURFACE DRAINS AND DRAINAGE STRUCTURES.

COMPLETE INSTALLATION OF ALL STORM SEWER, SUBSURFACE DRAINS, CATCH BASINS, JUNCTION BOXES, MANHOLES, ETC., INCLUDING ALL RELATED FITTINGS, JOINTS COVERS, GRATES, FRAMES, RUNGS, ETC.

ANY WORK WITHIN STREET OR HIGHWAY RIGHT-OF-WAY SHALL BE DONE IN ACCORDANCE WITH THE REQUIREMENTS OF THE GOVERNMENTAL AGENCIES HAVING JURISDICTION AND SHALL NOT BEGIN UNTIL ALL OF THESE GOVERNING AUTHORITIES HAVE BEEN NOTIFIED.

POLYVINYL CHLORIDE (PVC), FOR PIPE UP TO AND INCLUDING TEN INCHES (10") IN DIAMETER, SHALL CONFORM TO ASTM D3034 SDR 35 WITH ELASTOMERIC GASKET JOINTS CONFORMING TO ASTM D3212.

REINFORCED CONCRETE PIPE, FOR PIPE TWELVE INCHES (12") IN DIAMETER AND UP, SHALL CONFORM TO ASTM C-76, CLASS IV OR AASHTO M-170 WITH BELL AND SPIGOT OR TONGUE AND GROOVE COMPRESSION JOINT CONFORMING TO ASTM C-443.

MANHOLES, CATCH BASINS, ETC. SHALL BE SIZES AND TYPE INDICATED ON THE DRAWINGS AND SHALL BE CONSTRUCTED OF THE FOLLOWING:

REINFORCED PRECAST CONCRETE MANHOLE SECTION INCLUDING CONCENTRIC OR ECCENTRIC CONES AND GRADE RINGS SHALL BE 4000 PSI CONCRETE AND CONFORM TO ASTM C478 OR AASHTO M-199. SECTIONS SHALL BE COMPLETE WITH 3/4" ROUND CAST IN PLACE WROUGHT IRON STEPS.

BRICK SHALL BE SOUND, HARD BURNED THROUGHOUT AND OF UNIFORM SIZE AND QUALITY AND SHALL BE IN ACCORDANCE WITH ASTM C-32, GRADE MS OR MM.

CONCRETE MASONRY SHALL BE SOLID PRECAST SEGMENTAL CONCRETE MASONRY UNITS CONFORMING TO ASTM C-119.

IRON CASTINGS SHALL CONFORM TO ASTM A-48, CLASS 30, BEARING SURFACES BETWEEN CAST IRON FRAMES, COVERS AND GRATES SHALL BE MACHINED, FITTED TOGETHER AND MATCH MARKED TO PREVENT ROCKING.

SYSTEM IDENTIFYING LETTER 2" HIGH SHALL BE STAMPED OR CAST INTO ALL COVERS SO THAT THE MAY BE PLAINLY VISIBLE.

CASTINGS SHALL BE MANUFACTURED BY EAST JORDAN IRON WORKS, INC. NEEHAH FOUNDRY COMPANY, VULCAN FOUNDRY COMPANY OR EQUAL.

MANHOLE STEPS FOR BRICK OR CONCRETE MASONRY STRUCTURES SHALL BE CAST IRON ASPHALT COATED, NEEHAH FOUNDRY COMPANY "R-1980-E" OR EQUAL.

CONCRETE AND MASONRY MATERIALS FOR CONSTRUCTION OF STORM DRAINAGE STRUCTURES SHALL CONSIST OF THE FOLLOWING:

PORTLAND CEMENT SHALL BE STANDARD BRAND OF PORTLAND CEMENT CONFORMING TO ASTM C-150, TYPE I OR II.

FINE AND COARSE AGGREGATES FOR CONCRETE SHALL BE PER ASTM C-33, AGGREGATES SHALL BE WELL GRADED FROM FINE TO COARSE WITH LIMITS SPECIFIED IN ASTM C-33, MAXIMUM SIZE OF COARSE AGGREGATE SHALL BE 3/4".

AGGREGATE FOR CEMENT MORTAR SHALL BE CLEAN, SHARP SAND CONFORMING TO ASTM C-144, GRADE SAND FROM COARSE TO FINE WITH 100% PASSING NO. 8 SIEVE, AND NOT OVER 10 TO 30% PASSING NO. 50 SIEVE, HYDRATED LIME SHALL COMPLY WITH ASTM C-207, TYPE S, WATER SHALL BE CLEAN AND FREE FROM ELECTROLYTIC MATERIALS.

ALL MATERIAL USED FOR CONCRETE AND THE DESIGN OF ALL CONCRETE MIXES SHALL CONFORM WITH THE RECOMMENDATIONS OF THE AMERICAN CONCRETE INSTITUTE (ACI 211.1-81).

ALL CONCRETE, UNLESS NOTED OTHERWISE, SHALL DEVELOP A 28-DAY COMPRESSIVE STRENGTH OF 3000 PSI.

JOINT SEALANT SHALL BE HOT LAID BITUMINOUS SEALER.

RIP RAP SHALL BE SOUND, TOUGH DURABLE ROCK OR BROKEN CONCRETE AS APPROVED BY THE GEOTECHNICAL ENGINEER. RIP RAP SHALL BE AT LEAST EIGHT INCH (8") IN DIMENSION AN SHALL HAVE A VOLUME OF NOT LESS THAN 1/3 CUBIC FOOT, SMALLER PIECES PERMITTED FOR FILLING VOIDS.

REINFORCING STEEL FOR CONCRETE SHALL BE INTERMEDIATE GRADE NEW BILLET STEEL CONFORMING TO ASTM A618, GRADE 40. WELDED WIRE MESH SHALL CONFORM TO ASTM DESIGNATION A195 FOR SMOOTH WIRE AND ASTM A497 FOR DEFORMED WIRE.

FORMS FOR FOUNDATIONS AND OTHER CONCRETE WORK SHALL BE WOOD, FORMS SHALL BE OF SUFFICIENT STRENGTH TO SUPPORT THE WEIGHT OF THE CONCRETE BEING PLACED AND TO PREVENT LEAKAGE. FOUNDATIONS MAY BE POURED AGAINST EARTH WHERE CONDITIONS PERMIT.

ALL REINFORCEMENT SHALL BE FABRICATED AND PLACED IN ACCORDANCE WITH ACI 318-77. WELDED WIRE MESH SHALL BE LAPPED 6-INCHES AT ALL EDGES.

THE MIXING, PLACING, CURING AND FINISHING OF CONCRETE SHALL COMPLY WITH ACI 304 AND ACI 318. ALL EXPOSED SURFACES SHALL BE GIVEN A HARD STEEL TROWEL FINISH WITH NO TROWEL MARKS REMAINING, NO CEMENT SHALL BE DUSTED ON THE SURFACE. ALL CONCRETE SHALL BE CURED BY COATING WITH A CLEAR CURING NO CEMENT CONFORMING TO ASTM C-309, OR BY KEEPING IT WET FOR AT LEAST SIX DAYS AFTER POURING. AFTER THE FORMS ARE STRIPPED, ALL EXPOSED CONCRETE SURFACES SHALL BE POINTED AS NEEDED AND RUBBED TO A UNIFORM FINISH.

CONCRETE, UNLESS OTHERWISE NOTED, SHALL HAVE COMPRESSIVE STRENGTH AFTER 28 DAYS OF 3000 PSI. MINIMUM MIX SHALL BE SO PROPORTIONED TO PROVIDE A MINIMUM OF 517 POUNDS OF CEMENT PER CUBIC YARD.

CONCRETE FILL BELOW GRADE FOR PIPE CRADLES ETC. MAY BE 2500 PSI AT 28 DAYS.

CONCRETE, WHERE EXPOSED TO THE WEATHER, SHALL BE AIR ENTRAINED, AIR ENTRAINMENT SHALL BE ACCOMPLISHED BY THE USE OF ADDITIVES CONFORMING TO ASTM C-260. AIR CONTENT SHALL BE 12%. ADDITIVE SHALL BE USED STRICTLY IN ACCORDANCE WITH MANUFACTURER'S PRINTED DIRECTIONS.

READY-MIX CONCRETE SHALL CONFORM TO THE REQUIREMENTS OF ASTM C-94.

CEMENT MORTAR SHALL BE AS SPECIFIED HEREINAFTER. USE METHODS OF MIXING MORTAR MATERIALS CAN BE CONTROLLED AND ACCURATELY MAINTAINED DURING WORK PROGRESS. MORTAR SHALL NOT BE MIXED IN GREATER QUANTITIES THAN SATISFACTORY WORKABILITY. RETEMPERING OF MORTAR IS NOT PERMITTED.

MORTAR FOR LAYING BRICK OR CONCRETE MASONRY UNITS SHALL CONFORM TO ASTM C-270, TYPE M. AVERAGE COMPRESSIVE STRENGTH 2500 AT 28 DAYS. MORTAR MIX SHALL BE PROPORTIONED BY VOLUME. MORTAR FOR PARING SHALL CONSIST OF ONE PART PORTLAND CEMENT AND TWO PARTS SAND.

MORTAR FOR GROUTING OF RIP RAP SHALL CONSIST OF ONE PART PORTLAND CEMENT AND THREE PARTS SAND.

STORM WATER SEWERS: STORM SEWERS SHALL BE INSTALLED IN LOCATIONS AND OF SIZES INDICATED ON DRAWING.

LAY PIPE, EMBED IT FIRMLY TO REQUIRED LINE AND GRADE WITH BELLS OF GROOVE END UP-GRADE, FIT ENDS TOGETHER, EXCAVATE BELL HOLES, SO THAT SEWER WILL HAVE SMOOTH AND UNIFORM INVERT THROUGHOUT ITS LENGTH.

CORRUGATED METAL PIPE SHALL BE PLACED ON A FLAT BOTTOM TRENCH WITH HAUNCHES SOLIDLY SUPPORTED BY TAMPED BEDDING MATERIAL.

WHERE GROUND IS FOUND UNSUITABLE TO SUPPORT PIPE, PROVIDE CONCRETE CRADLES. DEPOSIT CONCRETE, FULL WIDTH OF TRENCH, 4" DEEP MINIMUM TO BOTTOM OF PIPE, REINFORCE CONTINUOUSLY WITH TWO (2) NO. 4 REINFORCING BARS, BEFORE CONCRETE IS SET, EMBED PIPE EVENLY, DEPOSIT REMAINDER OF CONCRETE TO CENTERLINE OF PIPE AND TAMP IN A MANNER TO AVOID DISTURBING PIPE.

WHERE STORM SEWER CROSSES A SANITARY SEWER OR WATER LINE AND THE STORM SEWER IS WITHIN ONE AND A HALF (1-1/2) FEET OF THE SANITARY SEWER PIPE OR WATER LINE, THE INTERSECTION OF THE PIPE OR LINE SHALL BE EMBEDDED IN CONCRETE FOR A DISTANCE OF FIVE FEET (5') EACH WAY FROM CENTERLINE OF INTERSECTION.

PROVIDE POURED CONCRETE FOUNDATIONS FOR DRAINAGE STRUCTURES.

PRECAST CONCRETE BASE MAY BE USED WHERE APPROVED BY THE GEO-TECHNICAL ENGINEER. PRECAST CONCRETE BASE MUST BE SET LEVEL ON SAND CUSHION OF NOT LESS THAN 2" NOR MORE THAN 4".

MANHOLES AND CATCH BASINS SHALL BE CONSTRUCTED OF BRICK, CONCRETE MASONRY OR PRECAST CONCRETE WITH CAST IRON FRAMES, COVERS AND MANHOLE STEPS, AS INDICATED ON DRAWINGS AND SPECIFIED HEREIN.

RIP RAP SHALL BE LAID OVER FILTER FABRIC FROM THE BOTTOM UPWARD, STONES SHALL BE LAID BY HAND WITH EIGHT (8") INCH MINIMUM DIMENSION PERPENDICULAR TO GRADE WITH WELL BROKEN JOINTS, COMPACTED AS IT GOES, TRUE TO LINE. ALL JOINTS SHALL BE FILLED WITH CEMENT MORTAR. SURFACE OF STONE TO BE EXPOSED. CLEAN JOINTS WITH SIRE BRUSH.

BEFORE BACKFILLING AROUND DRAINAGE STRUCTURES, ALL FORMS, TRASH AND DEBRIS SHALL BE REMOVED AND CLEARED AWAY. SELECTED EXCAVATED MATERIAL SHALL BE PLACED SYMMETRICALLY ON ALL SIDES IN EIGHT INCH (8") MAXIMUM LAYERS; EACH LAYER SHALL BE MOISTENED AND COMPACTED WITH MECHANICAL OR HAND TAMPERS.

INFILTRATION OF THE STORM DRAINAGE SYSTEM SHALL NOT EXCEED 0.60 GALLONS PER INCH OF INTERNAL PIPE DIAMETER PER ONE HUNDRED FEET (100') OF PIPELINE PER HOUR WITH A MINIMUM HYDROSTATIC HEAD AT THE CENTER LINE OF THE PIPE OF TWENTY FIVE FEET (25'), OR AS REQUIRED BY GOVERNING CODE AUTHORITIES.

CATCH BASIN FRAMES AND GRATINGS: ASPHALT COATED GRAY CAST IRON, ANSI/ASTM A 48, CLASS 30 B.

IT IS THE CONTRACTOR'S RESPONSIBILITY TO SUPPLY ALL MATERIALS NECESSARY TO COMPLETE DRAINAGE.



SEEDING RATE ZONES

| TYPE OF SEED | SEEDING RATES (LBS./AC) | | | | | | | | | | | |
|---------------------------------|-------------------------------|------------------------------|-------------------------------|------------------------------|-------------------------------|------------------------------|-------------------------------|------------------------------|-------------------------------|------------------------------|-------------------------------|------------------------------|
| | ZONE I | | | | | | ZONE II | | | | | |
| | COASTAL MAR. TO NOV. | INLAND NOV. TO MAR. | COASTAL MAR. TO OCT. | INLAND OCT. TO MAR. | COASTAL MAR. TO DEC. | INLAND DEC. TO FEB. | COASTAL FEB. TO DEC. | INLAND DEC. TO FEB. | COASTAL FEB. TO DEC. | INLAND DEC. TO FEB. | COASTAL FEB. TO DEC. | INLAND DEC. TO FEB. |
| PERMANENT GRASS | | | | | | | | | | | | |
| UNHULLED BERMUDA | 15 | 15 | 10 | 15 | 15 | 15 | 10 | 15 | 15 | 10 | 15 | |
| BAHIA ARGENTINA OR PENSACOLA | | | 30 | 30 | | | | | | 30 | 30 | |
| QUICK GROWING | | | | | | | | | | | | |
| BROWN TOP MILLET | 20 | | 20 | | 20 | | | | | 20 | | |
| ANNUAL RYE GRASS | | 20 | | 20 | | 20 | | 20 | | 20 | | |
| TOTAL POUNDS PER ACRE | 35 | 35 | 60 | 65 | 35 | 35 | 60 | 65 | 60 | 65 | | |

NOTE: THE SEEDING RATES SHOWN IN THIS TABLE APPLY ONLY WHEN SEED IS SPREAD BY AN APPROVED MECHANICAL SPREADER MEETING THE REQUIREMENTS OF SECTION 570 AND 577 OF THE STANDARD SPECIFICATIONS.

GENERAL NOTES

- SPECIAL ATTENTION IS TO BE DIRECTED TO THE CONSTRUCTION OF THE REQUIRED 1" DROP-OFF AT EDGE OF PAVEMENT.
- FERTILIZE ENTIRE UNPAVED SHOULDER AND FRONT SLOPE TO TOE OF SLOPE OR BOTTOM OF DITCH.
- TOPSOIL OBTAINED FROM BORROW PITS OR OTHER SOURCES MAY BE USED IN LIEU OF EXCAVATED TURF AND TOPSOIL WHEN ECONOMICALLY FEASIBLE. NO ADDITIONAL PAYMENT WILL BE MADE FOR SUBSTITUTING TOPSOIL FOR EXCAVATED TURF OR TOPSOIL.

TOPSOIL: IF THE QUANTITY OF EXISTING STORED OR EXCAVATED TOPSOIL IS INADEQUATE FOR PLANTING, SUFFICIENT ADDITIONAL TOPSOIL SHALL BE FURNISHED. TOPSOIL FURNISHED SHALL BE A NATURAL FERTILE, FRAGILE SOIL, POSSESSING CHARACTERISTICS OF REPRESENTATIVE PRODUCTIVE SOILS IN THE VICINITY. IT SHALL BE OBTAINED FROM NATURALLY WELL-DRAINED AREAS.

TOPSOIL SHALL BE WITHOUT ADMIXTURE OF SUBSOIL AND FREE FROM JOHNSON GRASS (SORGHUM HALPENSIS), NUT GRASS (CYPERUS ROTUNDUS) AND OBJECTIONABLE WEEDS AND TOXIC SUBSTANCES.

GROUND LIMESTONE (DOLOMITE) CONTAINING NOT LESS THAN 85 PERCENT OF TOTAL CARBONATES, AND SHALL BE FINISHED TO SUCH A FINENESS THAT 50 PERCENT WILL PASS A 100-MESH SIEVE AND 90 PERCENT WILL PASS A 20-MESH SIEVE.

16-16-16 FORMULATION OF WHICH 60 PERCENT OF THE NITROGEN IS IN THE UREA-FORMALDEHYDE FORM AND SHALL CONFORM TO THE APPLICABLE STATE FERTILIZER LAWS. IT SHALL BE GRANULATED SO THAT 80 PERCENT IS HELD ON A 16-MESH SCREEN, UNIFORM IN COMPOSITION, DRY AND FREE-FLOWING. MULCH: CLEAN HAY OR FREE STRAW MULCH.

AREAS TO BE GRASSED SHALL BE GRADED TO REMOVE DEPRESSIONS, UNDULATIONS, AND IRREGULARITIES IN THE SURFACE BEFORE GRASSING.

PLACING TOPSOIL: AREAS TO BE GRASSED SHALL HAVE A MINIMUM TOPSOIL OVER OF TWO INCHES. TOPSOIL SHALL NOT BE PLACED WHEN THE SUBGRADE IS EXCESSIVELY WET, EXTREMELY DRY OR IN A CONDITION OTHERWISE DETRIMENTAL TO THE PROPOSED PLANTING OR PROPER GRADING.

TILLAGE: THE AREA TO BE GRASSED SHALL BE THOROUGHLY TILLED TO A DEPTH OF FOUR INCHES USING A PLOW AND DISC, HARROW OR ROTARY TILLING MACHINERY UNTIL A SUITABLE BED HAS BEEN PREPARED AND NO CLODS OR CLUMPS REMAIN LARGER THAN 1-1/2 INCHES IN DIAMETER.

APPLICATION OF LIME: THE PH OF THE SOIL SHALL BE DETERMINED. IF THE PH IS BELOW 5.0, SUFFICIENT LIME SHALL BE ADDED TO PROVIDE A PH BETWEEN 5.5 AND 6.5. THE LIME SHALL BE THOROUGHLY INCORPORATED INTO THE TOP THREE TO FOUR INCHES OF THE SOIL. LIME AND FERTILIZER MAY BE APPLIED IN ONE OPERATION.

APPLICATION OF FERTILIZER: FERTILIZER SHALL BE APPLIED AT THE RATE OF 6 POUNDS PER 1,000 SQUARE FEET AND SHALL BE THOROUGHLY INCORPORATED INTO THE TOP THREE TO FOUR INCHES OF SOIL.

ALL AREAS DISTURBED DURING CONSTRUCTION SHALL BE SEED AS SPECIFIED HEREIN. IMMEDIATELY BEFORE SEEDS ARE SOWN AND AFTER FERTILIZER AND LIME ARE APPLIED, THE GROUND SHALL BE SCARIFIED AS NECESSARY AND SHALL BE RAKED UNTIL HE SURFACE IS SMOOTH, FRAGILE, AND OF UNIFORMLY FINE TEXTURE. AREAS TO BE GRASSED SHALL BE SEED EVENLY WITH A MECHANICAL SPREADER, RAKED LIGHTLY, ROLLED WITH A 200-POUND ROLLER, AND WATERED WITH A FINE SPRAY.

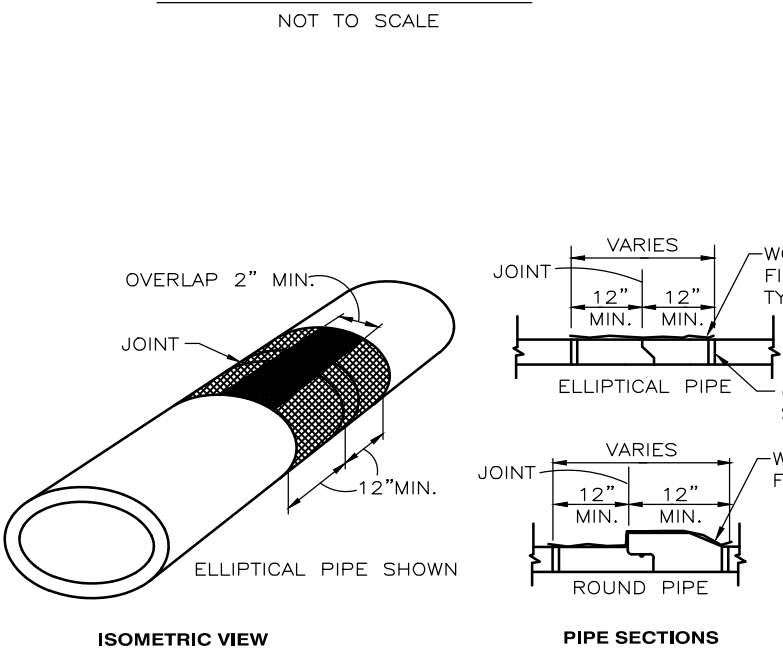
SEEDS SHALL BE APPLIED AT THE FOLLOWING RATE:
SEEDS RATE OF APPLICATION
BERMUDA 6 LBS./1000 SQ.FT.

SEEDED AREAS SHALL BE MULCHED AT THE RATE OF NOT LESS THAN 1-1/2" LOOSE MEASUREMENT OVER ALL SEEDED AREAS. SPREAD BY HAND, BLOWER, OR OTHER SUITABLE EQUIPMENT. MULCH SHALL BE CUT INTO THE SOIL WITH EQUIPMENT CAPABLE OF CUTTING THE MULCH UNIFORMLY INTO THE SOIL. MULCHING SHALL BE DONE WITHIN 24 OURS OF THE TIME SEEDING IS COMPLETED.

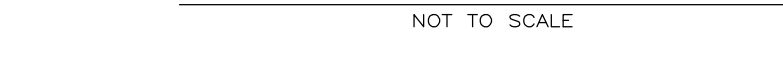
AFTER SEEDING AND MULCHING, A CULTIPACKER, TRAFFIC ROLLER, OR OTHER SUITABLE EQUIPMENT SHALL BE USED FOR ROLLING THE GRASSED AREAS. AREAS SHALL THEN BE WATERED WITHIN A FINE SPRAY.

ALL AREAS TO BE GRASSED SHALL BE PROTECTED AGAINST EROSION AT ALL TIMES. FOR PROTECTION DURING WINTER MONTHS (NOVEMBER 1ST THRU MARCH 31ST) ITALIAN RYE GRASS SHALL BE PLANTED AT A RATE OF FOUR POUNDS PER 1,000 SQUARE FEET ON ALL AREAS WHICH ARE NOT PROTECTED BY PERMANENT GRASS.

SEEDING DETAIL



FILTER FABRIC JACKET DETAIL



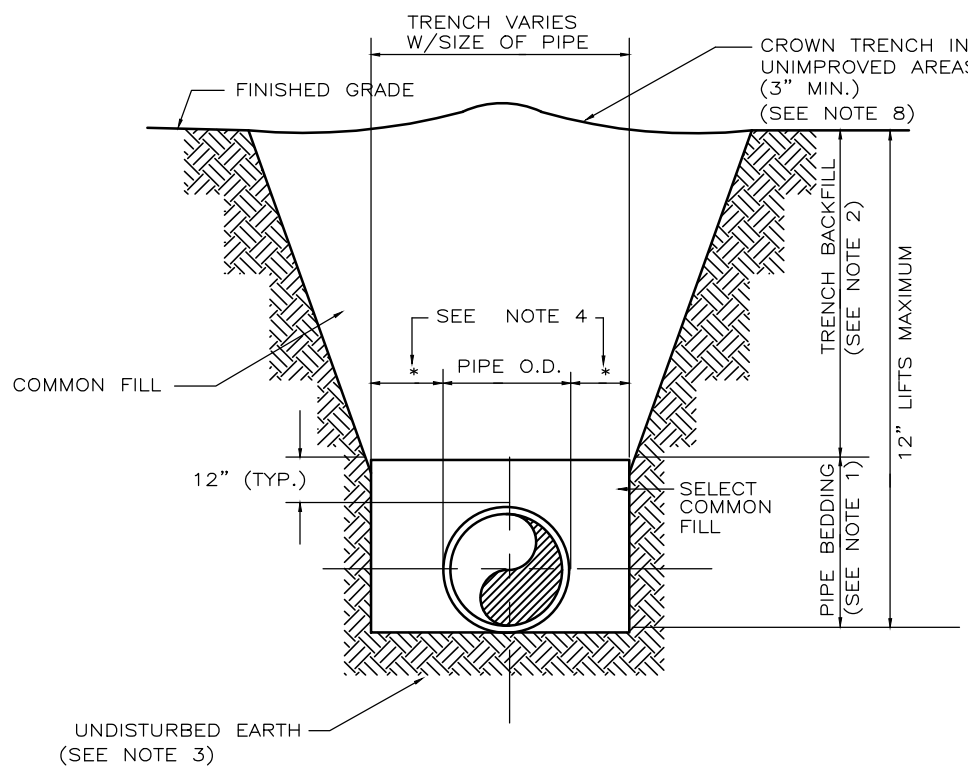
MINIMUM TECHNICAL STANDARDS CHECKLIST FOR UTILITY AS-BUILTS

CITY OF PANAMA CITY BEACH
DATED MAY, 2012

SURVEYORS AND MAPPERS MUST MEET THE FOLLOWING MINIMUM STANDARDS OF ACCURACY, COMPLETENESS, AND QUALITY FOR THE CITY OF PANAMA CITY BEACH TO ACCEPT AS-BUILTS.

- MUST IDENTIFY THE RESPONSIBLE SURVEYOR AND MAPPER.
- MUST STATE THE TYPE OF SURVEY IT DEPICTS AND THE PURPOSE OF THE SURVEY.
- MUST BEAR THE NAME, CERTIFICATE OF AUTHORIZATION NUMBER, AND STREET AND MAILING ADDRESS OF THE BUSINESS ENTITY ISSUING THE AS-BUILT SURVEY, ALONG WITH THE NAME AND LICENSE NUMBER OF THE SURVEYOR IN RESPONSIBLE CHARGE.
- MUST REFLECT A SURVEY DATE, WHICH IS THE DATE OF ACQUISITION. WHEN THE GRAPHICS OF THE AS-BUILT SURVEY ARE REVISED, BUT THE SURVEY DATE STAYS THE SAME, THE AS-BUILT SURVEY MUST LIST DATES FOR ALL REVISIONS.
- MUST BE SIGNED AND SEALED BY THE SURVEYOR IN RESPONSIBLE CHARGE.
- A DESIGNATED "NORTH ARROW" AND EITHER A STATED SCALE OR GRAPHIC SCALE SHALL BE SHOWN.
- APPROPRIATE LINE TYPES, LINE WEIGHTS, AND LINE WIDTHS SHALL BE USED ON THE AS-BUILT DRAWING TO DIFFERENTIATE EXISTING FROM PROPOSED AND WATER FROM SEWER, RECLAIM, AND STORM. ALL PHYSICAL ITEMS (I.E. PIPES, VALVES, ETC.), SURVEYED BOUNDARIES, AND EASEMENTS SHOULD BE CLEARLY MARKED, AND DIMENSIONED, AND IDENTIFIED BY SIZE AND MATERIAL.
- ALL UTILITIES IN THE PUBLIC RIGHT OF WAY AND WITHIN EASEMENTS OR TO THE END OF THE PUBLICLY OWNED PORTION OF THE UTILITY (I.E. METER AND BACKFLOW PREVENTER, CLEANOUT, ETC.) SHALL BE SHOWN WITH ASSOCIATED SIZES LABELED. THIS INCLUDES, BUT IS NOT LIMITED TO, STUB-OUTS/LATERALS, METERS, BFP'S, WATER MAINS, FORCE MAINS, GRAVITY SEWER MAINS, MANHOLES, STORM WATER PIPING AND ASSOCIATED STRUCTURES, VALVES, FIRE HYDRANTS, LIFT STATIONS, ETC. ALL PIPE LINE WORK MUST BE CONNECTED WITHIN THE SITE AS WELL AS TO EXISTING UTILITIES ADJACENT TO THE SITE (IT IS THE SURVEYOR'S RESPONSIBILITY TO COORDINATE WITH ALL CONTRACTORS FOR LOCATIONS AND SIZING). ALL UTILITY CONNECTIONS TO THE BUILDINGS MUST BE SHOWN.
- ALL PROPOSED UTILITY/INGRESS/EGRESS EASEMENTS MUST BE SHOWN ON THE DRAWING AND MUST HAVE THE ASSOCIATED LEGAL DESCRIPTION WRITTEN.
- EDGE OF PAVEMENT, ROADS (ASPHALT SHALDES), CURBS, DRIVEWAY CONNECTIONS, BUILDINGS, PARKING LOTS, RIGHT-OF-WAY, AND STREET NAMES MUST BE SHOWN IN ALL APPLICATIONS. ALL ITEMS MENTIONED ABOVE MUST BE FIELD LOCATED.
- IF A LIFT STATION IS TO BE DEDICATED TO THE CITY THE PLAN MUST SHOW A DETAIL SCALED AT 1"=10' SHOWING ALL IMPROVEMENTS INCLUDING: WATER AND SEWER SERVICES, MANHOLES, INVERTS, RIMS, BFP'S, YARD HYDRANTS, CONTROL PANELS, FENCING, PARCEL BOUNDARY, LEGAL DESCRIPTION OF PARCEL BOUNDARY, WET WELL, VALVE BOX, FORCE MAIN, FLOW METER (IF APPLICABLE), DRIVEWAY, GATE.
- PROPERTY BOUNDARY MUST BE CLEARLY LABELED AND DIMENSIONED.
- INVERTS, GRATES, TOPS, RIMS MUST BE SHOWN FOR ALL STORM WATER DRAINAGE STRUCTURES. INVERTS (PIPES AND CLEANOUTS) AND RIMS MUST BE SHOWN FOR ALL GRAVITY SEWER MANHOLES. SLOPES MUST BE SHOWN ON EACH RUN OF PIPE FOR REVIEW AND APPROVAL.
- "AS-BUILT" PROFILE OF ALL DIRECTIONAL BORES AND JACK-AND-BORES INDICATING GRADE AND PIPE ELEVATIONS AT 10 FOOT INTERVALS SHALL BE PROVIDED ON AS-BUILT PLAN SHEETS BASED ON BORE LOGS DEVELOPED BY BORING CONTRACTOR DURING INSTALLATION. PROFILES SHALL USE HORIZONTAL STATIONING WHICH TIES TO STATIONING ON PLANS. PROFILES SHALL ALSO SHOW EXISTING SURFACE ELEVATIONS AS WELL AS ANY PROPOSED SURFACE ELEVATIONS ON THE PROFILE. SURFACE PROFILES MUST SHOW ANY PAVEMENT SIDEWALKS, DITCHES, SWALES, ETC. NOTE THAT PROFILES LOCATING PIPE SOLELY BY "DEPTH BELOW EXISTING GROUND" WILL NOT BE ACCEPTED.
- COASTAL SETBACK LINE OR COASTAL CONSTRUCTION CONTROL LINE SHOULD BE DESIGNATED.
- ELEVATIONS AND LOCATION OF ANY FLOOD ZONES ALONG THE FLOOD HAZARD BOUNDARIES SHALL BE DELINEATED.
- NEARBY WETLANDS AND OTHER ENVIRONMENTALLY SIGNIFICANT RESOURCES CLEARLY LABELED.
- STORM WATER MANAGEMENT SYSTEM FEATURES INCLUDING DIMENSIONS OF: WET AND DRY SWALES, WET AND DRY PONDS, CONVEYANCE SYSTEMS; EASEMENTS; ALONG WITH ALL ASSOCIATED M.E.S. STRUCTURES AND INVERTS, OUTFALL STRUCTURES AND INVERTS, SKIMMERS, DISCHARGE STRUCTURES AND INVERTS AND SLOT ELEVATIONS, TOP OF BANK, SLOPE OF BANK AND BOTTOM OF ALL PONDS, SWALES, CLOSED AND OPEN CONVEYANCES. FOR FEMA LOBR SUBMITTALS ALSO PROVIDE: FINISHED FLOOR ELEVATIONS, SPOT ELEVATIONS AND/OR CONTOURS SHOWING LOWEST LOT ELEVATIONS.
- THE ENGINEER OF RECORD SHALL REVIEW AND APPROVE THE AS-BUILT PRIOR TO SUBMISSION TO THE CITY FOR FINAL APPROVAL. WRITTEN APPROVAL BY THE ENGINEER OF RECORD SHALL BE NOTED ON A TRANSMITTAL WITH A STATEMENT OF NO EXCEPTIONS TO MINIMUM STANDARDS PROVIDED HEREIN.

STORM WATER REQUIREMENTS FOR THE AS-BUILT SURVEYS ONLY APPLY TO PARCELS WITHIN CITY LIMITS. PLEASE SUBMIT THREE (3) HARD COPIES AND ONE (1) DIGITAL (AUTOCAD FORMAT & PDF) FOR REVIEW AND APPROVAL.



- NOTES:
- PIPE BEDDING: SELECT COMMON FILL COMPACTED TO 95% OF THE MAXIMUM DENSITY AS PER AASHTO T-180.
 - TRENCH BACKFILL: COMMON FILL COMPACTED TO 95% (6" LIFTS) OF THE MAXIMUM DENSITY AS PER AASHTO T-180.
 - PIPE BEDDING UTILIZING SELECT COMMON FILL OR BEDDING ROCK IN ACCORDANCE WITH TYPE A BEDDING AND TRENCHING DETAIL MAY BE REQUIRED AS DIRECTED BY THE CITY.
 - (*) 15" MAX. FOR PIPE DIAMETER LESS THAN 24", AND 24" MAX. FOR PIPE DIAMETER 24" AND LARGER.
 - WATER SHALL NOT BE PERMITTED IN THE TRENCH DURING CONSTRUCTION.
 - ALL PIPE TO BE INSTALLED WITH BELL FACING UPSTREAM TO THE DIRECTION OF THE FLOW.
 - REFER TO SECTION 32.5 OF THE MANUAL FOR SHEETING AND BRACING IN EXCAVATION.
 - FINAL RESTORATION IN IMPROVED AREAS SHALL BE IN COMPLIANCE WITH ALL APPLICABLE REGULATIONS OF GOVERNING AGENCIES. SURFACE RESTORATION WITHIN CITY RIGHT-OF-WAY SHALL COMPLY WITH THE REQUIREMENTS OF RIGHT-OF-WAY UTILIZATION REGULATIONS AND ROAD CONSTRUCTION SPECIFICATIONS.

TRENCHES AND EXCAVATION PITS SHALL NOT BE BACKFILLED UNTIL ALL TESTS AND INSPECTIONS COVERING THE INSTALLATION OF THE STORM DRAINAGE SYSTEM HAVE BEEN PERFORMED AND APPROVED.

ALL TIMBER SHEETING BELOW A PLANE ONE FOOT ABOVE TOP OF PIPE SHALL REMAIN IN PLACE IN ORDER NOT TO DISTURB PIPE GRADING. BEFORE BACKFILLING, REMOVE ALL OTHER SHEETING, BRACING AND SHORING. PIPE TO BE CAREFULLY COMPACTED TO NINETY FIVE PERCENT (95%) OF MAXIMUM DENSITY AS PER ASTM D-1557 UNTIL ONE FOOT (1') OF COVER EXISTS OVER PIPE.

IN STREETS, DRIVES, PARKING LOTS AND OTHER AREAS TO HAVE OR HAVING IMPROVED HARD SURFACES, BACKFILL SHALL BE MATERIAL SPECIFIED AS FOR PIPE BEDDING AND SHALL BE DEPOSITED IN SIX INCH (6") LOOSE LAYERS AS OPTIMUM MOISTURE CONTENT (+.2%) AND COMPACTED TO 95% OF MAXIMUM DENSITY AS PER ASTM D-1557 WHERE SERVICES OR UTILITY LINES CROSS STREET. BEDDING SHALL BE CARRIED TO FIVE FEET (5') BEHIND THE CURB, OR WHERE SIDEWALKS EXISTS, TO THE SIDE OF SIDEWALK FARTHEST AWAY FROM THE STREET.

MATERIAL USED FOR BEDDING SHALL MEET CURRENT RECOMMENDATIONS OF THE PIPE MANUFACTURER AND SHALL BE APPROVED BY THE ENGINEER. THE SPECIFIED COHESIONLESS MATERIAL SHALL BE PLACED IN THE TRENCH SIMULTANEOUSLY ON EACH SIDE OF THE PIPE TO THE FULL WIDTH OF THE TRENCH. MATERIAL WILL BE PLACED IN A MAXIMUM LIFT OF SIX (6) INCHES (COMPACTED DEPTH) TO A MINIMUM DEPTH OF ONE (1) FOOT ABOVE THE CROWN OF THE PIPE.

PERFORM ALL TRENCHING REQUIRED FOR THE INSTALLATION OF UTILITIES AS SHOWN ON PLANS AND SPECIFIED HEREIN. MAKE ALL TRENCHES OPEN VERTICAL CONSTRUCTION WITH SUFFICIENT WIDTH TO PROVIDE FREE WORKING SPACE AT BOTH SIDE OF THE TRENCH AND AROUND THE INSTALLED ITEMS AS REQUIRED FOR CAULKING, JOINING, BACKFILLING AND COMPACTING.

PROPERLY SUPPORT ALL TRENCHES IN STRICT ACCORDANCE WITH ALL PERTINENT RULES AND REGULATIONS.

GRADE THE TRENCH BOTTOM TO PROVIDE A SMOOTH, FIRM AND STABLE FOUNDATION FREE OF ROCK POINTS THROUGHOUT THE LENGTH OF THE PIPE. IN AREAS WHERE SOFT, UNSTABLE MATERIALS ARE ENCOUNTERED AT THE SURFACE UPON WHICH COHESIONLESS MATERIAL IS TO BE PLACED, REMOVE THE UNSTABLE MATERIAL AND REPLACE IT WITH MATERIAL APPROVED BY THE ENGINEER, MAKE SUFFICIENT DEPTH TO DEVELOP A FIRM FOUNDATION FOR THE ITEM BEING INSTALLED.

AT EACH JOINT IN PIPE, RECESS THE BOTTOM OF THE TRENCH AS REQUIRED INTO THE FIRM FOUNDATION IN SUCH A MANNER AS TO RELIEVE THE BELL OF THE PIPE OF ALL LOAD AND TO ENSURE CONTINUOUS BEARING OF THE PIPE BARREL ON THE FIRM FOUNDATION.

ACCURATELY SHAPE ALL PIPE SUBGRADE AND FIT THE BOTTOM OF THE TRENCH TO THE PIPE SHAPE. USE A DRAG TEMPLATE SHAPED TO CONFORM TO THE OUTER SURFACE OF THE PIPE IF OTHER METHODS DO NOT PRODUCE SATISFACTORY RESULTS. SHAPING WILL CONFORM TO THE OUTSIDE OF THE PIPE FOR A DEPTH OF NOT LESS THAN 10% OF THE TOTAL HEIGHT (OUTSIDE DIMENSION) OF THE PIPE.

PIPE TRENCHES SHALL BE EXCAVATED TO A DEPTH THAT WILL INSURE A MINIMUM OF THIRTY INCHES OF COVER LESS OTHERWISE SHOWN ON THE DRAWINGS OR DIRECTED.

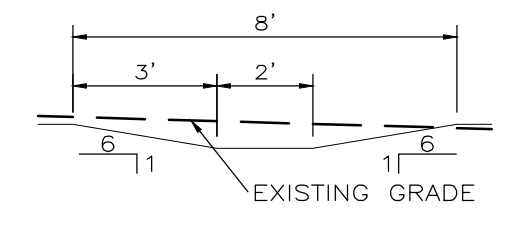
BACKFILL OF EARTH AROUND MANHOLES SHALL BE FILLED WITH THOROUGHLY COMPACTED SAND OR GRAVEL AT THE EXPENSE OF THE CONTRACTOR.

TRENCHES SHALL BE BACKFILLED WITH EXCAVATED MATERIALS, FREE FROM LARGE CLODS OR STONES. BACKFILL SHALL BE DEPOSITED IN LAYERS NOT TO EXCEED 6-INCHES (6") IN THICKNESS, MOISTENED, AND COMPACTED TO DENSITY EQUAL TO OR GREATER THAN 95% OF THE MAXIMUM DENSITY OF AASHTO STANDARD METHOD T-99, TO A MINIMUM DEPTH OF 12-INCHES OVER THE PIPE. THE REMAINDER OF THE BACKFILL SHALL BE PLACED IN 8-INCH LAYERS COMPACTED TO 95% MAXIMUM DENSITY UNLESS THE BACKFILL IS BENEATH PAVED OR BUILDING AREAS IN WHICH CASE IT SHALL BE COMPACTED TO 95% OF A MODIFIED PROCTOR.

EXCAVATIONS FOR PIPE LAYING OPERATIONS SHALL BE CONSTRUCTED IN A MANNER TO CAUSE THE LEAST INTERRUPTION TO TRAFFIC. WHEN TRAFFIC MUST CROSS OPEN TRENCHES THE CONTRACTOR SHALL PROVIDE SATISFACTORY BRIDGES.

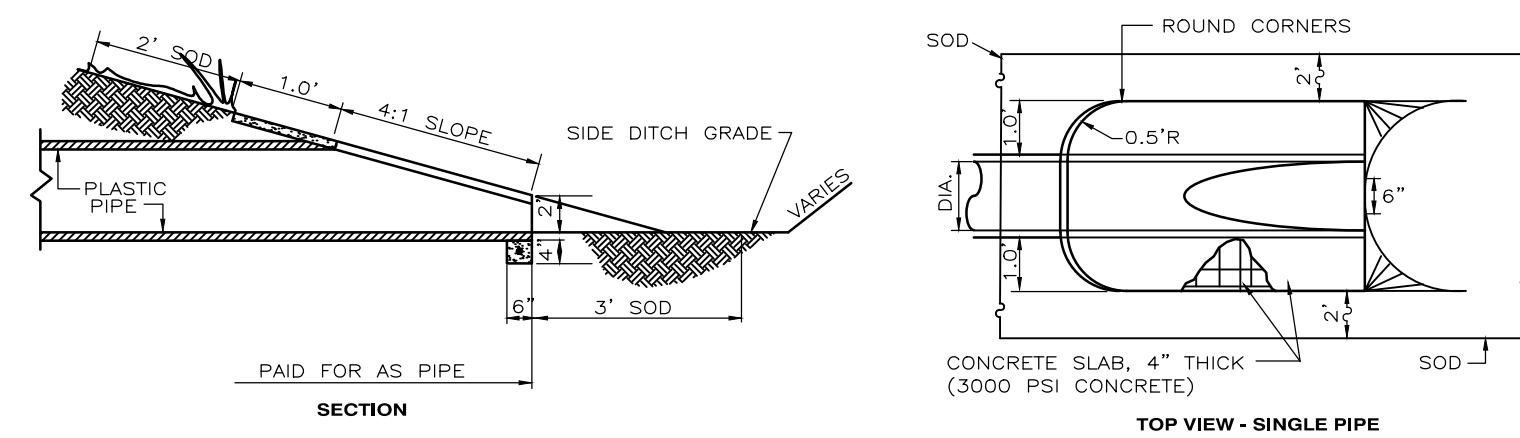
TYPE B BEDDING AND TRENCHING DETAIL

NOT TO SCALE



TYPICAL SWALE DETAIL

NOT TO SCALE



CONCRETE MITERED END DETAIL

NOT TO SCALE

REVISIONS

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PHASE

| | DRAWN | CHECKED | DATE |
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| SCHEMATIC DESIGN | MAY | SLB | 10/17/25 |
| DESIGN DEVELOPMENT | MAY | SLB | 1/9/26 |
| CONSTRUCTION DOCUMENTS | MAY | SLB | 4/3/26 |

JRA ARCHITECTS 2211 NAVY BLVD., STE 100
PANAMA CITY BEACH, FL
PHONE: (850) 236-9832
Commission Number: 25871

CONSULTANTS:

PROJECT:
BAY DISTRICT SCHOOLS
NEW SOFTBALL FIELD
HOUSE
MOSLEY HIGH SCHOOL
LYNN HAVEN, FLORIDA
SHEET TITLE:

CONSTRUCTION DETAILS

SHEET NUMBER:
C2.

ASPHALTIC CONCRETE PAVING

PROVIDE ALL LABOR, MATERIALS, EQUIPMENT, SERVICES, ETC. NECESSARY AND INCIDENTAL TO THE COMPLETION OF ALL PAVEMENT AS SHOWN ON THE DRAWINGS AND AS SPECIFIED HEREIN.

SUBMIT A "LETTER OF INTENT" FOR THE FOLLOWING:

ASPHALT PAVING MATERIAL AND MIX DESIGN. PROVIDE COPIES OF MATERIALS CERTIFICATES SIGNED BY MATERIAL PRODUCER AND CONTRACTOR, CERTIFYING THAT EACH MATERIAL ITEM COMPLIES WITH, OR EXCEEDS, SPECIFIED REQUIREMENTS.

WEATHER LIMITATIONS: APPLY PRIME AND TACK COATS WHEN AMBIENT TEMPERATURE IS ABOVE 50 DEGREES F. (10 DEGREES C), AND WHEN TEMPERATURE HAS NOT BEEN BELOW 35 DEGREES F. (1 DEGREE C) FOR 12 HOURS IMMEDIATELY PRIOR TO APPLICATION. DO NOT APPLY WHEN BASE IS WET OR CONTAINS AN EXCESS OF MOISTURE.

CONSTRUCT ASPHALT CONCRETE SURFACE COURSE WHEN ATMOSPHERIC TEMPERATURE IS ABOVE 40 DEGREES F. (4 DEGREES C), AND WHEN BASE IS DRY. SURFACE COURSE MAY BE PLACED WHEN AIR TEMPERATURE IS ABOVE 30 DEGREES F. (-1 DEGREE C) AND RISING. GRADE CONTROL: ESTABLISH AND MAINTAIN REQUIRED LINES AND ELEVATIONS.

THE SUBCONTRACTOR SHALL WARRANT ALL ASPHALT PAVING AGAINST DEFECTS IN MATERIALS AND WORKMANSHIP FOR A PERIOD OF TWO YEARS.

PRODUCTS: USE LOCALLY AVAILABLE MATERIALS AND GRADATIONS WHICH EXHIBIT A SATISFACTORY RECORD OF PREVIOUS INSTALLATIONS.

AGGREGATE: CRUSHED STONE, CRUSHED GRAVEL, AND SHARP-EDGED NATURAL SAND. MAXIMUM AGGREGATE SIZE SHALL BE NO GREATER THAN ONE-HALF OF THE DESIGN THICKNESS OF THE WEARING OR BINDER COURSE.

SURFACE PREPARATION: PROOF ROLL PREPARED BASE SURFACE TO CHECK FOR UNSTABLE AREAS AND AREAS REQUIRING ADDITIONAL COMPACTION.

NOTIFY CONTRACTOR OF UNSATISFACTORY CONDITIONS. DO NOT BEGIN PAVING WORK UNTIL DEFICIENT BASE AREAS HAVE BEEN CORRECTED AND ARE READY TO RECEIVE PAVING.

PRIME COAT: APPLY AT RATE OF 0.2 TO 0.5 GAL. PER SQ. YD., OVER COMPACTED BASE. APPLY MATERIAL AND SEAL BUT NOT FLOOD SURFACE. CURE AS DIRECTED AND DRY AS LONG AS NECESSARY TO ATTAIN PENETRATION AND EVAPORATION OF VOLATILE.

TACK COAT: APPLY TO CONTACT SURFACE OF PREVIOUSLY CONSTRUCTED ASPHALT OR PORTLAND CEMENT CONCRETE AND SURFACES ABUTTING OR PROJECTING INTO ASPHALT CONCRETE PAVEMENT. DISTRIBUTE AT RATE OF 0.05 TO 0.31 GAL. PER SQ. YD. OF SURFACE.

ALLOW TO DRY UNTIL AT PROPER CONDITION TO RECEIVE PAVING.

ASPHALT CONCRETE MIX: THIS ITEM SHALL CONSIST OF A WEARING SURFACE CONSTRUCTED OF ASPHALTIC CONCRETE ON A PREPARED BASE.

THE MATERIALS AND CONSTRUCTION METHODS SHALL COMPLY WITH THOSE SET FORTH FOR ASPHALTIC CONCRETE IN THE LATEST F.O.D.T. EDITION OF THE STANDARD SPECIFICATIONS.

THE ASPHALTIC CEMENT SHALL MEET THE REQUIREMENTS OF AASHTO SPECIFICATIONS M-20, VISCOSITY GRADE AC-20 (PENETRATION GRADE 60-70).

JOB MIX FORMULA: THE MARSHALL TESTING WILL BE USED IN ESTABLISHING THE JOB MIX FORMULA AND FOR CONTROL TESTING THROUGHOUT THE WORK.

THE DENSITY OF FIELD SAMPLES SHALL NOT BE LESS THAN 98% OF THE MARSHALL LABORATORY COMPACTED MIXTURE COMPOSED OF THE SAME MATERIALS IN LIKE PROPORTIONS.

THE THICKNESS OF THE SURFACE SHALL BE AS SPECIFIED IN THE SITE WORK PLANS. THIS REQUIREMENT SHALL BE CHECKED BY CORES AND WHERE A DEFICIENCY OF MORE THAN 1/4" EXISTS, THE CONTRACTOR SHALL BE REQUIRED TO CORRECT THE DEFICIENCY EITHER BY REPLACING THE FULL THICKNESS OR OVERLAYING THE AREAS TO THE SATISFACTION OF THE ENGINEER.

SAND ASPHALT BASE

PLACE ASPHALT CONCRETE MIXTURE ON PREPARED SURFACE. SPREAD AND STRIKE-OFF. SPREAD MIXTURE AT MINIMUM TEMPERATURE OF 225 DEGREES F. (107 DEGREES C).

PLACE IN STRIPS NOT LESS THAN 10' WIDE, UNLESS OTHERWISE ACCEPTABLE TO THE ENGINEER. AFTER FIRST STRIP HAS BEEN PLACED AND ROLLED, PLACE SUCCEEDING STRIPS AND EXTENDED ROLLING TO OVERLAP PREVIOUS STRIPS. COMPLETE BASE COURSE FOR A SECTION BEFORE PLACING SURFACE COURSE.

MAKE JOINTS BETWEEN OLD AND NEW PAVEMENTS, OR BETWEEN SUCCESSIVE DAYS' WORK, TO ENSURE CONTINUOUS BOND BETWEEN ADJOINING WORK. CLEAN CONTACT SURFACES AND APPLY TACK COAT.

BEGIN ROLLING WHEN MIXTURE WILL BEAR ROLLER WEIGHT WITHOUT EXCESSIVE DISPLACEMENT.

ACCOMPLISH BREAKDOWN OR INITIAL ROLLING IMMEDIATELY FOLLOWING ROLLING OF JOINTS AND OUTSIDE EDGE. CHECK SURFACE AFTER BREAKDOWN ROLLING, AND REPAIR DISPLACED AREAS BY LOOSENING AND FILLING, IF REQUIRED, WITH HOT MATERIAL. CONTINUE SECOND ROLLING UNTIL MIXTURE HAS BEEN THOROUGHLY COMPACTED.

PERFORM FINISH ROLLING WHILE MIXTURE IS STILL WARM ENOUGH FOR REMOVAL OF ROLLER MARKS. CONTINUE ROLLING UNTIL ROLLER MARKS ARE ELIMINATED AND COURSE HAS ATTAINED MAXIMUM DENSITY. AFTER FINAL ROLLING, DO NOT PERMIT VEHICULAR TRAFFIC ON PAVEMENT UNTIL IT HAS COOLED AND HARDENED. ERECT BARRICADES TO PROTECT PAVING FROM TRAFFIC UNTIL MIXTURE HAS COOLED ENOUGH NOT TO BECOME MARKED.

TEST IN-PLACE ASPHALT CONCRETE COURSES FOR PAVING AS DIRECTED BY ENGINEER FOR SMOOTHNESS.

THICKNESS: IN-PLACE COMPACTED THICKNESS WILL NOT BE ACCEPTABLE IF EXCEEDING FOLLOWING ALLOWABLE VARIATION FROM REQUIRED THICKNESS:

BASE COURSE: 1/2" PLUS OR MINUS
SURFACE COURSE: 1/4" PLUS OR MINUS

SURFACE SMOOTHNESS: TEST FINISHED SURFACE OF EACH ASPHALT CONCRETE COURSE FOR SMOOTHNESS, USING 10' STRAIGHT EDGE APPLIED PARALLEL WITH, AND AT RIGHT ANGLES TO CENTER OF PAVED AREAS. SURFACES WILL NOT BE ACCEPTABLE IF EXCEEDING THE FOLLOWING TOLERANCES FOR SMOOTHNESS:

BASE COURSE SURFACE: 1/4"
WEARING COURSE SURFACE: 3/16"
CHECK SURFACED AREAS AT INTERVALS AS DIRECTED BY ENGINEER.

FIELD DENSITY AND SOIL BEARING CAPACITY TESTS SHALL BE PERFORMED BY THE GEOTECHNICAL ENGINEER. PROVIDE INSPECTION, CERTIFICATION OF PAVEMENT CONSTRUCTION, FIELD TESTS AND CORE SAMPLES OF THE COMPLETE PAVEMENT CONSTRUCTION.

MISCELLANEOUS PAVEMENT

WORK INCLUDED CONSISTS OF BUT IS NOT LIMITED TO THE FOLLOWING:

CONCRETE SIDEWALKS, CURBS, CURB AND GUTTER, INCLUDING POROUS FILL.

CONCRETE LIGHT POLE BASES.

SUBMIT A "LETTER OF INTENT" FOR THE FOLLOWING:

CONCRETE MIX DESIGN.

THIS SUBCONTRACTOR SHALL WARRANT ALL ASPHALT PAVING AGAINST DEFECTS IN MATERIALS AND WORKMANSHIP FOR A PERIOD OF TWO (2) YEARS.

POROUS FILL SHALL BE CLEAN COARSE SAND, FREE DRAINING GRAVEL, OR CRUSHED ROCK ALL AS APPROVED BY THE GEOTECHNICAL ENGINEER.

POROUS FILL UNDER SIDEWALKS, ETC., SHALL BE GRADED BETWEEN 3/8" AND NO. 200 SIEVE.

POROUS FILL SHALL BE CAPABLE OF BEING COMPACTED TO NOT LESS THAN 95% OF THE MAXIMUM DRY DENSITY AS DETERMINED BY ASTM-1557.

STEEL REINFORCING BARS SHALL CONFORM TO "SPECIFICATIONS FOR DEFORMED BILLET STEEL BARS FOR CONCRETE REINFORCEMENT", ASTM A-615 GRADE NO. 60, HAVING A MINIMUM YIELD STRENGTH OF 60,000 PSI.

TIE WIRE SHALL BE BLACK ANNEALED WIRE, 16 GAUGE MINIMUM. BAR SUPPORTS SHALL CONFORM TO THE "BAR SUPPORT SPECIFICATIONS" CONTAINED IN "MANUAL OF STANDARD PRACTICE" AS PUBLISHED BY CRSI AND WCSI. BAR SUPPORTS AND ACCESSORIES WITHIN 1/2" OF SURFACE OF CONCRETE EXPOSED TO WEATHER SHALL BE NON-CORROSIVE.

CEMENT SHALL BE GRAY PORTLAND CEMENT, TYPE I OR II, CONFORMING TO ASTM C-150 OR ASTM C-175 FOR AIR-ENTRAINING PORTLAND CEMENT.

CONCRETE AGGREGATES SHALL CONFORM TO ASTM C-33.

FINE AND COARSE AGGREGATES SHALL BE REGARDED AS SEPARATE INGREDIENTS AND EACH SHALL CONFORM TO THE APPROPRIATE GRADING REQUIREMENTS OF ASTM C-33.

AIR-ENTRAINING ADMIXTURES SHALL CONFORM TO ASTM C-260. EXPANSION JOINTS SHALL BE 1/2" THICK GANE FIBER EXPANSION JOINTS, CONFORMING TO ASTM D-1751.

EXPANSION JOINT SEALANT SHALL BE TRAFFIC GRADE, SELF LEVELING TREMCO THC-900® OR FERRODIA CORPORATION "MF-200". COLOR SHALL BE BLACK. SHALL BE AS RECOMMENDED BY SEALANT MANUFACTURER.

CURING COMPOUND SHALL BE CLEAR, CONFORMING TO ASTM C-309. CURING COMPOUND SHALL BE COMPATIBLE WITH PAINTS, ETC., SCHEDULED OR SPECIFIED FOR APPLICATION TO CONCRETE SURFACE.

ALL CONCRETE, UNLESS OTHERWISE NOTED, SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH OF 3,000 PSI AT 28 DAYS. MIX DESIGN SHALL BE SO PROPORTIONED TO PROVIDE A MINIMUM OF 517 POUNDS OF CEMENT PER CUBIC YARD.

ALL CONCRETE SHALL BE PROPORTIONED TO HAVE A SLUMP OF 4" MAXIMUM. TOLERANCE IN SLUMP SHALL NOT EXCEED ACI RECOMMENDATIONS.

READY-MIXED CONCRETE SHALL CONFORM TO ASTM C-94 AND THE NATIONAL READY MIX CONCRETE ASSOCIATION.

POROUS FILL SHALL BE LAID AND COMPACTED TO A MINIMUM DEPTH OF 3", UNLESS OTHERWISE INDICATED, UNDER ALL SIDEWALKS, ETC..

POROUS FILL SHALL BE COMPACTED TO NOT LESS THAN 95% MAXIMUM DRY DENSITY AS DETERMINED BY ASTM D-1557.

IT IS THE CONTRACTOR'S RESPONSIBILITY TO SUPPLY ALL MATERIALS NECESSARY TO COMPLETE PAVING.

SITE IMPROVEMENTS

ALL OFF-SITE WORK INCLUDED CONSISTS OF BUT IS NOT LIMITED TO THE FOLLOWING:

SITE RELATED FENCING: GUARD POSTS, GUARD RAIL AND POSTS AND SIGN POSTS LOCATED ON THE SITE. TRAFFIC CONTROL SIGNS, GUARD POSTS,

GUARD RAIL AND POSTS AND SIGN POSTS:

STEEL SHAPES SHALL CONFORM TO ASTM A-36.

STEEL PIPE SHALL CONFORM TO ASTM A-53, E OR S, TYPE B.

STEEL PIPE SHALL CONFORM TO ASTM A-501.

SHOP COAT SHALL BE RUST INHIBITING RED OXIDE, RED LEAD OR LEAD CHROMATE OR EQUAL. IT IS THE INTENT TO PERMIT THE USE OF THE FABRICATORS STANDARD PRIME COATING.

ASPHALT BASED COATING IS NOT PERMITTED.

CONCRETE FOR SETTING FENCE AND GUARD RAIL POSTS AND SETTING AND FILLING OF SIGN AND GUARD POSTS SHALL BE PORTLAND CEMENT COMPLYING WITH ASTM C-150, AGGREGATES COMPLYING WITH ASTM C-33, AND CLEAN WATER. MIX MATERIALS TO OBTAIN CONCRETE WITH A MINIMUM 28 DAY COMPRESSIVE STRENGTH OF 2500 PSI, USING AT LEAST 4 SACKS OF CEMENT PER CU. YD., 1" MAXIMUM SIZE AGGREGATES, MAXIMUM 3" SLUMP, AND 2% TO 4% ENTRAINED AIR. PREPARE TO CONFORM TO ASTM C-94

MISCELLANEOUS NOTES

THE CONTRACTOR IS CAUTIONED TO VISIT THE SITE AND FAMILIARIZE HIMSELF WITH THE PROJECT PRIOR TO BIDDING.

THE ENGINEER HAS ATTEMPTED TO LOCATE EXISTING STRUCTURES AND EXISTING UTILITIES IN THE PROJECT AREA. IT IS THE CONTRACTOR'S RESPONSIBILITY TO DETERMINE THE EXACT LOCATIONS OF THESE STRUCTURES OR UTILITIES AND TO DETERMINE IF OTHER STRUCTURES OR UTILITIES WILL BE ENCOUNTERED DURING THE COURSE OF THE WORK. THE CONTRACTOR SHALL TAKE WHATEVER STEPS NECESSARY TO PROVIDE FOR THEIR PROTECTION AND RELOCATION OF UTILITIES IN CONFLICT WITH NEW CONSTRUCTION BY APPROPRIATE UTILITY COMPANY.

THE CONTRACTOR SHALL PLACE AND MAINTAIN ADEQUATE BARRICADES, CONSTRUCTION SIGNS, FLASHING LIGHTS, TORCHES, RED LANTERNS AND GUARDS DURING PROGRESS OF CONSTRUCTION WORK IN ACCORDANCE WITH STATE STANDARDS AND UNTIL IT IS SAFE FOR BOTH PEDESTRIAN AND VEHICULAR TRAFFIC.

CONTRACTOR IS RESPONSIBLE FOR REPLACING EXISTING SURROUNDINGS (I.E., ASPHALT, SIDEWALKS, CURBS, ETC.) THAT ARE DAMAGED DURING CONSTRUCTION. REPLACEMENT SHALL MATCH EXISTING.

ALL SITE WORK MATERIALS AND CONSTRUCTION METHODS SHALL BE IN ACCORDANCE WITH THE LATEST EDITION OF THE FLORIDA DEPARTMENT OF TRANSPORTATION STANDARD SPECIFICATIONS.

CONTRACTOR SHALL HAVE ALL PERMITS PRIOR TO CONSTRUCTION IN WETLANDS, COUNTY RIGHT OF WAY, ETC.

CONSTRUCTION PLANS ARE BASED ON FIELD SURVEY AND OTHER DATA AS SHOWN. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FIELD VERIFY ALL LOCATIONS OF NEW AND EXISTING CONNECTIONS NECESSARY TO COMPLETE THE INTENT OF THE PLANS. IN THE EVENT THERE IS A CONFLICT DUE TO UNFORESEEN OBSTRUCTIONS OR SHORT FALLS TO CONNECTIONS (WHICH DOES NOT MEET THE INTENT OF THE CONSTRUCTION PLANS), THE CONTRACTOR SHALL CONTACT THE ENGINEER IMMEDIATELY FOR DIRECTION. THE CONTRACTOR SHALL RELOCATE OR REMOVE OBSTACLES AS DIRECTED BY OWNER.

CONCRETE SIDEWALKS, CURBS, CURB AND GUTTER, SIDEWALKS, CONCRETE PAVING, ETC. SCHEDULE APPLIES TO SITE WORK ONLY. SEE ARCHITECT'S SPECIFICATIONS FOR FOUNDATION/BUILDING TESTING.

CONCRETE FOR SITE WORK INCLUDES BUT IS NOT LIMITED TO CURB, CURB & GUTTER, SIDEWALKS, CONCRETE PAVING, ETC. SCHEDULE APPLIES TO SITE WORK ONLY. SEE ARCHITECT'S SPECIFICATIONS FOR FOUNDATION/BUILDING TESTING.

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Addendum #2

Mosley Softball Fieldhouse

JRA Commission. 25871 CA/BC

Bay District Schools
1311 Balboa Avenue
Panama City, Florida 32401

JRA Architects, Inc.
2211 Navy Blvd- Suite 100
Panama City, Florida 32408

Date of Issue of addendum: **April 17, 2026**

The changes herewith form part of the Construction Documents and modify the original “Construction Documents” dated April 3, 2026.

This Addendum consists of **1** page(s), **1** attachment(s) and **2** revised plan sheet(s) attached and as referenced herein.

ITEM 2.1

Drawings:

Refer to **Drawings sheet A1.1 Architectural Floor Plan** – The hollow cells of the 8” CMU walls are to be filled with spray foam insulation as noted on the **Architectural wall types** on the index sheet.

ITEM 2.2

Geotech Report:

Refer to **Attachment “A” - NOVA Geotechnical Engineering Report** dated January 20, 2026.

ITEM 2.3

Drawings:

Replace **Drawings sheets P1.1 Plumbing New work Floor Plans and P2.1 Plumbing Riser Diagrams** from the contract documents with the Attached Drawing Sheets P1.1 & P2.1 with a revision date of 4/17/26.

END OF ADDENDUM #2

Attachment "A"

GEOTECHNICAL ENGINEERING REPORT



MOSLEY HS SOFTBALL FIELDHOUSE
Lynn Haven, Bay County, Florida

PREPARED FOR:

JRA ARCHITECTS, INC.
2211 Thomas Drive, Suite 100
Panama City Beach, Florida

NOVA Project Number: 10111-2026005

March 6, 2026





March 6, 2026

Mr. Dave Vincent, AIA, President
JRA ARCHITECTS, INC.
2211 Thomas Drive, Suite 100
Panama City Beach, Florida

Subject: Geotechnical Engineering Report
MOSLEY HS SOFTBALL FIELDHOUSE
Lynn Haven, Bay County, Florida
NOVA Project Number 10111-2026005

Dear Mr. Vincent:

NOVA ENGINEERING AND ENVIRONMENTAL LLC (NOVA) has completed the authorized subsurface exploration and geotechnical engineering evaluation for the proposed site improvements located in Lynn Haven, Bay County, Florida. Our services were performed in general accordance with NOVA Proposal Number 10111-2026005, dated January 26th, 2026. This report briefly discusses our understanding of the project at the time of the subsurface exploration, describes the geotechnical consulting services provided by NOVA, and presents our findings, conclusions, and recommendations.

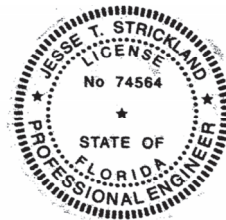
We appreciate your selection of NOVA and the opportunity to be of service on this project. If you have any questions, or if we may be of further assistance, please do not hesitate to contact us.

Sincerely,
NOVA ENGINEERING AND ENVIRONMENTAL, LLC

Michael R. Keramidis
Staff Engineer

Daniel C. Brahana, P.E. (Georgia)
Geotechnical Service Line Leader

Jesse T. Strickland, P.E.
Senior Engineer
Florida Registration No. 74564



This item has been electronically signed and sealed by Jesse T. Strickland, P.E., using a Digital Signature. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.

Digitally signed
by jesse t
strickland

Date: 2026.03.06
15:28:55 -05'00'

Copies Submitted: Addressee (electronic)

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APPENDICES

Appendix A – Figures and Maps

Appendix B – Subsurface Data

Appendix C – Laboratory Test Data

Appendix D – Support Documents

1.0 INTRODUCTION

Our services for this project were performed as described in our Proposal Number 10111-2026005, authorized by the Client on January 28th, 2026. The primary objectives were to perform a geotechnical exploration within the proposed construction areas of the project site and to assess these findings as they relate to geotechnical aspects of the planned site development. The authorized geotechnical engineering services included a site reconnaissance, soil test borings and sampling, engineering evaluation of the field and laboratory data, and the preparation of this report. As authorized in the above-mentioned proposal, this geotechnical report includes:

- A description of the site, fieldwork, laboratory testing and general soil conditions encountered, together with a Boring Location Plan, and individual Test Boring Records.
- Site preparation considerations that include geotechnical discussions regarding site stripping and subgrade preparation and engineered fill/backfill placement.
- Recommendations for controlling groundwater and/or run-off during construction.
- Shallow foundation system recommendations for the proposed structures, including allowable foundation capacities, recommended bearing depths, and installation considerations
- Slab-on-grade construction considerations based on the geotechnical findings, including the need for a sub-slab vapor barrier or a capillary barrier.
- Geotechnical soil input parameters for SMS design.
- Suitability of on-site soils for re-use as structural fill and backfill and the criteria for suitable fill materials.
- Recommended quality control measures (i.e., sampling, testing, and inspection requirements) for site grading and foundation construction operations.

The assessment of the presence of wetlands, floodplains, or water classified as state waters was beyond the scope of this exploration. Additionally, the assessment of site environmental conditions, including the detection of pollutants in the soil, rock, or groundwater or a site-specific seismic and/or karst-related study are also beyond the scope of this geotechnical exploration and evaluation. If requested, NOVA can provide these services under a supplemental study at a later date.

2.0 PROJECT INFORMATION

Our understanding of this project is based on discussions with the Client, a review of the provided site plan, site reconnaissance during the boring layout and testing process, and our experience with similar projects.

2.1 NAME AND LOCATION OF PROJECT

The +/- 1/2-acre Subject Property (*Bay County Parcel ID# 11800-020-000*) is located at 501 Mosley Drive, in Lynn Haven, Bay County, Florida. The location of the Subject Property (project site) is indicated on the Site Location Map included in Appendix A.

2.2 PROJECT SITE

At the time of our services, the project site was an existing school facility, with the specific area of testing consisting of a sports field complex, with surface conditions consisting primarily of short grasses. The surrounding area is generally developed with a softball field to the southwest, a baseball field to the northeast and short grass fields to the northwest and southeast. The site topography was observed to be generally flat. Based on a review of ground surface elevation data obtained from publicly available GIS-database, the existing ground surface elevation is reported to be on the order of approximately EL +36 feet Earth Gravitational Model of 1996 (EGM96). EGM96 is a global ellipsoidal model used to approximate the shape of the Earth and should be considered as approximate.

2.3 PROPOSED DEVELOPMENT

NOVA understands the project includes the construction of an approximate 2,600 ft² single-story fieldhouse structure, and an associated stormwater management system (SMS) to treat and dispose of stormwater runoff related with the site improvements. The structure is anticipated to be of CMU construction with light gauge metal roofs trusses with a slab-on-grade and supported by a conventional shallow foundation system. The SMS is anticipated to be desired to consist of a conventional dry retention basin.

Maximum Loads & Site Grading

Final structural loading information was not available from the Design Team at the time of this report. We have therefore assumed that maximum loadings will not exceed 1 to 2 kips per linear foot for continuous load bearing wall footings and 40 kips for isolated column footings. Finished grades are anticipated to match existing site grades, with any cut or fill limited to 2 feet or less. The SMS basin is anticipated to be 3 feet or less in depth relative to existing site grades.

3.0 SUBSURFACE EXPLORATION

3.1 AREA GEOLOGY

The subject site is located in Bay County, and according to the United States Geological Survey (USGS), within the Gulf Coastal Plain which is separated from the Florida Platform by geologic structures known as the Gulf Trough and Apalachicola Embayment. These structures formed a bathymetric and environmental barrier from the earliest Eocene or earliest Oligocene periods into the Miocene. This physiographic region is generally underlain by undifferentiated sediments deposited during the Quaternary period. These sediments typically consist of siliciclastics (sand), organics and freshwater carbonates. These soils are highly permeable and form the Sand and Gravel Aquifer of the surficial aquifer system. Surficial soils in the region are primarily siliciclastic sediments deposited in response to the renewed uplift and erosion in the Appalachian highlands to the north and sea-level fluctuations. The extent and type of deposit is influenced by numerous factors, including mineral composition of the parent rock and meteorological events.

3.2 FIELD EXPLORATION

Our subsurface exploration was conducted on February 5th and February 6th, 2026, and included performing:

- One 50-foot-deep SPT boring and one 20-foot-deep SPT boring at the locations provided by the Client within the footprint of the proposed structure (designated as B-1 & B-2, respectively, in the Appendix).
- Two hand auger borings at the locations provided by the Client, and collection of one bulk sample from the top 3 feet within the footprint of the proposed SMS basin (S-1 & S-2).

The boring and test locations were established in the field by NOVA personnel using a handheld GPS device and by estimating distances and angles from site landmarks. Prior to initiating field testing, underground utilities were marked by the state utility locate service (811, or Sunshine One-Call). The approximate test locations are shown in the Boring Location Plan provided in Appendix B. If increased accuracy is desired by the Client, test locations and elevations may be surveyed.

The Test Boring Records in Appendix B show the Standard Penetration Test (SPT) resistances, or “N-values”, for the structure borings and present the soil conditions encountered in all of the borings. These records represent our interpretation of the subsurface conditions based on the field exploration data, visual examination of the split-barrel samples, laboratory test data, and generally accepted geotechnical

engineering practices. The stratification lines and depth designations represent approximate boundaries between various subsurface strata. Actual transitions between materials may be gradual.

The groundwater levels reported on the Test Boring Records represent measurements made at the completion of each test boring, following a suitable stabilization period. The test borings were subsequently backfilled with soil cuttings from the drilling process for safety concerns.

SPT Borings

The SPT borings were performed using the guidelines of ASTM Designation D-1586, "Penetration Test and Split-Barrel Sampling of Soils". A mud-rotary drilling process was used to advance the borings once groundwater was encountered. At regular intervals, soil samples were obtained with a standard 1.4-inch I.D., 2.0-inch O.D., split-tube sampler. The sampler was first seated six inches and then driven an additional foot with blows of a 140-pound safety-hammer falling 30 inches. The number of hammer blows required to drive the sampler the final foot is designated the "Penetration Resistance". Representative portions of the soil samples, obtained from the sampler, were placed in sealed containers and transported to our laboratory for further evaluation and laboratory testing.

Auger Borings

The auger borings were performed using the guidelines of ASTM Designation D-1452, "Soil Exploration and Sampling by Auger Borings". A manually advanced 3¼-inch diameter orchard-type auger was utilized with disturbed samples acquired continuously for the full depth of the boring. Representative portions of the soil samples, obtained from the sampler, were placed in sealed containers and transported to our laboratory for further evaluation and laboratory testing.

3.3 LABORATORY TESTING

Following completion of the field work, soil and rock samples obtained in the field were returned to our office for classification and laboratory testing assignment. These tests included the following:

- Moisture Content
- Fines Content
- Organic Content
- Re-molded Falling Head Permeability

The purpose of the testing program was to classify the subsurface materials relative to the Unified Classification System and to determine various physical characteristics of the soils tested. The results of the laboratory testing are in Appendix C.

3.4 SUBSURFACE CONDITIONS

The following paragraphs provide generalized descriptions of the subsurface profiles and soil conditions encountered within the test borings conducted during this exploration.

SPT Boring

The SPT test borings generally encountered loose to medium dense slightly silty fine sands to silty fine sands (USCS classifications of SP-SM and SM) to the maximum depths explored ranging from approximately 20 to 50 feet BEG. Standard Penetration Test (SPT) resistance values (“N”-values) generally ranged from 4 to 12 blows-per-foot (bpf) to a depth of 10 feet BEG and from 11 to 22 bpf until the maximum termination depth of approximately 50 feet BEG.

Hand Auger Borings

The hand auger test borings generally encountered mixed strata of slightly silty fine sands to silty fine sands (SP-SM and SM) to the maximum depths explored of approximately 4 feet BEG. We note that the hand auger borings were terminated prior to the planned termination depth due to groundwater intrusion causing cave-in of the boreholes.

Groundwater Conditions

Groundwater in the Bay County, Florida area typically occurs as an unconfined aquifer condition. Consequently, the groundwater table is expected to be a subdued replica of the original surface topography. Recharge is provided by the infiltration of rainfall and surface water through the soil overburden. More permeable zones in the soil matrix can affect groundwater conditions. Groundwater levels vary with changes in season and rainfall, construction activity, surface water runoff, and other site-specific factors. Groundwater levels in the Bay County area are typically lowest in the late fall to winter and highest in the early spring to mid-summer with annual groundwater fluctuations by seasonal rainfall; consequently, the water table may vary at times.

A stabilized groundwater table was encountered in the test borings at depths ranging from approximately 2 feet to 3 feet BEG at the time of our final field exploration, which occurred during a period of relatively normal seasonal rainfall. Based on comparisons of current annual monthly rainfall data to historical rainfall data extending back 50+ years in time, groundwater levels encountered during our subsurface exploration presented herein, and a review of published historical soils and groundwater in the project vicinity, we estimate that the normal permanent seasonal high groundwater (SHGW) table for this site will occur within 1-foot of the natural ground surface elevation during the wet season.

4.0 GEOTECHNICAL ASSESSMENT

The following assessment is based on our understanding of the proposed construction, our site observations, our evaluation and interpretation of the field data obtained during this exploration, our experience with similar subsurface conditions, and generally accepted geotechnical engineering principles and practices.

Based on the results of the test borings, the encountered subsurface conditions appear to be adaptable for supporting the proposed construction utilizing conventional shallow foundation systems, provided that the recommendations outlined in the following sections are appropriately implemented. However, due to the relatively near-surface groundwater levels reported at the site and encountered during the subsurface exploration presented herein, we anticipate a wet detention system will be required for the proposed SMS basin.

Subsurface conditions in unexplored locations can and will vary from those encountered at the boring locations considered and discussed herein. If such variations are noted during construction, or if project development plans are changed, we request the opportunity to review the changes and amend our recommendations, if necessary.

The following sections present our recommendations for site preparation and grading, and for the design of the proposed shallow foundation system, and the SMS.

5.0 RECOMMENDATIONS

5.1 SITE PREPARATION

Prior to proceeding with construction, all topsoil and vegetation, and any other deleterious non-soil materials found to be present should be stripped from the proposed construction areas). Clean topsoil may be stockpiled and subsequently re-used in landscaped areas to receive sod as a “finishing layer”. Debris-laden materials should be excavated, transported, and disposed of off-site in accordance with appropriate solid waste rules and regulations. Any existing utility locations should be reviewed to assess their impact on the proposed construction and relocated/grouted in-place as appropriate.

The site should be graded during construction to maintain positive drainage away from the construction areas, to prevent ponding of stormwater on the site during and shortly following significant rain events. The construction areas should be sealed and crowned with a smooth roller to minimize ponding water from storm events at the end of each day of work.

The soils exposed at the stripped grade elevation should be compacted to a minimum soil density of at least 95 percent of the maximum dry density as determined by the Modified Proctor test method (ASTM D-1557). The upper 12 inches of soil beneath all footing excavation areas should be compacted to at least 98 percent.

NOVA should observe the compaction (i.e. proofrolling) of the subgrade to locate soft, weak, or excessively wet fill or existing soils present at the time of construction. Any unstable materials observed during the evaluation and compaction operations should be undercut and replaced with structural fill or stabilized in-place by scarifying and re-densifying. Actual remedial recommendations can best be determined by the geotechnical engineer in the field at the time of construction.

5.2 EXCAVATION

Excavations greater than five feet deep (such as for deeper foundations and underground utilities) should be sloped or shored in accordance with local, state, and federal regulations, including OSHA (29CFR Part 1926), excavation safety standards. It should be noted that the Contractor is solely responsible for site safety. This information is provided only as a service and under no circumstances should NOVA be assumed to be responsible for construction site safety. Each excavation should be observed and classified by an OSHA-competent person. All excavations below the groundwater level are classified as OSHA Class C soils for excavation purposes.

5.3 GROUNDWATER CONTROL

A stabilized groundwater table was encountered in the test borings at depths ranging from approximately 2 feet to 3 feet BEG at the time of our final field exploration, which occurred during a period of relatively normal seasonal rainfall. We recommend that measures be taken to reduce infiltration of water into the building foundation areas as recommended in *Section 5.4 – Drainage Considerations*.

Maintaining proper grades (i.e., positive drainage paths) during the construction phase of this project will be critical to avoid the development of “bird baths” within the proposed structure footprint area, which would degrade the underlying silty fine sand soils.

Additionally, the time frame that excavations needed to install building foundations and retaining walls remain open to inclement weather should be kept as short as practical, as water ponding in these excavations will degrade the underlying soil profile which could subsequently require remediation including possibly over-excavating pumping or otherwise overly wet soils. Sheet flowing stormwater exiting the overall site should be prevented from entering these excavations, and a pump system should be engaged immediately following the passing of rain events to minimize the time that standing water would be ponding on exposed soils.

Should elevated groundwater conditions be encountered during the earthwork phase of this development, most likely localized dewatering efforts (e.g., construction ditches, temporary sumps, etc.) will suffice to allow for earthwork operations to be performed in the dry. Given the anticipated fill heights of 3 feet above existing grades within the low-lying areas of the site, permanent dewatering measures are not anticipated as being necessary for this development

Temporary Dewatering: Design of a temporary dewatering system is usually the responsibility of the contractor. However, based on our experience with similar conditions, we anticipate that a well point dewatering system could potentially be necessary to properly control groundwater if deeper excavations are required. Since well point system construction is partially dependent on the technique and experience of the contractor, we believe the system should only be installed by a contractor with a minimum of 5 years of experience in dewatering system design and installation. Design flexibility should be allowed for the specialty contractor to choose the most appropriate dewatering system, including the well depths and spacing.

At the time of construction, groundwater must be lowered and continuously maintained at a minimum depth of 2 feet below the desired working elevation to permit subgrade preparation and foundation excavation and construction. The dewatering system should be installed and operational prior to excavation beneath the water table. The

dewatering system should also remain in continuous operation until the foundation concrete installation is complete.

Although dewatered, the subgrade will remain saturated and susceptible to damage caused by construction traffic. Undercutting, stabilization, and replacement of unstable soils should be assumed to be necessary. As previously noted, groundwater levels are subject to seasonal, climatic, tidal and other variations and may be different at other times and locations. The extent and nature of any dewatering required during construction will be dependent on the actual groundwater conditions prevalent at the time of construction and the effectiveness of construction drainage to prevent run-off into open excavations.

5.4 DRAINAGE CONSIDERATIONS

Soil strength and settlement potential is highly dependent upon the moisture condition of the supportive soil. Soil characteristics can change dramatically when moisture conditions change. As such, building pads, pavements, structures and surrounding grades should be properly designed and constructed to properly control water (surface and subsurface). Building pads should be designed to shed surface water prior to building construction. Grades surrounding structures should be adequately sloped away from the structure to promote positive drainage and prevent water from ponding near or against the structure. Swales and/or storm drainage structures should be constructed to collect and remove all surface water run-off. All roof drain downspouts should be connected to drain leaders that are properly daylighted or connected to storm drainage structures such that water is removed from structural areas. Interior and/or exterior foundation drains, if provided, should be installed to properly protect foundations from changing moisture conditions.

5.5 FILL PLACEMENT

Fill Suitability

Fill materials should be relatively clean sands with less than 20 percent fines (material passing the No. 200 sieve) and a Plasticity Index (PI) of less than 15, and free of non-soil materials and rock fragments larger than 3 inches in diameter. We note that soils with fines contents between approximately 15 and 20 percent will require strict moisture control at the time of placement and the Contractor should be prepared for difficulties during placement and compaction operations due to their moisture sensitivity.

Prior to construction, bulk samples of all proposed fill materials (both native and import) should be laboratory tested to confirm their suitability. Based on visual examination and limited laboratory soil testing results, the in-situ soils encountered

during this exploration typically consisted of slightly silty fine sands and silty fine sands (SP-SM and SM) that should be suitable for re-use as fill or backfill material, as laboratory testing indicated fines contents to range from approximately 7 to 18 percent.

We recommend that stockpiles of all materials planned for re-use be sealed as they are excavated to prevent (to the greatest extent practical) the intrusion of moisture into the core of the soil stockpile(s) during significant rain events prior to their potential re-use as fill and/or backfill soils.

Topsoil can be wasted in architectural areas to receive sod as a “finishing layer”. Organic and/or debris-laden material is not suitable for re-use as structural fill and should be excavated, transported, and disposed of off-site in accordance with appropriate solid waste rules and regulations.

Soil Compaction

All structural fill should be placed in thin, horizontal loose lifts (maximum 12-inch) and compacted to a minimum soil density of at least 95 percent of the Modified Proctor maximum dry density (ASTM D-1557). The upper 12 inches of soil beneath all footing excavation areas should be compacted to at least 98 percent. In confined areas, such as utility trenches, portable compaction equipment and thinner fill lifts (3 to 4 inches) may be necessary.

Fill materials used in structural areas should have a target maximum dry density of at least 95 pounds per cubic foot (pcf). If lighter weight fill materials are used, the NOVA geotechnical engineer should be consulted to assess the impact on design recommendations.

Soil moisture content should be maintained within 3 percent of the optimum moisture content. We recommend that the grading contractor have equipment on site during earthwork for both drying and wetting fill soils. Moisture control may be difficult during rainy weather. Soils excavated from below the groundwater table will likely require significant efforts to achieve acceptable moisture contents prior to re-use as fill.

Filling operations should be observed by a NOVA soils technician, who can confirm suitability of material used and uniformity and appropriateness of compaction efforts. The technician can also document compliance with the specifications by performing field density tests using thin-walled tube, nuclear, or sand cone testing methods (ASTM D-2937, D-6938, or D-1556, respectively). One test per 2,500 square feet in structure areas should be performed at the stripped subgrade elevation as well as in each lift of fill, with test locations well distributed throughout construction footprint. When filling in small areas, at least one test per day per area should be performed. One test at

conventional spread foundations and one test per 50 linear feet of continuous strip foundations are also recommended.

5.6 SHALLOW FOUNDATIONS

Design: After the recommended site and subgrade preparation and fill placement has been completed, it is our opinion that conventional shallow foundations can be used to support the proposed structure. Foundations bearing on densified native in-situ soils, and/or properly placed and compacted structural fill, as recommended in this report, may be designed employing a maximum allowable soil bearing pressure of **2,000 pounds per square foot (psf)**.

We recommend a value of 0.35 can be employed as the coefficient of friction (sliding resistance) between foundations and the underlying residual or fill soils. Footings should be a minimum of 24 inches in width for ease of construction and to reduce the possibility of localized shear failures. Isolated exterior and interior footing bottoms should be established at least 18 inches below finished surrounding exterior grades. When utilizing a post-tensioned monolithic slab-on-grade design, exterior and interior footing bottoms should be established a minimum of 12 inches below adjacent finished grades.

Settlement: Settlements for conventional foundations bearing on improved subgrade soils were assessed using SPT values to estimate elastic modulus, based on published correlations and previous NOVA experience. We note that the settlements presented are based on a subsoil profile deemed representative of the subsurface conditions encountered in the test borings. Conditions may be better or worse in other areas; however, we believe the estimated settlements stated herein are reasonable, but if subsurface conditions at the time of construction are determined to be different from those described herein, then NOVA should be retained to evaluate the differing conditions.

Based on the assumed structural loadings, the soil bearing capacity provided above, the presumed foundation elevations as discussed above, and successful completion of the site preparations provided herein, we expect residual primary total settlement beneath individual foundations to be on the order of 1-inch or less.

The amount of differential settlement is difficult to predict because the subsurface and foundation loading conditions can vary considerably across the site. However, we anticipate residual differential settlement between adjacent foundations will be less than 1/2-inch. The final deflected shape of the structure will be dependent on actual foundation locations and loading.

Construction: Foundation excavations should be evaluated by the NOVA geotechnical engineer prior to reinforcing steel placement to observe foundation subgrade preparation and confirm bearing pressure capacity. Foundation excavations should be level and free of debris, ponded water, mud, and loose, frozen, or water-softened soils. Concrete should be placed as soon as is practical after the foundation is excavated and the subgrade evaluated. Foundation concrete should not be placed on frozen or saturated soil.

If a foundation excavation remains open overnight, or if precipitation is imminent, a 3 to 4-inch thick "mud mat" of lean concrete should be placed in the bottom of the excavation to protect the bearing soils until reinforcing steel and concrete can be placed.

5.7 SLABS-ON-GRADE

General

The conditions exposed at subgrade levels will vary across the site and may include structural fill or densified in-situ soils. Slab(s)-on-grade may be adequately supported on these subgrade conditions subject to the recommendations in this report. The slab-on-grade should be jointed around columns and along walls to reduce cracking due to differential movement. An underdrain system is not necessary beneath the slab, provided that the slab is installed at least 2 feet above the seasonal high groundwater level. An impermeable vapor barrier is recommended beneath finished spaces to reduce dampness.

A coefficient of subgrade reaction (k) of 125 pci (psi per inch) may be used for conventional slab design where slabs bear upon subgrades prepared in accordance with previous recommendations. Once grading is completed, the subgrade can be exposed to adverse construction activities and weather conditions during the period of sub-slab utility installation. The subgrade should be well drained to prevent the accumulation of water. If the exposed subgrade becomes unstable, excessively wet or exhibits excessive rutting or pumping, the geotechnical engineer should be consulted.

5.8 STORMWATER MANAGEMENT SYSTEM

Based on the results of the SMS test borings, the subsurface conditions encountered beneath the proposed SMS site appear poorly suited for the construction of the desired dry retention basin. Due to the relatively near-surface groundwater levels encountered during our subsurface exploration presented herein and a review of published historical soils and groundwater in the project vicinity, we recommend a wet retention basin alternative is utilized for the site improvements. Recommended soil input parameters for the SMS basin design are presented in the table below:

| SMS Soil Design Parameters | |
|---|-----------------|
| Corresponding Soil Boring Depths from Boring S-2 | 0' – 3' |
| Estimated Depth to Confining Stratum, BEG | Below 10 feet |
| Measured Vertical Permeability Rate (k_v)* | 1 feet/day |
| Calculated Horizontal Permeability Rate (k_h)* | 2 feet/day |
| Measured In-Situ Infiltration Rate* | <0.1 inches/hr. |
| Measured Depth to Apparent Groundwater Table, BEG | 2 feet |
| Estimated Depth to Normal Permanent SHGW table, BEG | 1-foot |

* Factors of Safety have not been applied to the hydraulic conductivity and infiltration values.

General Considerations

The seasonal high groundwater level estimate provided in the table above is based on our experience with projects in this locale, the soil strata and groundwater levels encountered in our test borings, and a review of publicly available historical data. Should these estimates become critical to design, then as previously stated, we recommend the locations and associated ground surface elevations are determined by a licensed and registered land surveyor.

The actual exfiltration rate from the pond may be influenced by basin geometry, natural soil variability, in-situ depositional characteristics and soil density, retention volume, and groundwater mounding effects. Appropriate factors of safety should be incorporated into the design process. We note that NOVA performs remolded laboratory permeability testing using generally accepted practices of the local engineering community. These types of tests are the quickest and most economical for stormwater retention basin design. However, the user of this information is cautioned that the potential variability of results of these types of tests can be significant, and the reproducibility of results can vary by factors of up to 100 percent.

Also, the permeability rate measured by such tests may not be representative of the total effective aquifer thickness. Factors of safety can compensate for part of the inherent test limitations, but the designer must exercise judgment regarding final selection and applicability of provided soil design input parameters. Should the modeling analysis indicate marginally acceptable compliance with Water Management District design criteria, it may be advisable to perform more extensive and representative in-situ permeability testing by collecting “undisturbed” horizontal and vertical soil samples and/or installing grouted piezometers or wells for slug testing. NOVA can perform these field tests under separate scope & fee, if desired at a later date.

6.0 LIMITATIONS

The findings, conclusions and recommendations presented in this report represent our professional opinions concerning subsurface conditions at the site. The opinions presented are relative to the dates of our site work and should not be relied on to represent conditions at significantly later dates or at locations not explored. The opinions included herein are based on information provided to us, the data obtained at specific locations during the study and our experience. If additional information becomes available that might impact our geotechnical opinions, it will be necessary for NOVA to review the information, reassess the potential concerns, and re-evaluate our conclusions and recommendations.

Regardless of the thoroughness of a geotechnical exploration, there is the possibility that conditions between test locations will differ from those encountered at specific test locations, that conditions are not as anticipated by the designers and/or the contractors, or that either natural events or the construction process have altered the subsurface conditions. These variations are an inherent risk associated with subsurface conditions in this region and the approximate methods used to obtain the data. These variations may not be apparent until construction.

This report is intended for the sole use of **JRA ARCHITECTS, INC.** for the above noted project. The scope of work performed during this study may not satisfy other user's requirements. Use of this report or the findings, conclusions or recommendations by others will be at the sole risk of the user. NOVA is not responsible or liable for the interpretation by others of the data in this report, nor their conclusions, recommendations or opinions.

Our professional services have been performed, our findings obtained, our conclusions derived and our recommendations prepared in accordance with generally accepted geotechnical engineering principles and practices in the State of Florida. This warranty is in lieu of all other statements or warranties, either expressed or implied.

APPENDIX A

Figures and Maps



Project Location



PROJECT LOCATION MAP
Mosley HS Softball Fieldhouse
 Lynn Haven, Bay County, Florida
 NOVA Project Number 10111-2026005

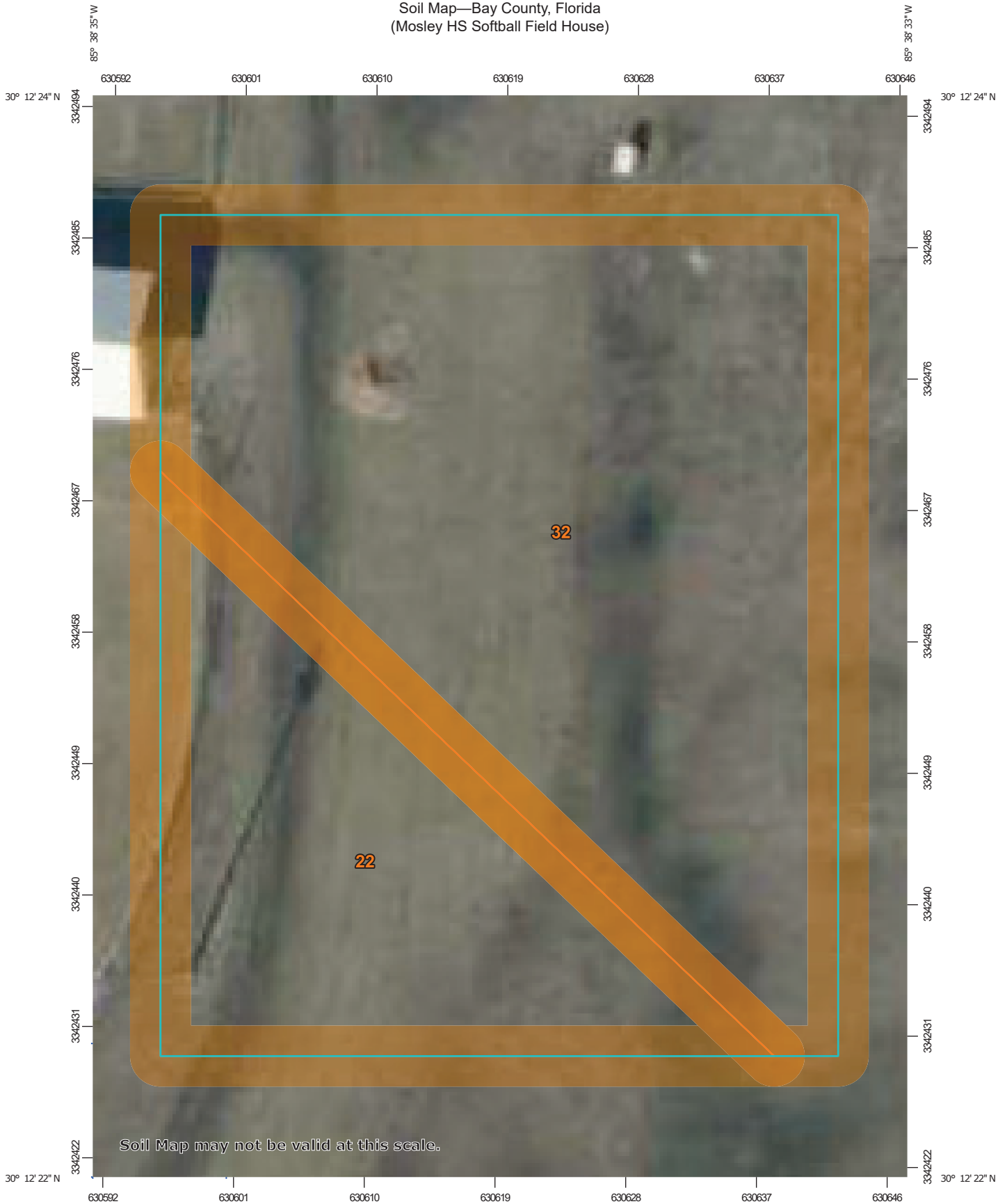
17612 Ashley Drive
 Panama City Beach, Florida 32413
 850.249.6682 ♦ 850.249.6683



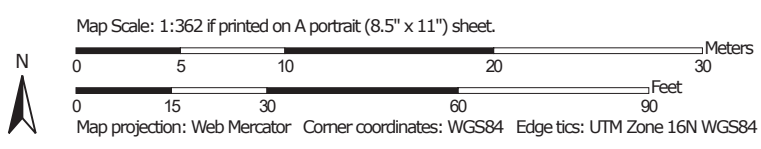
Base map provided by Google Earth

Scale: Not To Scale
 Date Drawn: February 10, 2026
 Drawn By: B. Hardtke
 Checked By: J. Strickland






























Soil Map—Bay County, Florida
(Mosley HS Softball Field House)



Soil Map may not be valid at this scale.



MAP LEGEND

-  Area of Interest (AOI)
-  Soil Map Unit Polygons
-  Soil Map Unit Lines
-  Soil Map Unit Points
- Special Point Features**
 -  Blowout
 -  Borrow Pit
 -  Clay Spot
 -  Closed Depression
 -  Gravel Pit
 -  Gravelly Spot
 -  Landfill
 -  Lava Flow
 -  Marsh or swamp
 -  Mine or Quarry
 -  Miscellaneous Water
 -  Perennial Water
 -  Rock Outcrop
 -  Saline Spot
 -  Sandy Spot
 -  Severely Eroded Spot
 -  Sinkhole
 -  Slide or Slip
 -  Sodic Spot
- Water Features**
 -  Streams and Canals
- Transportation**
 -  Rails
 -  Interstate Highways
 -  US Routes
 -  Major Roads
 -  Local Roads
- Background**
 -  Aerial Photography
-  Spoil Area
-  Stony Spot
-  Very Stony Spot
-  Wet Spot
-  Other
-  Special Line Features

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Bay County, Florida
Survey Area Data: Version 25, Aug 27, 2025

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jan 10, 2024—Jan 20, 2024

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI |
|------------------------------------|-------------------------|--------------|----------------|
| 22 | Pamlico-Dorovan complex | 0.2 | 31.5% |
| 32 | Plummer sand | 0.5 | 68.5% |
| Totals for Area of Interest | | 0.7 | 100.0% |

Bay County, Florida

32—Plummer sand

Map Unit Setting

National map unit symbol: brv2

Landscape: Coastal plains

Elevation: 0 to 450 feet

Mean annual precipitation: 61 to 69 inches

Mean annual air temperature: 63 to 70 degrees F

Frost-free period: 252 to 282 days

Farmland classification: Not prime farmland

Map Unit Composition

Plummer and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Plummer

Setting

Landscape: Coastal plains

Landform: Flats on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Sandy and loamy marine deposits

Typical profile

A - 0 to 7 inches: sand

Eg - 7 to 48 inches: sand

Btg1 - 48 to 59 inches: sandy loam

Btg2 - 59 to 80 inches: sandy clay loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat):

Moderately high to high (0.60 to 2.00 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None

Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum: 4.0

Available water supply, 0 to 60 inches: Moderate (about 6.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: A/D

Ecological site: F152AY320FL - East Central Sandy Flat

Forage suitability group: Sandy soils on flats of mesic or hydric lowlands (G152AA141FL)

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G152AA141FL)

Hydric soil rating: Yes

Minor Components

Pelham, hydric

Percent of map unit: 4 percent

Landscape: Coastal plains

Landform: Flats on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Linear

Across-slope shape: Linear

Ecological site: F152AY335FL - East Central Sandy Flooded Flat

Other vegetative classification: Sandy over loamy soils on stream terraces, flood plains, or in depressions (G152AA245FL)

Hydric soil rating: Yes

Albany

Percent of map unit: 3 percent

Landscape: Coastal plains

Landform: Knolls on marine terraces, Rises on marine terraces, Flats on marine terraces

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex

Across-slope shape: Linear

Ecological site: F152AY320FL - East Central Sandy Flat

Other vegetative classification: Sandy soils on rises and knolls of mesic uplands (G152AA131FL)

Hydric soil rating: No

Rutlege

Percent of map unit: 3 percent

Landscape: Coastal plains

Landform: Depressions on marine terraces

Landform position (three-dimensional): Dip

Down-slope shape: Concave

Across-slope shape: Concave

Ecological site: F152AY350FL - East Central Sandy Lowland

Other vegetative classification: Sandy soils on stream terraces, flood plains, or in depressions (G152AA145FL)

Hydric soil rating: Yes

Pottsburg, hydric

Percent of map unit: 3 percent

Landscape: Coastal plains

Landform: Flats on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Ecological site: F152AY320FL - East Central Sandy Flat
Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G152AA141FL)
Hydric soil rating: Yes

Rains

Percent of map unit: 2 percent
Landscape: Coastal plains
Landform: Flats on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Ecological site: F152AY320FL - East Central Sandy Flat
Other vegetative classification: Loamy and clayey soils on flats of hydric or mesic lowlands (G152AA341FL)
Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Bay County, Florida
Survey Area Data: Version 25, Aug 27, 2025

Bay County, Florida

22—Pamlico-Dorovan complex

Map Unit Setting

National map unit symbol: brtq
Landscape: Coastal plains
Elevation: 0 to 450 feet
Mean annual precipitation: 61 to 69 inches
Mean annual air temperature: 63 to 70 degrees F
Frost-free period: 252 to 282 days
Farmland classification: Not prime farmland

Map Unit Composition

Pamlico and similar soils: 40 percent
Dorovan and similar soils: 35 percent
Minor components: 25 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Pamlico

Setting

Landscape: Coastal plains
Landform: Flood plains on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Concave
Parent material: Herbaceous organic material over sandy marine deposits

Typical profile

Oa - 0 to 32 inches: muck
2Cg - 32 to 72 inches: sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat):
Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: Frequent
Frequency of ponding: Frequent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: High (about 9.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7w
Hydrologic Soil Group: A/D
Forage suitability group: Organic soils in depressions and on flood plains (G152AA645FL)
Other vegetative classification: Organic soils in depressions and on flood plains (G152AA645FL)
Hydric soil rating: Yes

Description of Dorovan

Setting

Landscape: Coastal plains
Landform: Flood plains on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Organic material

Typical profile

Oa - 0 to 60 inches: muck
2Cg - 60 to 80 inches: sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat):
Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: Frequent
Frequency of ponding: Frequent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: Very high (about 22.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7w
Hydrologic Soil Group: B/D
Forage suitability group: Organic soils in depressions and on flood plains (G152AA645FL)
Other vegetative classification: Organic soils in depressions and on flood plains (G152AA645FL)
Hydric soil rating: Yes

Minor Components

Rutlege

Percent of map unit: 10 percent
Landscape: Coastal plains
Landform: Depressions on marine terraces

Landform position (three-dimensional): Dip
Down-slope shape: Concave
Across-slope shape: Concave
Other vegetative classification: Sandy soils on stream terraces, flood plains, or in depressions (G152AA145FL)
Hydric soil rating: Yes

Pantego

Percent of map unit: 3 percent
Landscape: Coastal plains
Landform: Depressions on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Concave
Across-slope shape: Concave
Other vegetative classification: Loamy and clayey soils on stream terraces, flood plains, or in depressions (G152AA345FL)
Hydric soil rating: Yes

Plummer

Percent of map unit: 3 percent
Landscape: Coastal plains
Landform: Flats on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G152AA141FL)
Hydric soil rating: Yes

Pottsburg, hydric

Percent of map unit: 3 percent
Landscape: Coastal plains
Landform: Flats on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G152AA141FL)
Hydric soil rating: Yes

Alapaha

Percent of map unit: 2 percent
Landscape: Coastal plains
Landform: Flats on marine terraces, Drainageways on marine terraces, Depressions on marine terraces
Landform position (three-dimensional): Talf, dip
Down-slope shape: Linear
Across-slope shape: Concave
Other vegetative classification: Sandy over loamy soils on stream terraces, flood plains, or in depressions (G152AA245FL)
Hydric soil rating: Yes

Rains

Percent of map unit: 2 percent

Landscape: Coastal plains
Landform: Flats on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Other vegetative classification: Loamy and clayey soils on flats of hydric or mesic lowlands (G152AA341FL)
Hydric soil rating: Yes

Pansey

Percent of map unit: 2 percent
Landscape: Coastal plains
Landform: Flats on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Other vegetative classification: Loamy and clayey soils on flats of hydric or mesic lowlands (G152AA341FL)
Hydric soil rating: Yes

Data Source Information

Soil Survey Area: Bay County, Florida
Survey Area Data: Version 25, Aug 27, 2025

APPENDIX B

Subsurface Data

BORING LOCATION PLAN



Keyboard shortcuts | Map data ©2026 Imagery ©2026 Airbus | 10 m | Terms



PREPARED BY
NOVA Engineering and Environmental, LLC
Kennesaw, GA

PROJECT
Name: Mosley HS Softball Fieldhouse
Number: 10111-2026005

LOCATION
30.206815, -85.643291
Lynn Haven, FL

SYMBOL KEY
● Test Boring
● Soil Boring

KEY TO SYMBOLS AND CLASSIFICATIONS

DRILLING SYMBOLS

| | |
|--------|--|
| | Standard Penetration Testing Sample |
| | Undisturbed Sample (UD) |
| | Auger without Sampling |
| | Rock Core Sample |
| | Standard Penetration Resistance (ASTM D1586) |
| | Dynamic Cone Penetrometer (DCP) Resistance |
| | Water Table at least 24 Hours after drilling |
| | Water Table 1 Hour or less after drilling |
| 50/2" | Number of Blows (50) to Drive the Spoon a Number of Inches (2) |
| NX, NQ | Core Barrel Sizes: 2½- and 2-Inch Diameter Rock Core, Respectively |
| REC | Percentage of Rock Core Recovered |
| RQD | Rock Quality Designation - Percentage of Recovered Core Segments 4 or more Inches Long |
| | Loss of Drilling Fluid |
| N/E | Not Encountered |
| N/M | Not Measured |
| | Boring Cave-in Depth |
| WOH | Weight of Hammer |

DRILLING PROCEDURES

Soil sampling and standard penetration testing performed in general accordance with ASTM D1586-18¹. The standard penetration resistance (N-value) is the number of blows of a 140-pound hammer falling 30 inches to drive a 2-inch O.D., 1.375-inch I.D. split-barrel sampler one foot. Core drilling performed in general accordance with ASTM D2113-14. The undisturbed sampling procedure is described by ASTM D1587-15. Unless other arrangements are made, NOVA will dispose of all soil and rock samples at the time of report submission.

| | | | | | |
|--|--------------------------------|--|--|--|--------------------------------|
| | Paving | | Well Graded Sand - SW | | Silt - ML |
| | Gravel / Graded Aggregate Base | | Silty Sand - SM | | Elastic Silt - MH |
| | Fill | | Clayey Sand - SC | | Low Plasticity Clay - CL |
| | Topsoil | | Poorly graded silty, clayey sand - SM/SC | | High Plasticity Clay - CH |
| | Alluvium | | Clayey Sand and Gravel - SC/GC | | Partially Weathered Rock (PWR) |
| | Poorly Graded Sand - SP | | Silty Sand and Gravel - SM/GM | | Rock |

CORRELATION OF PENETRATION RESISTANCE WITH RELATIVE DENSITY AND CONSISTENCY

| | <u>Number of Blows, "N"</u> | <u>Approximate Relative Density</u> |
|-------|-----------------------------|-------------------------------------|
| SANDS | 0 – 4 | Very Loose |
| | 5 – 10 | Loose |
| | 11 – 30 | Medium Dense |
| | 31 – 50 | Dense |
| | Over 50 | Very Dense |

| | <u>Number of Blows, "N"</u> | <u>Approximate Consistency</u> |
|-----------------------|-----------------------------|--------------------------------|
| SILTS and CLAYS | 0 – 2 | Very Soft |
| | 3 – 4 | Soft |
| | 5 – 8 | Firm |
| | 9 – 15 | Stiff |
| | 16 – 30 | Very Stiff |
| | 31 – 50 | Hard |
| | Over 50 | Very Hard |

SOIL CLASSIFICATION CHART

| | | | | |
|---|--|---|-------------|-----------------------|
| COARSE GRAINED SOILS | GRAVELS | Clean Gravel less than 5% fines | GW | Well graded gravel |
| | | | GP | Poorly graded gravel |
| | | Gravels with Fines more than 12% fines | GM | Silty gravel |
| | | | GC | Clayey gravel |
| | SANDS | Clean Sand less than 5% fines | SW | Well graded sand |
| | | | SP | Poorly graded sand |
| Sands with Fines more than 12% fines | | SM | Silty sand | |
| | | SC | Clayey sand | |
| FINE GRAINED SOILS | SILTS AND CLAYS Liquid Limit less than 50 | Inorganic | CL | Lean clay |
| | | | ML | Silt |
| | | Organic | OL | Organic clay and silt |
| | | | CH | Fat clay |
| | SILTS AND CLAYS Liquid Limit 50 or more | Inorganic | MH | Elastic silt |
| | | | OH | Organic clay and silt |
| HIGHLY ORGANIC SOILS | | Organic matter, dark color, organic odor | PT | Peat |

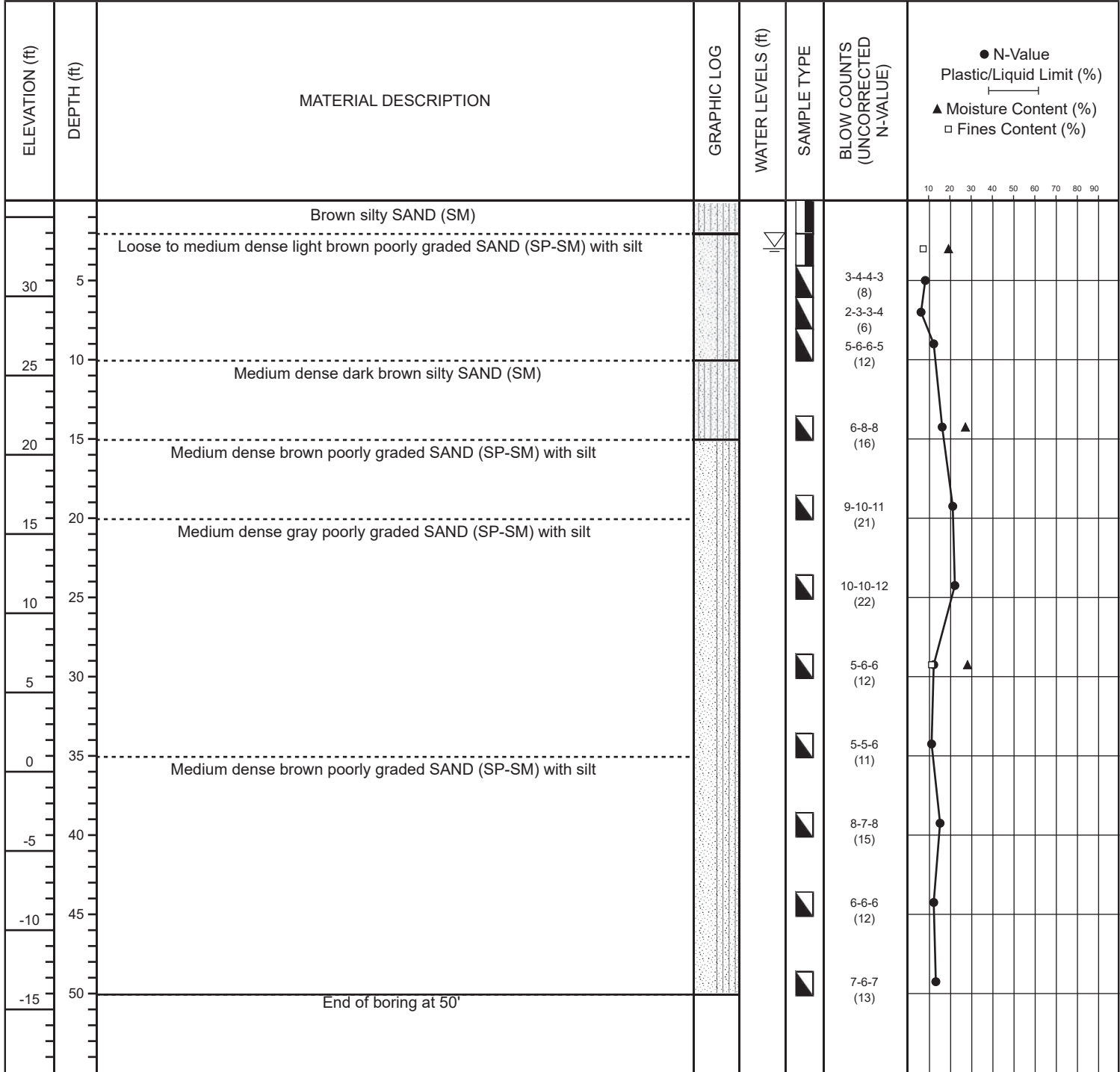
PARTICLE SIZE IDENTIFICATION

| | | |
|------------------------|--------|--------------------|
| GRAVELS | Coarse | ¾ inch to 3 inches |
| | Fine | No. 4 to ¾ inch |
| | | |
| SANDS | Coarse | No. 10 to No. 4 |
| | Medium | No. 40 to No. 10 |
| | Fine | No. 200 to No. 40 |
| | | |
| SILTS AND CLAYS | | Passing No. 200 |



TEST BORING RECORD B-1

PROJECT NAME Mosley HS Softball Fieldhouse **PROJECT NO.** 10111-2026005
CLIENT JRA Architects, Inc **LATITUDE** 30.20682
PROJECT LOCATION Lynn Haven, Bay County, Florida **LONGITUDE** -85.64300
LOCATION North side of building footprint **ELEVATION** 36' (EGM96)
DRILLER Watson's Drilling LLC **LOGGED BY** B. Hardtke
DRILLING METHOD Mud Rotary - Manual **% ENERGY** 60% **DATE** 02/05/2026
DEPTH TO-WATER ▽ INITIAL 3' ▼ AFTER 24 HOURS N/M ○ CAVING N/M

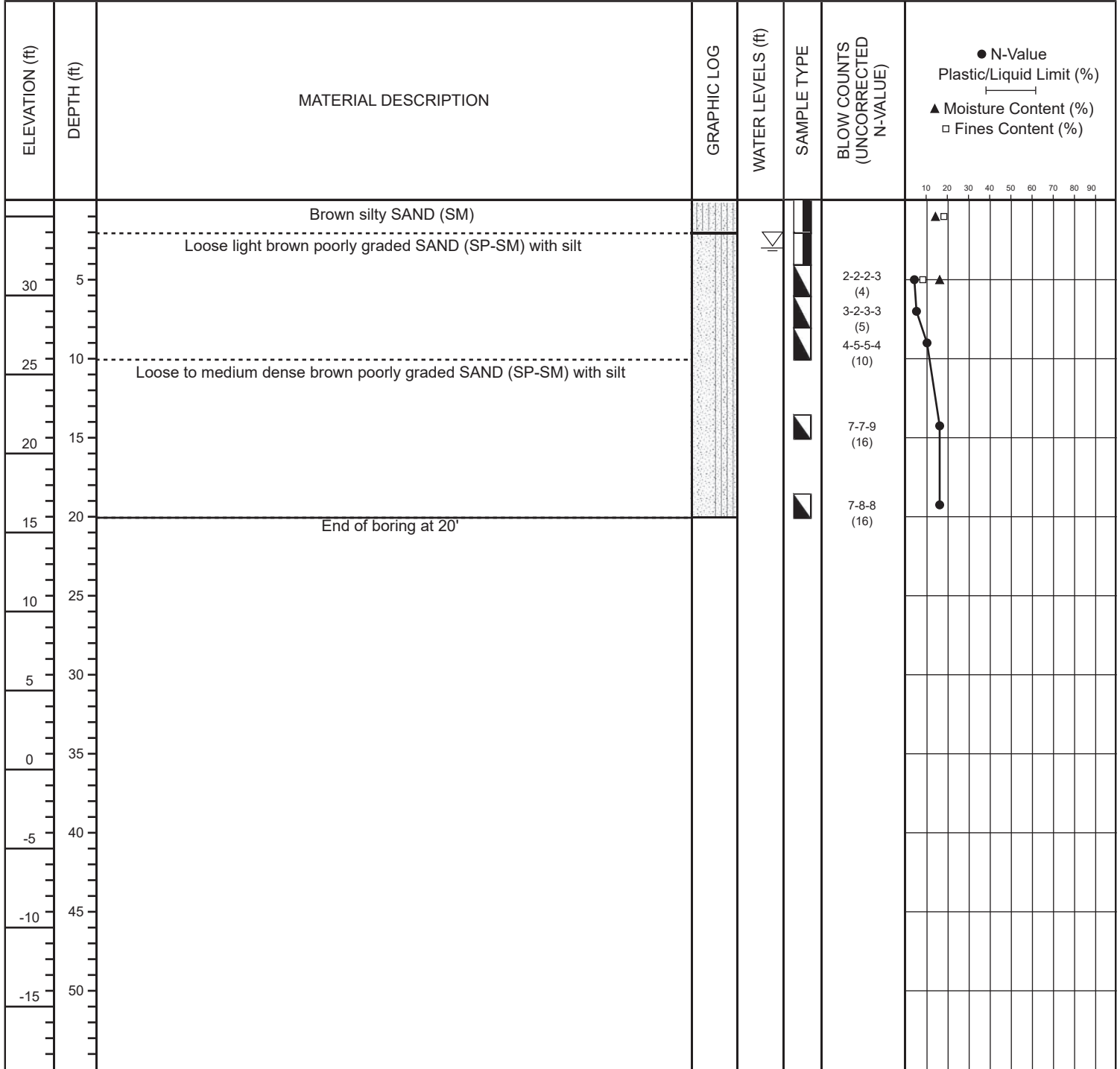


Notes: 1) Ground Surface Elevations were interpolated through Google Earth imagery and should be noted as approximate. 2) A manual hammer with rope and cathead was used for the SPT sampling and testing. 3) Hammer energy efficiency of 60% is a published reference value for manual safety hammers.



TEST BORING RECORD B-2

PROJECT NAME Mosley HS Softball Fieldhouse **PROJECT NO.** 10111-2026005
CLIENT JRA Architects, Inc **LATITUDE** 30.20671
PROJECT LOCATION Lynn Haven, Bay County, Florida **LONGITUDE** -85.64299
LOCATION South side of building footprint **ELEVATION** 36' (EGM96)
DRILLER Watson's Drilling LLC **LOGGED BY** B. Hardtke
DRILLING METHOD Mud Rotary - Manual **% ENERGY** 60% **DATE** 02/05/2026
DEPTH TO-WATER ▽ INITIAL 3' ▼ AFTER 24 HOURS N/M **CAVING** N/M



Notes: 1) Ground Surface Elevations were interpolated through Google Earth imagery and should be noted as approximate. 2) A manual hammer with rope and cathead was used for the SPT sampling and testing. 3) Hammer energy efficiency of 60% is a published reference value for manual safety hammers.



**SOIL BORING
RECORD
S-1**

PROJECT NAME Mosley HS Softball Fieldhouse **PROJECT NO.** 10111-2026005
CLIENT JRA Architects, Inc **LATITUDE** 30.20676
PROJECT LOCATION Lynn Haven, Bay County, Florida **LONGITUDE** -85.64293
LOCATION South side of pond footprint **ELEVATION** 36' (EGM96)
DRILLER B. Hardtke **LOGGED BY** B. Hardtke
DRILLING METHOD Hand Auger **DATE** 02/06/2026
DEPTH TO-WATER INITIAL 2' AFTER 24 HOURS N/M CAVING 3'

| ELEVATION (ft) | DEPTH (ft) | MATERIAL DESCRIPTION | GRAPHIC LOG | WATER LEVELS (ft) | SAMPLE TYPE | BLOW COUNTS (UNCORRECTED N-VALUE) | <ul style="list-style-type: none"> ● N-Value Plastic/Liquid Limit (%) ▲ Moisture Content (%) □ Fines Content (%) |
|----------------|------------|--|-------------|-------------------|-------------|-----------------------------------|--|
| | | Brown poorly graded SAND (SP-SM) with silt | | | | | |
| 35 | | Dark gray silty SAND (SM) | | | | | <div style="text-align: center;"> □▲ </div> |
| | | Light brown poorly graded SAND (SP-SM) with silt | | ▽ | | | |
| | | Collapsed at 3' | | | | | |

Notes: 1) Ground Surface Elevations were interpolated through Google Earth imagery and should be noted as approximate.

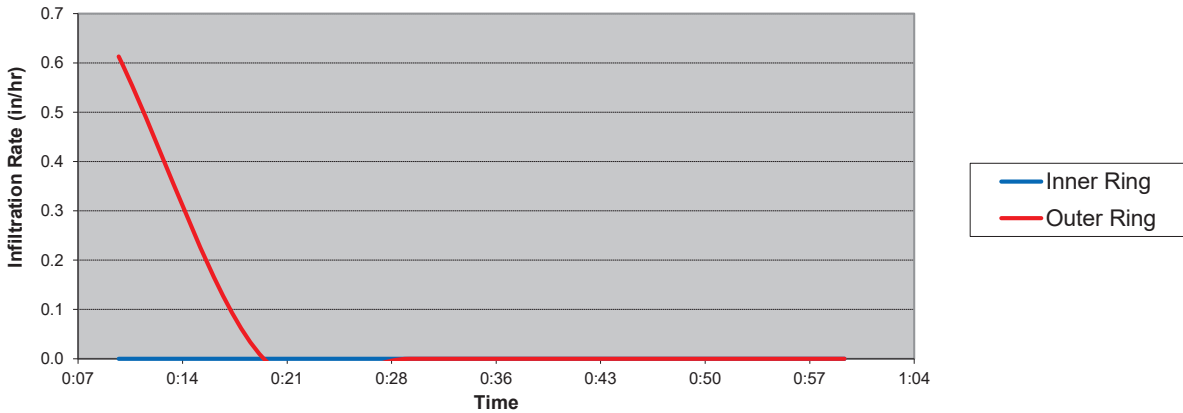
| | | |
|--------------------------|--|---------------------------------------|
| Project: | Mosley HS Softball Fieldhouse | Report of DRI - 1 (Boring S-1) |
| Project Location: | Lynn Haven, Bay County, Florida | |
| Project Number: | 10111-2025005 | |

| | | | | | |
|--------------------|------------------|--|--------------------|--------------------|--------------------------|
| Date(s) of Test | February 6, 2026 | Tested by | B. Hardtke | Weather | Sunny |
| Test Method | ASTM D 3385 | Logged by | B. Hardtke | Type of liquid | tap water |
| Area Inner Ring | 110.75 sq. in. | Checked by | J. Strickland | Liquid Temperature | 80 °F |
| Area Outer Ring | 447.69 sq. in. | See Auger Boring Record for Soil Profile | | Soil Temperature | 83 °F |
| Area Annular Space | 334.59 sq. in. | Approx. Elevation | 12 in. below grade | Location | Per Boring Location Plan |

INCREMENTAL INFILTRATION RATE vs. TOTAL ELAPSED TIME

| Time | Elapsed Time (minutes) | Inner Ring | | Outer Ring | | Comments |
|------|------------------------|--------------|---------------------------|--------------|---------------------------|----------|
| | | Volume (gal) | Infiltration Rate (In/hr) | Volume (gal) | Infiltration Rate (In/hr) | |
| 0:10 | 10 | 0.0 | 0.0 | 0.2 | 0.6 | |
| 0:20 | 10 | 0.0 | 0.0 | 0.0 | 0.0 | |
| 0:30 | 10 | 0.0 | 0.0 | 0.0 | 0.0 | |
| 0:40 | 10 | 0.0 | 0.0 | 0.0 | 0.0 | |
| 0:50 | 10 | 0.0 | 0.0 | 0.0 | 0.0 | |
| 1:00 | 10 | 0.0 | 0.0 | 0.0 | 0.0 | |
| | | | | | | |
| | | | | | | |
| | | | | | | |

Infiltration Rate



INFILTRATION RATE = 0 in/hr



Figure DRI-1



SOIL BORING RECORD S-2

PROJECT NAME Mosley HS Softball Fieldhouse **PROJECT NO.** 10111-2026005
CLIENT JRA Architects, Inc **LATITUDE** 30.20688
PROJECT LOCATION Lynn Haven, Bay County, Florida **LONGITUDE** -85.64292
LOCATION North side of pond footprint **ELEVATION** 36' (EGM96)
DRILLER B. Hardtke **LOGGED BY** B. Hardtke
DRILLING METHOD Hand Auger **DATE** 02/06/2026
DEPTH TO-WATER ▽ INITIAL 3' ▼ AFTER 24 HOURS N/M C CAVING 4'

| ELEVATION (ft) | DEPTH (ft) | MATERIAL DESCRIPTION | GRAPHIC LOG | WATER LEVELS (ft) | SAMPLE TYPE | BLOW COUNTS (UNCORRECTED N-VALUE) | ● N-Value Plastic/Liquid Limit (%) ▲ Moisture Content (%) □ Fines Content (%) |
|----------------|------------|--|-------------|-------------------|-------------|-----------------------------------|--|
| | | Brown poorly graded SAND (SP-SM) with silt | | | | | |
| | | Dark gray silty SAND (SM) | | | | | |
| 35 | | | | | | | |
| | | Light brown poorly graded SAND (SP-SM) with silt | | ▽ | | | □ ▲ |
| | | Collapsed at 4' | | | | | |

Notes: 1) Ground Surface Elevations were interpolated through Google Earth imagery and should be noted as approximate.

APPENDIX C

Laboratory Data

Laboratory Testing

Mosley HS Softball Fieldhouse
Lynn Haven, Bay County, Florida
NOVA Project Number 10111-2026005

Moisture Content

The moisture content is the ratio expressed as a percentage of the weight of water in a given mass of soil to the weight of the solid particles. This testing was conducted in general accordance with ASTM Designation D-2216. Six moisture content tests were performed in this study.

Fines Content

The percentage of fines passing through the No. 200 sieve is generally considered to represent the amount of silt and clay of the tested soil sample. The sieve analysis testing was conducted in general accordance with ASTM Designations D-6913 and D-1140. Six fines content tests were performed in this study.

Organic Content

The organic content is the ratio expressed as a percentage of the weight of organic material in a given mass of soil to the weight of the solid particles. This testing was conducted in general accordance with ASTM D-2974. Five organic content tests were performed in this study.

Remolded Falling Head Permeability Testing

A remolded falling head permeability test (ASTM D-5084) is a common laboratory test used to determine the hydraulic conductivity of fine-grained soils. The test involves the flow of water through a re-molded, fully saturated soil sample inside a rigid-wall permeameter connected to a standpipe of constant diameter. Before beginning the flow measurements, the soil sample is saturated, and the standpipe is filled with water to a given level. The test then starts by allowing the water to flow through the sample until the water in the standpipe reaches a lower limit. The time required for the water to flow from the upper to lower limit is recorded. One remolded permeability test was performed in this study.

SUMMARY OF CLASSIFICATION & INDEX TESTING

Mosley HS Softball Fieldhouse
Lynn Haven, Bay County, Florida
NOVA Project Number 10111-2026005

| Boring Number | Sample Depth (ft) | Natural Moisture (%) | Percent (%) Passing Sieve #200 | Percent Organic (%) | USCS Soil Classification |
|---------------|-------------------|----------------------|--------------------------------|---------------------|--------------------------|
| B-2 | 0 - 2 | 14 | 18 | 4 | SM |
| S-1 | 1 - 2 | 19 | 15 | 2 | SM |
| B-1 | 2 - 4 | 19 | 7 | N/A | SP-SM |
| S-2 | 3 - 4 | 19 | 10 | 1 | SP-SM |
| B-2 | 4 - 6 | 16 | 8 | 0 | SP-SM |
| B-1 | 28.5 - 30 | 28 | 11 | 1 | SP-SM |

PERMEABILITY, -200 SIEVE WASH, AND MOISTURE CONTENT

PROJECT: Mosley HS Softball Fieldhouse NOVA PROJECT #: 10111-2026005

DATE: 2/12/2026 ASSIGNED BY: J. Strickland TESTED BY: M. Keramidas

| | |
|------------------------------|-------|
| Sample LOCATION / BORING NO. | S-2 |
| Sample NUMBER / DEPTH | 0 - 3 |

| PERMEABILITY TESTING SUMMARY | | |
|--------------------------------|---|-----|
| PERMEABILITY (K _v) | → | 1 |
| Corresponding K _h | → | 2 |
| DRY DENSITY | → | 100 |
| MOISTURE CONTENT | → | 4 |
| -200 FINES CONTENT | → | 11 |

| FALLING HEAD PERMEABILITY (ASTM D 5084) | | | | |
|---|----------------|-------------------------|----------------------------|------------|
| No. of LAYERS: | 3 | Wt. of MOLD (lbs): | 9.31 | |
| BLOWS/LAYER: | 15 | Wt. of MOLD/SOIL (lbs): | 12.77 | |
| HEIGHT (FT) | TRIAL #1 (SEC) | TRIAL #2 (SEC) | PERMEABILITY | ASTM Check |
| 5 | 0.0 | 0.0 | | |
| 4 | 86.1 | 96.1 | 4.45E-04 | Passed |
| 3 | 120.0 | 132.6 | 4.14E-04 | Passed |
| 2 | 187.1 | 187.2 | 3.94E-04 | Passed |
| 1 | 317.0 | 320.4 | 3.95E-04 | Passed |
| | | | Below Standard: Rerun Test | |
| | | | Below Standard: Rerun Test | |
| Average Permeability | | | 4.1E-04 | cm/sec |

NUMBER OF INCHES MOLD WAS SHORT? 0.000 INCHES (ZERO INCHES IS DEFAULT)
 PERMEABILITY CONSTANT USED WAS → 0.07 (Includes 1/2" ID tubing)

| MOISTURE CONTENT (ASTM D 2216) | |
|--------------------------------|-------|
| Pan NUMBER | J-72 |
| Wt. of WET SOIL & | 225.6 |
| Wt. of DRY SOIL & | 218.7 |
| Wt. of PAN (g) | 50.3 |
| Wt. of Water (g) | 6.9 |
| Wt. of Dry Soil (g) | 168.4 |
| MOISTURE CONTE | 4.1 |

| -200 SIEVE WASH (ASTM D 1140) | |
|-------------------------------|-------|
| Pan NUMBER | J-72 |
| Wt. of DRY SOIL & P | 156.3 |
| Wt. of WASH SOIL & | 144.6 |
| Wt. of PAN (g) | 50.3 |
| Wt. of Original Dry S | 106.0 |
| Wt. of -200 Material (| 11.7 |
| Wt. of Washed Dry S | 94.3 |
| -200 FINES CONTEN | 11.0 |

APPENDIX D

Support Documents

Important Information about This

Geotechnical-Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical-engineering study conducted for a civil engineer may not fulfill the needs of a constructor — a construction contractor — or even another civil engineer. Because each geotechnical-engineering study is unique, each geotechnical-engineering report is unique, prepared *solely* for the client. No one except you should rely on this geotechnical-engineering report without first conferring with the geotechnical engineer who prepared it. *And no one — not even you — should apply this report for any purpose or project except the one originally contemplated.*

Read the Full Report

Serious problems have occurred because those relying on a geotechnical-engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

Geotechnical Engineers Base Each Report on a Unique Set of Project-Specific Factors

Geotechnical engineers consider many unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk-management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical-engineering report that was:

- not prepared for you;
- not prepared for your project;
- not prepared for the specific site explored; or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical-engineering report include those that affect:

- the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a light-industrial plant to a refrigerated warehouse;
- the elevation, configuration, location, orientation, or weight of the proposed structure;
- the composition of the design team; or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes—even minor ones—and request an

assessment of their impact. *Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.*

Subsurface Conditions Can Change

A geotechnical-engineering report is based on conditions that existed at the time the geotechnical engineer performed the study. *Do not rely on a geotechnical-engineering report whose adequacy may have been affected by:* the passage of time; man-made events, such as construction on or adjacent to the site; or natural events, such as floods, droughts, earthquakes, or groundwater fluctuations. *Contact the geotechnical engineer before applying this report to determine if it is still reliable.* A minor amount of additional testing or analysis could prevent major problems.

Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ — sometimes significantly — from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide geotechnical-construction observation is the most effective method of managing the risks associated with unanticipated conditions.

A Report's Recommendations Are Not Final

Do not overrely on the confirmation-dependent recommendations included in your report. *Confirmation-dependent recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations *only* by observing actual subsurface conditions revealed during construction. *The geotechnical engineer who developed your report cannot assume responsibility or liability for the report's confirmation-dependent recommendations if that engineer does not perform the geotechnical-construction observation required to confirm the recommendations' applicability.*

A Geotechnical-Engineering Report Is Subject to Misinterpretation

Other design-team members' misinterpretation of geotechnical-engineering reports has resulted in costly

problems. Confront that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Constructors can also misinterpret a geotechnical-engineering report. Confront that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing geotechnical construction observation.

Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical-engineering report should *never* be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, *but recognize that separating logs from the report can elevate risk.*

Give Constructors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make constructors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give constructors the complete geotechnical-engineering report, *but* preface it with a clearly written letter of transmittal. In that letter, advise constructors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. *Be sure constructors have sufficient time* to perform additional study. Only then might you be in a position to give constructors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

Read Responsibility Provisions Closely

Some clients, design professionals, and constructors fail to recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations," many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help

others recognize their own responsibilities and risks. *Read these provisions closely.* Ask questions. Your geotechnical engineer should respond fully and frankly.

Environmental Concerns Are Not Covered

The equipment, techniques, and personnel used to perform an *environmental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnical-engineering report does not usually relate any environmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures.* If you have not yet obtained your own environmental information, ask your geotechnical consultant for risk-management guidance. *Do not rely on an environmental report prepared for someone else.*

Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the *express purpose* of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold-prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, many mold-prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical-engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; *none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.*

Rely, on Your GBC-Member Geotechnical Engineer for Additional Assistance

Membership in the Geotechnical Business Council of the Geoprofessional Business Association exposes geotechnical engineers to a wide array of risk-confrontation techniques that can be of genuine benefit for everyone involved with a construction project. Confer with your GBC-Member geotechnical engineer for more information.

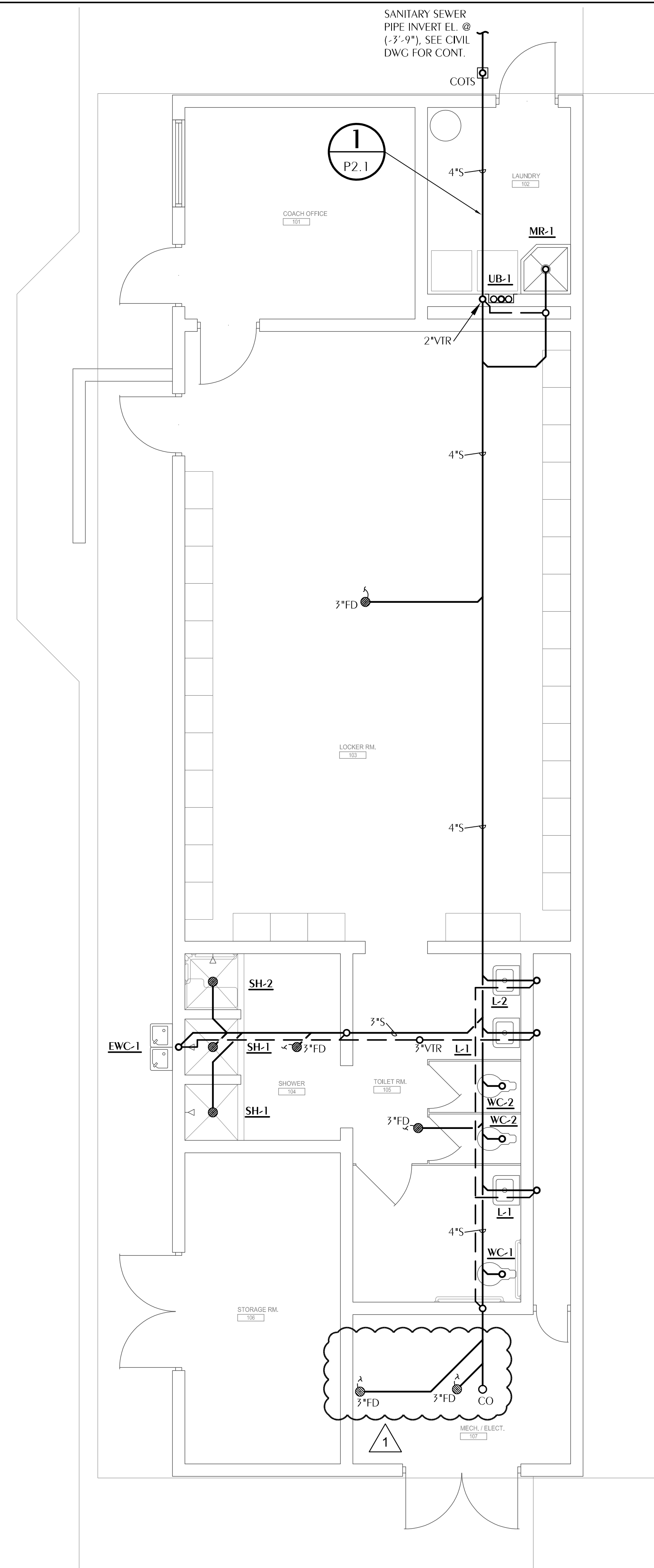


8811 Colesville Road/Suite G106, Silver Spring, MD 20910

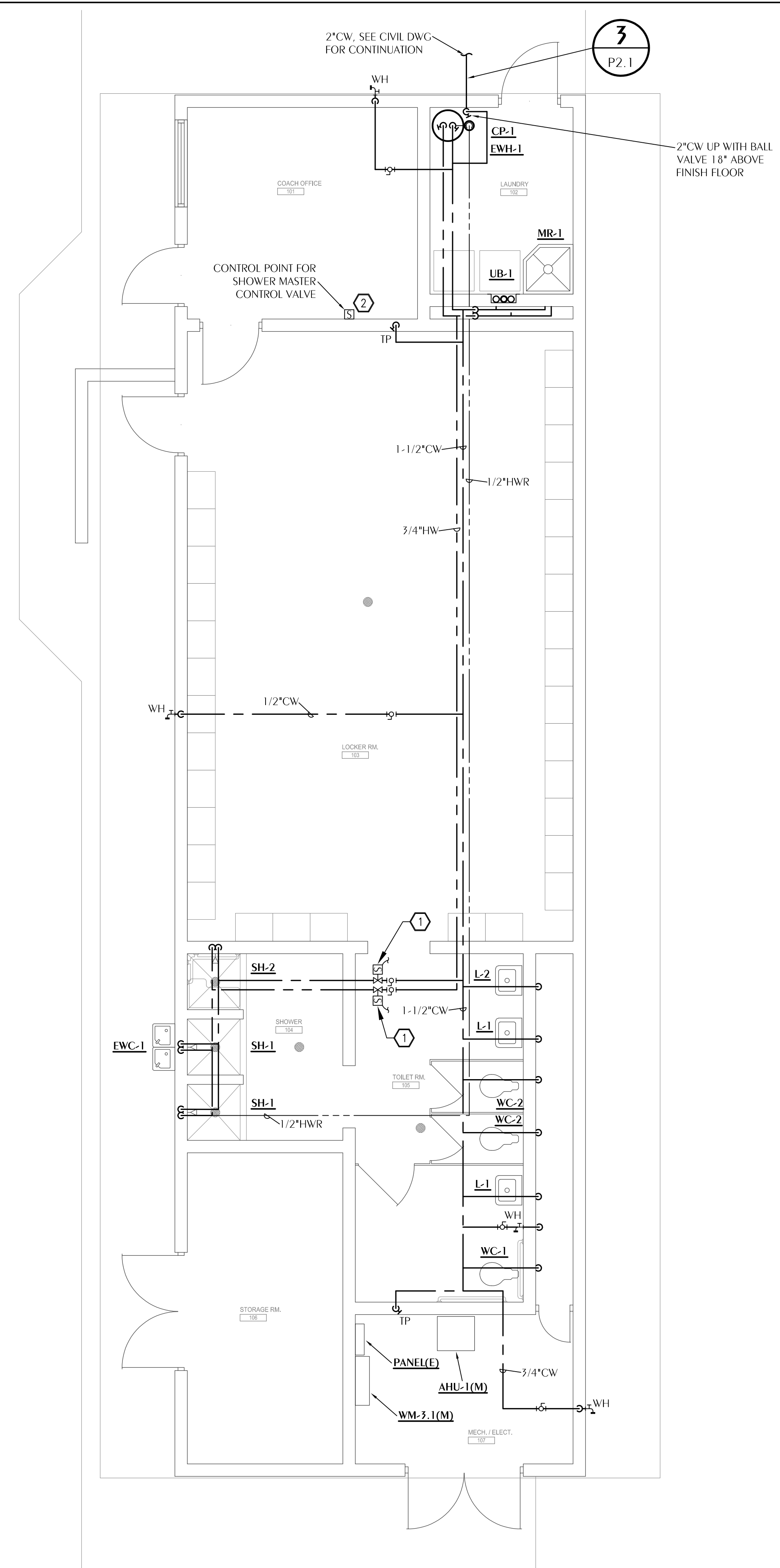
Telephone: 301/565-2733 Facsimile: 301/589-2017

e-mail: info@geoprofessional.org www.geoprofessional.org

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1 SANITARY NEW WORK FLOOR PLAN
 P1.1 SCALE: 1/4" = 1'-0"



2 DOMESTIC WATER NEW WORK FLOOR PLAN
 P1.1 SCALE: 1/4" = 1'-0"

REFERENCE:
 FINISHED FLOOR ELEVATION = 0'-0"

GENERAL NOTES

1. DUE TO PROXIMITY BETWEEN DOMESTIC WATER AND SANITARY BEING CLOSE WHILE ENTERING AND EXITING THE BUILDING, MAINTAIN MINIMUM 12" VERTICAL CLEARANCE BETWEEN THE TWO SYSTEMS PER SECTION 603.2 OF THE 2023 FLORIDA BUILDING CODE, PLUMBING, 8TH EDITION.

SHEET NOTES

1. PROVIDE 120 VOLT NORMALLY CLOSED SOLENOID VALVE FOR ON/OFF MASTER VALVE SERVING SHOWER AREAS. COORDINATE WITH ELECTRICAL POWER DRAWINGS. VALVE CONTROLS LOCATED IN COACHES' OFFICE.
2. VALVE CONTROLS FOR ON/OFF MASTER VALVE. INTERLOCK WITH OTHER CONTROLLED AREAS. COORDINATE WITH ELECTRICAL DRAWINGS. MOUNT AT 5'-4" ABOVE FLOOR. PROVIDE ENGRAVED PLASTIC SIGNAGE IDENTIFYING CONTROL AS "MASTER SHOWER CONTROL VALVE".

REVISIONS

| NO. | DESCRIPTION | DRAWN | CHECKED | DATE |
|-----|-------------|-------|---------|---------|
| 1 | ADDENDUM 2 | JDD | KAJ | 4/11/26 |
| | | | | |
| | | | | |
| | | | | |

PHASE

| PHASE | DRAWN | CHECKED | DATE |
|------------------------|-------|---------|----------|
| SCHEMATIC DESIGN | JDD | KAJ | 10/11/25 |
| DESIGN DEVELOPMENT | JDD | KAJ | 1/9/26 |
| CONSTRUCTION DOCUMENTS | JDD | KAJ | 4/3/26 |

JRA ARCHITECTS 2211 NAVY BLVD., STE 100
 PANAMA CITY BEACH, FL
 PHONE: (850) 236-9832
 Commission Number: 25871

WATFORD ENGINEERING
 4432 Clinton Street, Marianna, Florida 32446 Florida Certificate of Authorization: 27825
 850.256.3447 Project Number: 2025056 Keith A. Johnson, PE Florida License #6462

PROJECT:
 BAY DISTRICT SCHOOLS
 NEW SOFTBALL FIELD HOUSE
 MOSLEY HIGH SCHOOL
 LYNN HAVEN, FLORIDA

SHEET TITLE:
 PLUMBING NEW WORK
 FLOOR PLANS

SHEET NUMBER:
 P1.1

Addendum #3

Mosley Softball Fieldhouse

JRA Commission. 25871 CA/BC

Bay District Schools
1311 Balboa Avenue
Panama City, Florida 32401

JRA Architects, Inc.
2211 Navy Blvd- Suite 100
Panama City, Florida 32408

Date of Issue of addendum: **April 23, 2026**

The changes herewith form part of the Construction Documents and modify the original “Construction Documents” dated April 3, 2026.

This Addendum consists of **1** page(s), **0** attachment(s) and **2** revised plan sheet(s) attached and as referenced herein.

ITEM 3.1

Drawings: **Clarification to Construction Documents** – See Note 1 on sheet M1.1 the dryer exhaust goes to a gooseneck on the roof.

ITEM 3.2

Drawings: **Clarification to Construction Documents**

- The condensate drain for CC-2.1 should be drained to the mop sink in 102.
- The condensate drain for WM-1.1 and WM-3.1 should be drained to the new floor drain that was added in Mech. / Electrical 107.

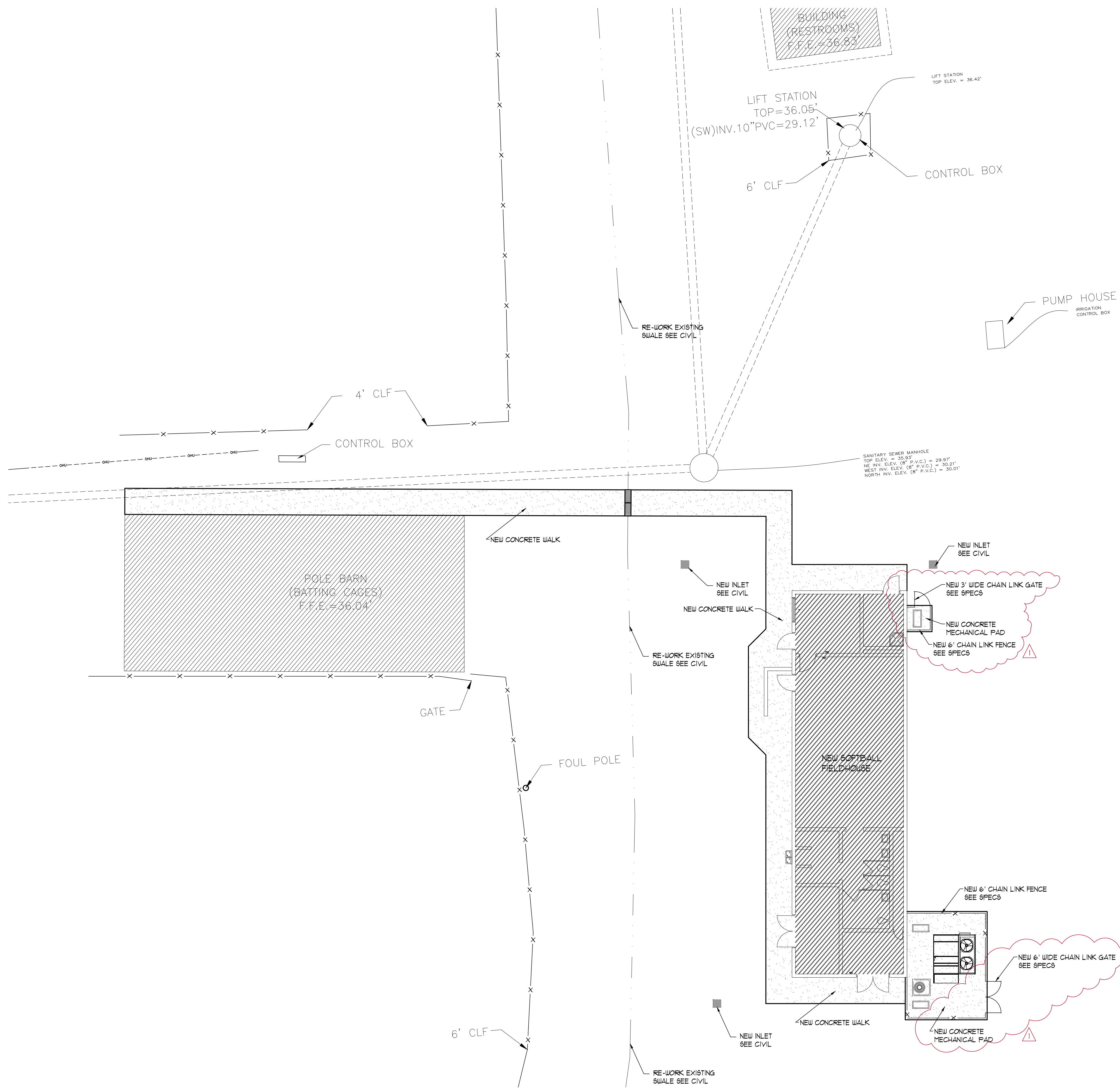
ITEM 3.3

Drawings: Replace **Drawings sheet A0.1 Site Plan** with the Attached Drawing Sheet A0.1 with a revision date of 4/23/26.

ITEM 3.4

Drawings: Replace **Drawings sheet A1.1 Floor Plan** with the Attached Drawing Sheet A1.1 with a revision date of 4/23/26.

END OF ADDENDUM #3



| REVISIONS | | | | |
|------------------------|-------------|-------|---------|----------|
| NO. | DESCRIPTION | DRAWN | CHECKED | DATE |
| 1 | ADDENDUM 3 | | | 4/23/26 |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| PHASE | | | | |
| | | DRAWN | CHECKED | DATE |
| SCHEMATIC DESIGN | | MAY | SLB | 10/11/25 |
| DESIGN DEVELOPMENT | | MAY | SLB | 1/9/26 |
| CONSTRUCTION DOCUMENTS | | MAY | SLB | 4/3/26 |

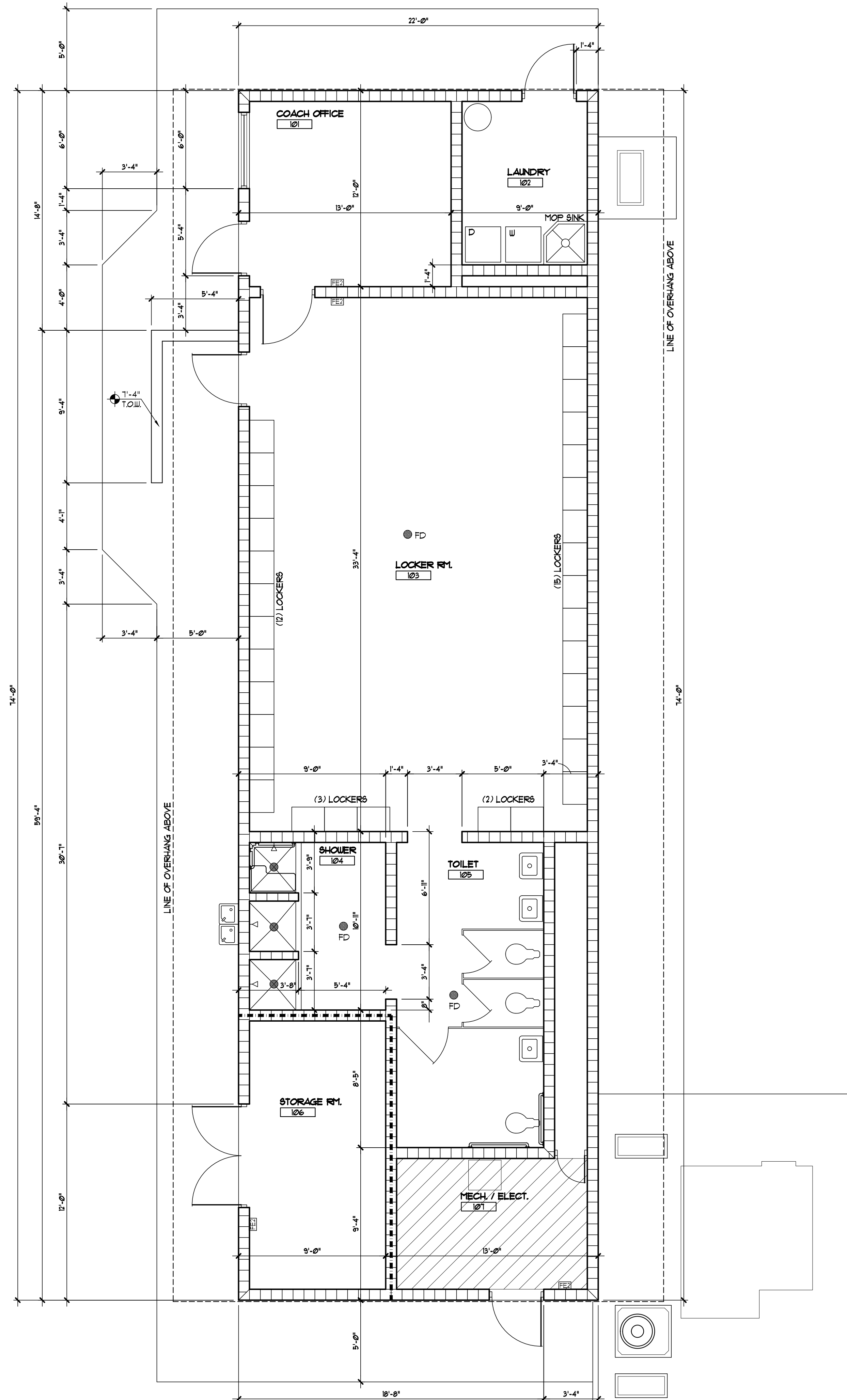
JRA ARCHITECTS
 2211 NAVY BLVD., STE 100
 PANAMA CITY BEACH, FL
 PHONE: (850) 236-9832
 Commission Number: 25871

CONSULTANTS:
 PROJECT:

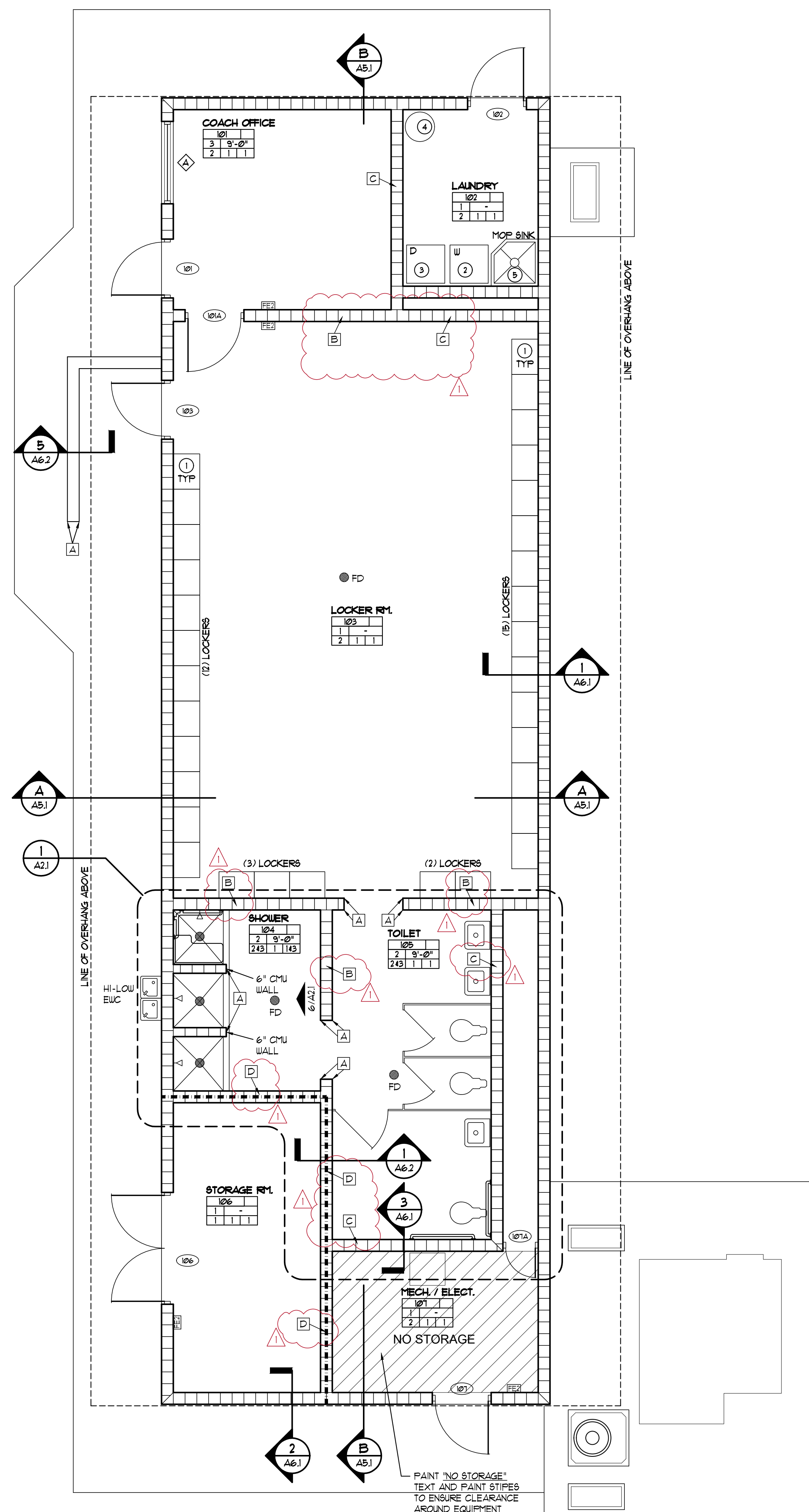
BAY DISTRICT SCHOOLS
 NEW SOFTBALL FIELD HOUSE
 MOSLEY HIGH SCHOOL
 LYNN HAVEN, FLORIDA

SHEET TITLE:
 SITE PLAN

SHEET NUMBER:
 A0.1



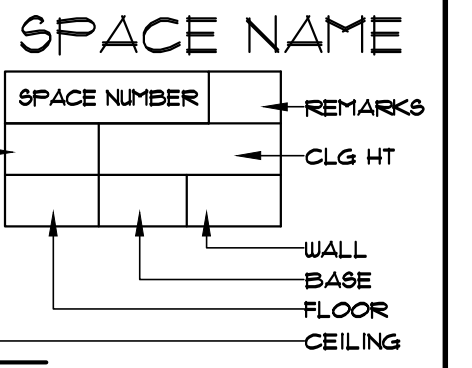
DIMENSIONED FLOOR PLAN
SCALE: 1/4" = 1'-0"



ARCHITECTURAL FLOOR PLAN
SCALE: 1/4" = 1'-0"

FINISH SCHEDULE

- FLOORS**
1. SEALED CONCRETE
 2. EPOXY PAINT
 3. RESINOUS EPOXY FLOORING
 4. NOT USED
- BASE**
1. VINYL
 2. NOT USED
 3. NOT USED
 4. NOT USED
- WALLS**
1. EPOXY PAINTED CMU
 2. NOT USED
 3. APPLIED EPOXY
 4. NOT USED
- CEILING**
1. EXPOSED TRUSSES
 2. MR GYP BC
 3. ACOUSTICAL LAY IN
 4. NOT USED
- REMARKS**



LEGEND

- (E) - SURFACE MOUNTED FIRE EXTINGUISHER
- (B) - SEMI-RECESSED FIRE EXTINGUISHER
- (F) - BRACKET HUNG FIRE EXTINGUISHER

EQUIPMENT SCHEDULE

1. 24"W x 14 3/4"H x 18" D - SINGLE TIER LOCKERS, N.C.
2. WASHER, N.C.
3. DRYER, N.C.
4. ELECTRIC WATER HEATER - SEE PLUMBING
5. JANITOR'S MOP SINK - SEE PLUMBING

CONSTRUCTION KEYNOTES

- (A) BULL NOSE - CMU BLOCK
- (B) METAL FRAMED WALL W/ MOISTURE RESISTANT GUB FINISH @ EA. SIDE (CONT.) FROM TOP OF CMU WALL TO ROOF DECK - SEE SECTIONS.
- (C) METAL FRAMED WALL W/ MOISTURE RESISTANT GUB FINISH @ EA. SIDE (CONT.) W/ (R-19) OPEN CELL SPRAYED INSULATION (CONT.) FROM TOP OF CMU WALL TO ROOF DECK - SEE SECTIONS.
- (D) MTL FRAMED WALL W/ 5/8" TYPE "X" FIRE RATED GYP BD BOTH SIDES (CONT. FROM TOP OF CMU PORTION OF THE WALL TO UNDERSIDE OF MTL ROOF DECK W/ MINERAL WOOL BETWEEN TOP OF MTL TRACK & MTL ROOF DECK ABOVE & FIRE CAULKED @ TOP OF GYP BD TO DECKING ABOVE - ENTIRE WALL TO BE FIRE RATED - METAL FRAMED PORTION OF THE WALL TO MEET (UL # U465) CMU PORTION OF THE WALL TO MEET (UL # 1906)

REVISIONS

| NO. | DESCRIPTION | DRAWN | CHECKED | DATE |
|-----|-------------|-------|---------|---------|
| 1 | ADDENDUM 3 | | | 4/23/26 |

PHASE

| | DRAWN | CHECKED | DATE |
|------------------------|-------|---------|----------|
| SCHEMATIC DESIGN | MAY | SLB | 10/11/25 |
| DESIGN DEVELOPMENT | MAY | SLB | 1/9/26 |
| CONSTRUCTION DOCUMENTS | MAY | SLB | 4/3/26 |

JRA ARCHITECTS 2211 NAVY BLVD., STE 100
PANAMA CITY BEACH, FL
PHONE: (850) 236-9832
Commission Number: 25871

CONSULTANTS:

PROJECT:

**BAY DISTRICT SCHOOLS
NEW SOFTBALL FIELD HOUSE
MOSLEY HIGH SCHOOL**
LYNN HAVEN, FLORIDA

SHEET TITLE:
FLOOR PLAN

SHEET NUMBER:
A11

BDS Mosley HS New Softball Field House

| RFI # | Question | Bid Package | Architect/School District Response |
|-------|---|----------------|--|
| 1 | Confirm there are no requirements for access control, fire alarm or telecom for the Mesley Softball Field House Project? 4.20.26 9AM | 16A | There are no requirements for access control, fire alarm or telecom for the Mosely Softball Field House 4.20.26 10:25AM |
| 2 | Confirm that Asphaltic Concrete Paving is not needed Sheet C1.10 There is no drawing detail. 4.20.26 11:08AM | 02A | This is correct, there is no asphalt paving on this project. 4.20.26 11:08AM |
| 3 | Opening dimension needed for the window A4.1 4.20.26 11:08AM | 10A | The size of the window is provided on sheet A9.1 and in the specifications 08 43 13 paragraph 2.2 performance requirements item C states that wind loads are to be as indicated on the structural drawings. Wind Velocity is given on sheet S0.2 and component and cladding pressures are given there as well. 4.20.26 11:08AM |
| 4 | Is there a specific Waterproof Material needed for Sheet E1.2 Keynote 7 4.20.26 11:08AM | 16A | This note is referencing an in-use weatherproof switch cover. |
| 5 | Regarding the window Type; the specs call for both fixed and operable window systems. Which window system will be used? 4.20.26 12:34PM | 07A | Fixed 4.20.26 12:41PM |
| 6 | Confirm no gutter and downspout required. | 07A | That Is Correct there are now gutters and downspouts |
| 7 | 1)Sheet A0.1 a.The plan does not show the exterior mechanical pad/fencing that is shown on the civil and mechanical plans. | 03A 15C 10A | See Addendum 3 |
| 8 | b.Need information on the fencing for the mechanical areas (height and gate width) Sheet A0.1 | 10A | See Addendum 3 |
| 9 | c.Confirm both areas will have an exterior concrete pad and if the HVAC units will have bases or if concrete bases will be needed. Sheet A0.1 | 02A 03A | Yes both will have concrete pads See Addendum 3 |

| | | | |
|----|---|-----------------|---|
| 10 | d. There is a note to rework the swale and what appears to be some type of culvert?? Please confirm what that is and provide a detail. Sheet A0.1 | 02A | Answered in Addendum 2 C1.5 DS1, DS2, DS3 |
| 11 | 2) Sheet A1.1 a. Need designation for the type of CMU wall for the exterior (Shane said it will need spray foam in the CMU but it's not called out and the wall sections don't show it either). | 04A 05A | Answerd in Addendum 2 - Refer to Drawings Sheet A1.1 Architectural Floor Plan |
| 12 | b. Many interior walls are showing metal stud framing/sheathing with spray foam above the CMU and ceiling. Shane and I discussed we may not need to have all the walls shown with spray foam and he is supposed to correct some. Sheet A1.1 | 09A 05A | See Addendum 3 |
| 13 | c. The plumbing chase wall is shown as type "E" which is fire rated but it doesn't need to be. Sheet A.1 | 09A | See Addendum 3 |
| 14 | d. Need wall designation for the laundry room chase wall. Sheet A1.1 | 09A | See Addendum 3 |
| 15 | e. Is door 107A for the entrance into the needed? Structural plans show a lintel but both areas are exposed to the deck. A1.1 | 08A Doors | Yes this is needed and the wall is continuous over the door as well |
| 16 | 3) Sheet A5.1 a. Are the lockers that are N.I.C. coming with an integral base or will concrete bases be needed so the resinous flooring can be rolled up? | 09B Flooring | The lockers have no base and simply sit on the floor |
| 17 | 4) Sheet M1.1 a. Confirm if the dryer exhaust vents through the roof. Note says it goes to a gooseneck but doesn't show penetration. | 15C HVAC | See addendum 3 |
| 18 | b. Where will all the mini-split condensate drains be routed? Storage room has no drains shown in the plumbing. The mechanical room split is on the west wall but the only drain is in the center of the room. Where will the ceiling cassette in the coach's office be routed? | 15C HVAC | Answered in Addendum #2. (pg 47-48) New drain is to go into the mechanical room per P1.1 and P2.1 |
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