

STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION
DRAINAGE CONNECTION PERMIT

To be completed by DOT

Drainage Connection Permit No. 2024-D-391-00036 Date 11/20/2024
Received By One-Stop Permitting System Maintenance Unit Panama City Operations
State Road No. 30 Work Program Project No. _____
Section No. 010 Construction Project No. _____
Milepost .206 - .425 Station _____

Instructions for Drainage Connection Permit

Pursuant to 14-86.004(5), F.A.C. Once approved by the Department, the drainage connection application and supporting documents become the Drainage Connection Permit.”

Each completed Drainage Connection Permit package shall include the following items. If an item does not apply to your project, indicate “Not Applicable” or “N/A.”

Included	Part	Title	Completed by:	Special Instructions
	1	Permit Information Sheet	Applicant	
	2	Certification by a Licensed Professional	Licensed Professional	Signed and Sealed
	3	Certification	Applicant	Signature
	4	Owner's Authorization of a Representative	Owner	Signature
	5	Affidavit of Ownership or Control and Statement of Contiguous Interest	Owner	Signature
	6	Permit General Conditions	FDOT	
	7	Permit Special Conditions	FDOT	
	8	As-Built Certification	Licensed Professional	Signed and Sealed – Submit within 15 working days of completion of construction
	Attachment	Legal Description		
	Attachment	Photographs of Existing Conditions		
	Attachment	Location Map		
	Attachment	Grading Plan	Licensed Professional	Signed and Sealed
	Attachment	Soil Borings		
	Attachment	Water Table / Percolation		
	Attachment	Calculations		
	Attachment	CD with Electronic Files of all Submittal Items		Scanned Images in pdf format

Note: Different Licensed Professionals may complete parts of the permit package. For example, the Licensed Professional signing and sealing the as-built certification may be different from the Licensed Professional who signed and sealed the calculations for the permit package.

EXCEPTIONS: Activities that qualify for an Exception are listed in Rule 14-86, F.A.C. A permit application to the Department is NOT required. However, if you desire verification whether the work qualifies for an exception, send a completed copy of this permit package with its requested information to the applicable FDOT District Office.

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

PART 1 – Permit Information SheetSelect one: ☒ Permit ☐ Exception**Pursuant to 14-86.002(2), F.A.C. "Applicant means the owner of the adjacent property or the owner's authorized representative."****Applicant**Select one: ☐ Property Owner ☒ Owner's Representative (Complete Part 4)Name: SIGNE ULSAMERTitle and Company: GEORGE AND ASSOCIATES CONSULTING ENGINEERSAddress: 1967 Commonwealth Lane Suite 200City: Tallahassee State: Florida Zip: 32303Telephone: (850) 521-0344 ext. 115 FAX: _____ Email: sulsamer@gaceng.net**Property Owner (If not applicant)**Name: David MatsonTitle and Company: Assistant Bureau Chief, FDEP- Bureau of Design and Construction - DRPAddress: 3900 Commonwealth Blvd.City: Tallahassee State: Florida Zip: _____Telephone: (850) 245-2594 ext. _____ FAX: _____ Email: david.matson@floridadep.gov**Applicant's Licensed Professional**Name: James Peterson Florida License Number: 80485Title and Company: Project Manger, George & Associates Consulting EngineersAddress: 1967 Commonweath LaneCity: Tallahassee State: Florida Zip: 32303Telephone: (850) 521-0344 ext. 103 FAX: _____ Email: sulsamer@gaceng.net**Project Information:**Project Name: Camp Helen ImprovementsLocation: SR 30 Panama City Beach

STREET	SR. NO.	US HWY NO.	CITY
<u>Bay</u>	<u>010</u>	<u>2S</u>	<u>17W</u>
COUNTY	SECTION(S)	TOWNSHIP(S)	RANGE(S)

Geographic Coordinates: Latitude (DMS.SSS): 30.275565 Longitude (DMS.SSS): 85.992041Benchmark Horizontal Datum: (/ _____.) State Plane Coordinates: Northing 0 Easting: 0Projection Zone: ☒ Florida North ☐ Florida East ☐ Florida West

Coordinate shall be the center of the driveway intersection with FDOT R/W, or, if there is no driveway connection, near the center of the property line nearest the state highway.

*Check with the FDOT Office for requirement.

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

Brief description of facility and proposed connection:

Please see attached Drainage Design Manual.

Briefly describe why this activity requires a Drainage Connection Permit (Include where the stormwater will discharge to FDOT right of way):

Please see attached Drainage Design Manual.

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

PART 2 – Certification by a Licensed Professional

In accordance with Rule 14-86, Florida Administrative Code (F.A.C.), I hereby certify that the following requirements are and/or will be met.

This project has been designed in compliance with all applicable water quality design standards as required by state or federal governmental entity(ies).

14-86.004(3)(f) (F.A.C.): Certification by a Licensed Professional that the complete set of plans and computations complies with one of the following Rules Sections:

☐ 14-86.003(2)(a) (F.A.C.), or ☐ 14-86.003(2)(b) (F.A.C). (check one)

I further certify that a National Pollutant Discharge Elimination System (NPDES) permit for stormwater discharges associated with industrial activity from construction sites

☐ is required ☐ is not required. (check one)

I am aware that there are significant penalties for submitting false information, including the possibility of fines and imprisonment.

This certification shall remain valid for any subsequent revision or submittal of plans, computation or other project documents by me.

Name of Licensed Professional: James Peterson (JAMES H. PETERSON, IV)

Florida License Number: 80485

Company Name (if applicable): George & Associates Consulting Engineers

Certificate of Authorization Number (if applicable): _____

Address: 1967 Commonwealth Lane

City: Tallahassee State: Florida Zip: 32303

Telephone: (850) 521-0344 ext. 103 Fax: _____ Email: sulsamer@gaceng.net

JPETERSON@GACENG.NET

Signature of Licensed Professional

Date

(Affix Seal)

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

PART 3 – Certification by Applicant

I hereby certify that the information in this submittal is complete and accurate to the best of my knowledge.

Applicant's Signature: Signe Ulsamer Digitally signed by Signe Ulsamer
Date: 2024.11.20 12:59:11 -05'00' Date: _____
Name (Printed): SIGNE ULSAMER
Title and Company: Project Engineer, GEORGE AND ASSOCIATES CONSULTING ENGINEERS
Address: 1967 Commonwealth Lane Suite 200, Tallahassee, Florida 32303
Phone Number: (850) 521-0344 ext. 115 E-mail address: sulsamer@gaceng.net

PART 4 – Owner's Authorization of a Representative

I (we), the owner, David Matson FDEP/BDC Assistant Bureau Chief, do hereby authorize the following person, or entity, as my representative:

Name (Printed): SIGNE ULSAMER
Title and Company: Project Engineer, GEORGE AND ASSOCIATES CONSULTING ENGINEERS
Address: 1967 Commonwealth Lane Suite 200, Tallahassee, Florida 32303
Phone Number: (850) 521-0344 ext. 115 E-mail address: sulsamer@gaceng.net

Part 5 – Affidavit of Property Ownership or Control and Statement of Contiguous Interest

I, David Matson FDEP/BDC Assistant Bureau Chief, certify that I own or lawfully control the following described property:
Camp Helen State Park, Parcel ID: 35205-000-000, 23937 PC BCH PKWY, PANAMA CITY BEACH 32413
31 2S 17W -7- 5C ALL OF GOVT LOTS 2, 7, 8, 10 & 11 LESS HWY 98 R/W IN SEC 31 ORB 1094 P 1910 ORB 1640 P1928

Does the property owner own or have any interests in any adjacent property?

☒ No ☐ Yes If yes, please describe.

Owner's Signature required for Parts 4 and/or 5

We will not begin on the drainage connection until I receive the Permit and I understand all the conditions of the Permit. When work begins on the connection, I am accepting all conditions listed in the Permit.

Name (Printed): David Matson
Address: 3900 Commonwealth Blvd., Tallahassee, Florida
Phone Number: (850) 245-2594 ext.
Signature: David Matson Digitally signed by David Matson
Date: 2024.11.20 11:27:37 -05'00' Date: _____

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

PART 6 – Permit General Conditions

1. This permit is a license for permissive use only and does not convey any property rights either in real estate or material, or any exclusive privilege and it does not authorize any injury to private property or invasion of private rights, or any infringement of Federal, State or local laws, rules or regulations; nor does it obviate the necessity of obtaining any required state or local approvals.
2. The drainage connection as authorized herein shall be constructed and thereafter maintained in accordance with the documents attached hereto and incorporated by reference herein. All work performed in the Department's right of way shall be done in accordance with the most current Department standards, specifications and the permit provisions. Such construction shall be subject to the inspection and approval of the Department, and the Department may at any time make such inspections as it deems necessary to assure that the drainage connection is in compliance with this permit.
3. The entire expense of construction within the Department right of way, including replacement of existing pavement or other existing features, shall be borne by the permittee.
4. The permittee shall maintain that portion of the drainage connection authorized herein located on permittee's property in good condition. The Department shall maintain that portion of the drainage connection authorized herein located within its right of way.
5. If the drainage connection is not constructed, operated or maintained in accordance with this permit, the permit may be suspended or revoked. In this event modification or removal of any portion of the drainage connection from the Department's right of way shall be at the permittee's expense.
6. The Department reserves the right to modify or remove the drainage connection to prevent damage or in conjunction with road improvements.
7. It is understood and agreed that the rights and privileges herein set out are granted only to the extent of the Department's right, title, and interest in the land to be entered upon and used by the permittee, and the permittee will, at all times, assume all risk of and indemnify, defend and save harmless the Department from and against any and all loss, damage, cost or expense arising in any manner on account of the exercise or attempted exercises by said permittee of these rights and privileges, regardless of the respective degrees of fault of the parties.
8. Utilities, including gas lines, may exist within the right of way. Prior to beginning work the permittee shall contact Sunshine State One Call of Florida, Inc at 811 or 800-432-4770, who will notify all utility owners near the scheduled project. The utility owners have two (2) full business days to provide locations of their respective facilities. The permittee shall be solely responsible for any damage to or conflicts with gas lines, utilities and/or third persons.
9. The permittee shall notify the Department of Transportation Maintenance Office located at Panama City Operations Phone (850) 767-4914 ext. _____ 48 hours in advance of starting any work on the drainage connection authorized by this permit and also 24 hours prior to any work within the Department's right of way. Construction of any work on the right of way shall be completed within _____ days after such notification. If such construction is not completed within _____ days after such notification, the permittee shall notify the Department of the anticipated completion date.
10. This permit shall expire if construction on the drainage connection is not begun within one year from the date of approval and if construction on the drainage connection is not completed by (Date) 1/16/2026.
11. A permittee may request an extension of the Drainage Connection Permit expiration date by filing a written request for a permit time extension. All requests for time extensions must be received by the Department 15 working days prior to the expiration date.
12. All the provisions of this permit shall be binding on any assignee or successor in interest of the permittee.

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

PART 7 – Permit Special Conditions – To be completed by FDOT

The above request has been reviewed and has been found to meet the regulations as prescribed in Rule 14-86, F.A.C., and is hereby approved, subject to the following special conditions:

Department of Transportation:

Signature Lisa Ward

Title MAINTENANCE MANAGER/PERMITS

Date 1/16/2025

Approved
 2024-D-391-00036
 Lisa Ward
 1/16/2025

PART 8 – As-Built Certification

Within 15 working days of completion of construction, you must send this certification to the Department office in which you filed your DOT Drainage Permit.

1. STORMWATER FACILITY INFORMATION

Permit No.: _____

Source (Project) Name: _____

Source Location: Street _____

City: _____ County: _____

Source Owner: _____

Owner Address: _____

2. AS-BUILT CERTIFICATION

I hereby certify that this stormwater facility has been built substantially in accordance with the certified design plans, and that any substantial deviations (noted below) will not prevent the facility from functioning in compliance with the requirements of Chapter 14-86 F.A.C. when properly maintained and operated. These determinations have been based upon on-site observation of construction, scheduled and conducted by me or by a project representative under my direct supervision.

Name of Licensed Professional: _____

Florida License Number: _____

Company Name (if applicable): _____

Certificate of Authorization Number (if applicable): _____

Address: _____

City: _____ State: _____ Zip: _____

Telephone: _____ Fax: _____ Email: _____

Signature of Licensed Professional_____
Date

(Affix Seal)

Substantial deviations from the approved plans and specifications (attach additional sheets if required).

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1/16/2025

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☐ is required ☐ is not required. (check one)

I am aware that there are significant penalties for submitting false information, including the possibility of fines and imprisonment.

This certification shall remain valid for any subsequent revision or submittal of plans, computation or other project documents by me.

Name of Licensed Professional: James Peterson (JAMES H. PETERSON, IV)

Florida License Number: 80485

Company Name (if applicable): George & Associates Consulting Engineers

Certificate of Authorization Number (if applicable): _____

Address: 1967 Commonwealth Lane

City: Tallahassee State: Florida Zip: 32303

Telephone: (850) 521-0344 ext. 103 Fax: _____ Email: sulsamer@gaceng.net

JPETERSON@GACENG.NET

Signature of Licensed Professional

Date

(Affix Seal)

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

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I hereby certify that the information in this submittal is complete and accurate to the best of my knowledge.

Applicant's Signature: Signe Ulsamer Digitally signed by Signe Ulsamer
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Title and Company: Project Engineer, GEORGE AND ASSOCIATES CONSULTING ENGINEERS
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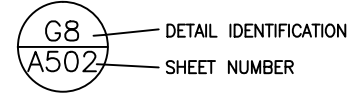
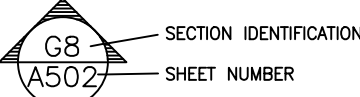
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Lisa Ward
1/16/2025

ABBREVIATIONS

A.F.F.	ABOVE FINISHED FLOOR
A.H.U.	AIR HANDLING UNIT
ALUM.	ALUMINUM
ALT.	ALTERNATE
APPROX.	APPROXIMATE
BD.	BOARD
BLDG.	BUILDING
BULK.	BLOCK
BLDG.	BLOCKING
BLT.	BUILT
BRK.	BRICK
BRKR.	BREAKER
BSMT.	BASEMENT
C.J.	CONTROL JOINT
C.D.	CEILING
CLR.	CLEAR
CMU	CONCRETE MASONRY UNIT
CO.	CLEAN OUT
CONC.	CONCRETE
CU.	COPPER
CU. FT.	CUBIC FOOT
CU. IN.	CUBIC INCH
CU. YD.	CUBIC YARD
DA./Ø.	DIAMETER
DBL.	DOUBLE
DBT.	DRY-BULB TEMPERATURE
DEG.	DEGREE
DEPT.	DEPARTMENT
DF.	DRINKING FOUNTAIN
DISC.	DISCONNECT
D.	DEAD LOAD
DN.	DOWN
D.S.	DOWN SLOUT
DWG.	DRAWING
E.F.	EXHAUST FAN
EXH	EXHAUST
EXP. JT.	EXPANSION JOINT
EXT.	EXTERIOR
FIN.	FINISH
FL.	FLOOR
FLUOR.	FLUORESCENT
FR.	FIRE RATING
FT.	FOOT/FEET
FIG.	FIGURING
GALV.	GALVANIZED
GF1	GROUND FAULT
GOVT.	GOVERNMENT
GR.FL.	GROUND FLOOR
GYP.	GYPSPUM
H.C.	HOLLOW CORE
H.D.G.	HOT DIPPED GALVANIZED
HDR.	HEADER
HDWR.	HARDWARE
H.P.	HORSEPOWER
HT.	HEIGHT
HTR.	HEATER
HV.	HIGH VOLTAGE
HVAC.	HEATING, VENTILATING AND AIR CONDITIONING
HWY.	HIGHWAY
ID.	INSIDE DIAMETER
IN.	INCH
INCAND.	INCANDESCENT
INCL.	INCLUDED
INSUL.	INSULATION
INT.	INTERIOR
INV. EL.	INVERT ELEVATION
JST.	JOIST
KD.	KILN DRIED
KW.	KILOWATT
KWH.	KILOWATT HOUR
LAM.	LAMINATED
LAV.	LAVATORY
LB.	POUND
LTC.	LIGHTING
LGTH.	LENGTH
LIN.	LINEAR
LL.	LIVE LOAD
MANUF.	MANUFACTURE
MAX.	MAXIMUM
MF.	MILL FINISH
MIN.	MINIMUM
MLDG.	MOLDING
MHW.	MEAN HIGH WATER
MHRW.	MEAN HIGHER HIGH WATER
M.L.W.	MEAN LOW WATER
MLW.	MEAN LOWER LOW WATER
MSL.	MEAN SEA LEVEL
MOD.	MODIFICATION
NTS.	NOT TO SCALE
NO./#.	NUMBER
OA.	OVERALL
O.C.	ON CENTER
O.D.	OUTSIDE DIAMETER
OFF.	OFFICE
O/H.	OVER HEAD
OPP.	OPPOSITE
PARTN.	PARTITION
PC.	PORTLAND CEMENT
PF.	POUNDS PER CUBIC FOOT
P.E.	PROFESSIONAL ENGINEER
PERF.	PERFORATE
PERF.	PERRPENDICULAR
PL.	PLATE
P.G.	PILING
PLYWD.	PLYWOOD
PNL.	PANEL
PREFAB.	PREFABRICATED
PRELIM.	PRELIMINARY
PSF.	POUNDS PER SQUARE FOOT
PSI.	POUNDS PER SQUARE INCH
P.T.	PRESSURE TREATED
QS.	QUARTER SAWN
R.	RADIUS
RCPT.	RECEPTACLE
REBAR.	REINFORCING BAR
REFRIG.	REFRIGERATION
REINF.	REINFORCING
RG.	ROOFING
RGH.	ROUGH
RM.	ROOM
R.O.	ROUGH OPENING
RS.	ROUGH SAWN
SC.	SOLID CORE
SCD.	SCHEDULE
SDG.	SIDING
SECT.	SECTION
SFTWD.	SOFTWOOD
SGD.	SLIDING GLASS DOOR
SH.	SHINGLES
SPEC.	SPECIFICATION
SPR.	SPRUCE
SQ.	SQUARE
SQ. FT.	SQUARE FOOT
SQ. IN.	SQUARE INCH
SQ. YD.	SQUARE YARD
SS.	STAINLESS STEEL
STL.	STEEL
SUB. FL.	SUBFLOOR
SUP.	SUPPLY
SW.	SWITCH
SYM.	SYMMETRICAL
S.Y.P.	SOUTHERN YELLOW PINE
SAS.	SURFACED FOUR SIDES
TEL.	TELEPHONE
T&G.	TONGUE-AND-GROOVE
TYP.	TYPICAL
U.E.	UNDERGROUND ELECTRIC
U.G.	UNDER GROUND
UL.	UNDERWRITERS LABORATORIES, INC.
V.	VOLT
VENT.	VENTILATOR
VERT.	VERTICAL
VF.	VERIFY IN FIELD
VOL.	VOLUME
VP.	VENT PIPE
VTR.	VENT THRU ROOF
W.	WATER
WBT.	WET BULB TEMPERATURE
WC.	WATER CLOSET
WD.	WOOD
WP.	WATERPROOF
WWF.	WELDED WIRE FABRIC
YD.	YARD

REFERENCE LEGEND

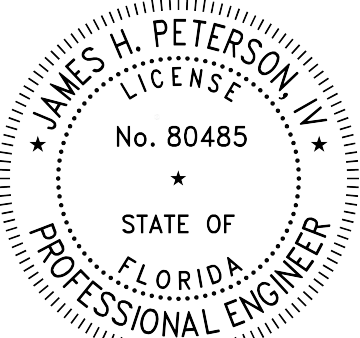


APPLICABLE CODES AND DESIGN DATA

CODE LIST

FLORIDA BUILDING CODE, BUILDING (FBC-B).....	2023 Edition
FLORIDA BUILDING CODE, FUEL GAS (FBC-FG).....	2023 Edition
FLORIDA BUILDING CODE, MECHANICAL (FBC-M).....	2023 Edition
FLORIDA BUILDING CODE, PLUMBING (FBC-P).....	2023 Edition
FLORIDA BUILDING CODE, EXISTING BUILDING (FBC-EB).....	2023 Edition
FLORIDA BUILDING CODE, RESIDENTIAL (FBC-R).....	2023 Edition
FLORIDA FIRE PREVENTION CODE (FFPC).....	Latest Edition
NATIONAL ELECTRICAL CODE NFPA-70.....	Latest Edition
FDOT STANDARD SPECIFICATIONS FOR ROAD & BRIDGE CONST.	Latest Edition
FDOT STANDARD PLANS FOR ROAD CONST.....	Latest Edition
FLORIDA ACCESSIBILITY CODE.....	2023 Edition

SEE LS001 FOR DESIGN DATA



NOT FOR CONSTRUCTION

CAMP HELEN
STATE PARK
DISTRICT 1
BAY COUNTY

PARK IMPROVEMENT

PROJECT # 61307C - N3803

SCOPE OF PROJECT

CONTRACTOR SHALL PROVIDE ALL LABOR, MATERIALS, EQUIPMENT, SUPERVISION, AND PERMITTING TO SUCCESSFULLY CONSTRUCT ROADWAY ALTERATIONS, NEW DRIVEWAY, ENTERANCE PARKING AREA, RESTROOM, PAVILIONS, ADA ACCESSIBLE WALKWAYS, RAMPS, STAIRWAY, ADA ACCESSIBLE CANOE/KAYAK LAUNCH, AND ANY OTHER SITE WORK PER THE CONTRACT DOCUMENTS.

THE CONSTRUCTION OF A DAY-USE RESTROOM FACILITY CONSISTING OF 650 GSF OF ENCLOSED AREA INCLUDING A MEN’S RESTROOM, WOMEN’S RESTROOM, UNISEX RESTROOM AND CHASE AREA. THESE AREAS ARE NATURALLY VENTILATED. AN OPEN BREEZEWAY SHELTERS A VENDING AREA, THE ENTRANCES INTO THE RESTROOMS, AND A HIGH-LOW WATER FOUNTAIN. ALL WORK MUST BE PERFORMED PER CODE. ADA COMPLIANCE MUST BE MAINTAINED.

JAMES H. PETERSON IV, P.E.
DESIGNER

CN539-TA01
CONSULTANT CONTRACT No.

NOVEMBER 11TH 2024 100% PLANS
INITIAL ISSUE DATE

SHEET NUMBER
G001

LS001
A001
A101
A102
A201
A301
A302-303
A401
A402-403
A601

C003
C004
C005
C201-202
C301
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SHEET TITLE
COVER PAGE

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LEGENDS & LOUVER DETAILS
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GENERAL NOTES
PROJECT LOCATION MAP
TYPICAL SECTIONS
DEMOLITION & EROSION CONTROL PLAN
SITE PLAN NORTH SIDE PICNIC AREA
PROPOSED UTILITY PLAN NORTH SIDE PICNIC AREA
DRIVEWAY PLAN & PROFILE
SITE PLAN TURN LANES
ADA KAYAK LAUNCH PLAN & PROFILE
LANDSCAPE PLAN
NORTH PICNIC AREA GRADING PLAN
NORTH PARKING LOT GRADING PLAN
NORTH DRIVEWAY GRADING PLAN
ADA KAYAK LAUNCH GRADING PLAN
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WEST BOUND TURN LANE CROSS SECTIONS
MULTI-USE PATH CROSS SECTIONS
CONCRETE PATH EXTENSION CROSS SECTIONS
DRAINAGE PLAN TURN LANES

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S301
S302-303
S401-402
S511
S521
S701-702
S907

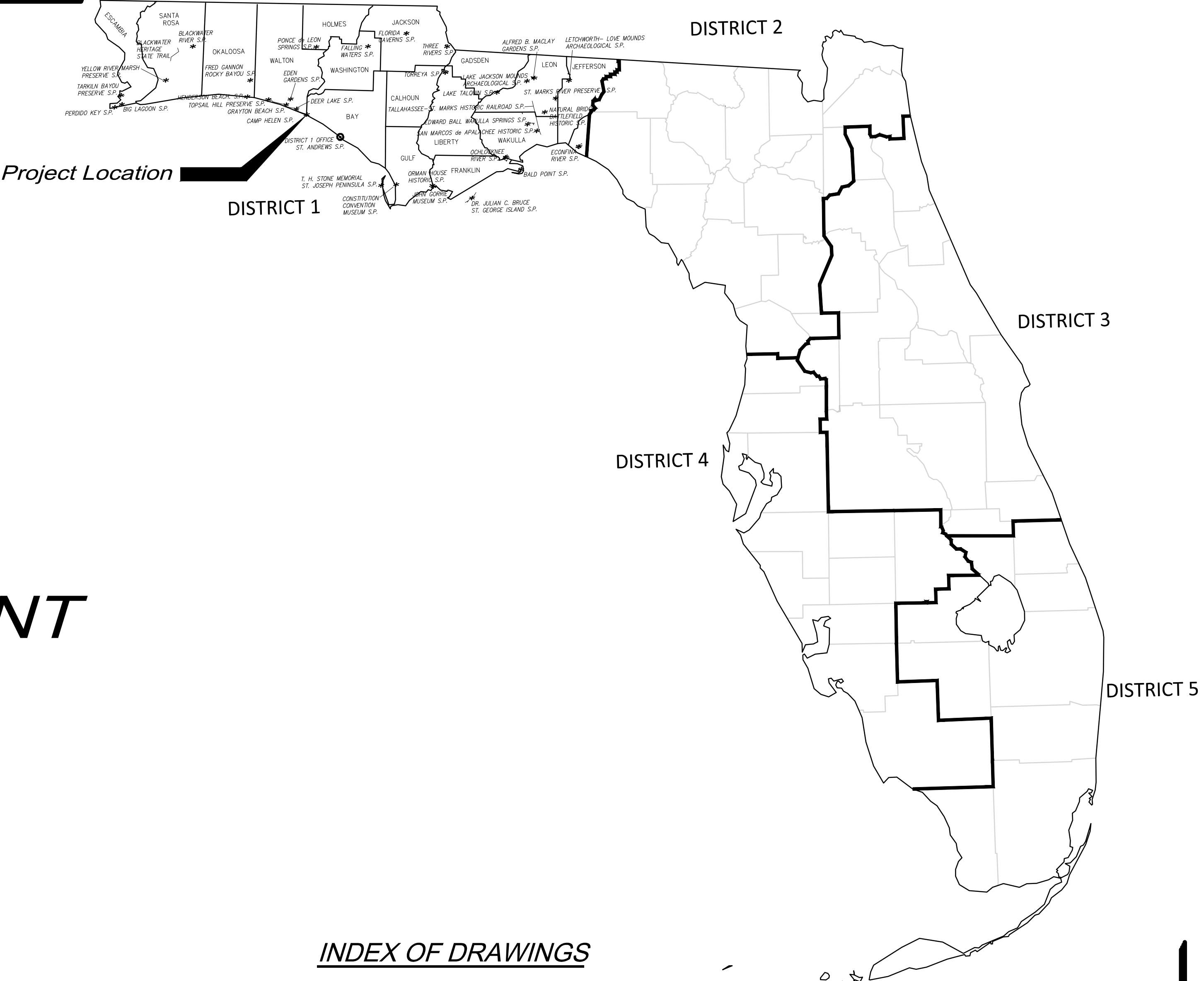
TURN LANE UTILITY PLAN
SIGNAGE & PAVEMENT MARKING PLAN
TRAFFIC CONTROL PLAN
CONSTRUCTION DETAILS
EROSION CONTROL DETAILS

COVER SHEET
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RESTROOM GROUND & ROOF FRAMING PLANS AT PICNIC AREA
SITE RAMPS & STAIRS AT PICNIC AREA
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KAYAK LAUNCH
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RAMP SECTIONS
TYPICAL SCHEDULE
TYPICAL FOUNDATIONS & SLAB ON GRADE DETAILS
TYPICAL MASONRY DETAILS
TYPICAL WOOD DETAILS
WOOD DOCK & DECK DETAILS

M100
MECHANICAL NOTES, SCHEDULE, & PLAN

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DETAILS AND SCHEDULES
SITE PLAN AND ONE LINE
POWER & LIGHTING ENLARGED PLANS

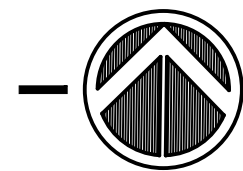
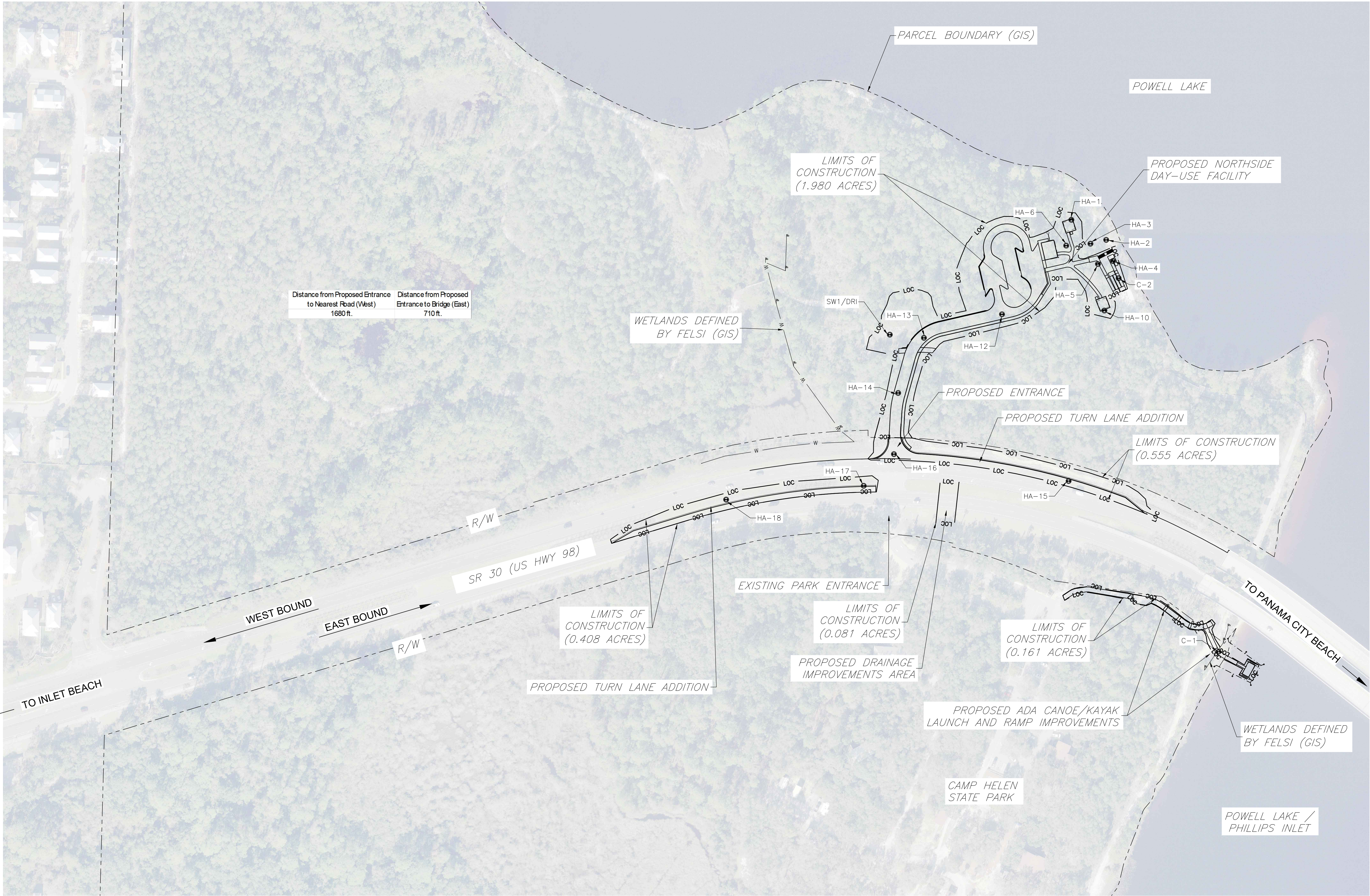
P100-101
P200
P300
P400
PLUMBING NOTES AND LEGEND
PLUMBING NEW WORK PLAN
PLUMBING DETAILS
PLUMBING RISERS



CAMP HELEN STATE PARK
PARK IMPROVEMENT

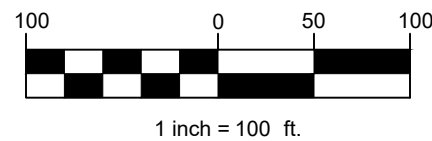


J:\PETERSON November 15, 2024 P:\Project\24-548 BDC Camp Helen State Park\GIS\swing\GIS\Map\004 Project Location Map.dwg



PROJECT LOCATION MAP

SCALE: 1" = 100'



NOT FOR CONSTRUCTION

LINETYPE LEGEND	
— W —	WETLAND LINE
— LOC —	LIMITS OF CONSTRUCTION
●	GEOTECHNICAL BORINGS

CAMP HELEN STATE PARK

PROJECT LOCATION MAP

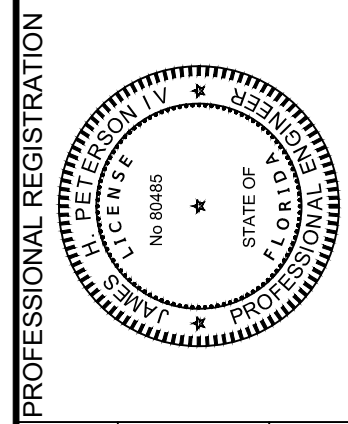
PARK IMPROVEMENT

SHEET TITLE

PROJECT TITLE

SHEET NO.

C004



PROFESSIONAL REGISTRATION

DESIGNER: SWU
DRAWN BY: KOP
REVIEWED BY: JHP

CONSULTANT:

George & Associates
Consulting Engineers, Inc.
CIVIL - ENVIRONMENTAL - LANDSCAPE ARCHITECTURE - SURVEYING - LAND USE
1907 Commonwealth Lakeside Drive, Suite 200 Tallahassee, FL 32303
PHONE: 850/521-0344 - FAX: 850/521-0345

ISSUE DATE: 11/11/2024 100% PLANS
COMP. FILE NO.: 21-5486
STATE PROJECT NO.: 61307C-N3803

SYMBOL

REVISION

DATE

SYMBOL

REVISION

DATE

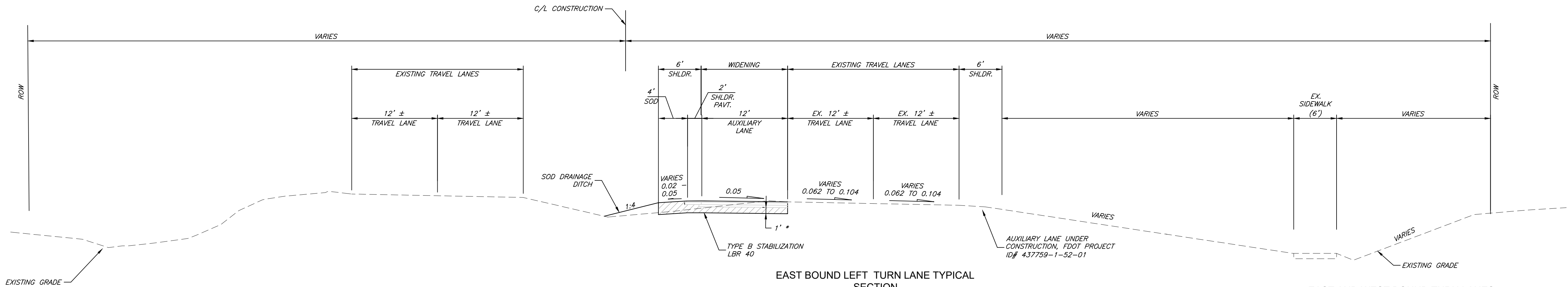
SYMBOL

REVISION

DATE

Department of Environmental Protection
Division of Recreation and Parks
Bureau of Design and Construction
3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157

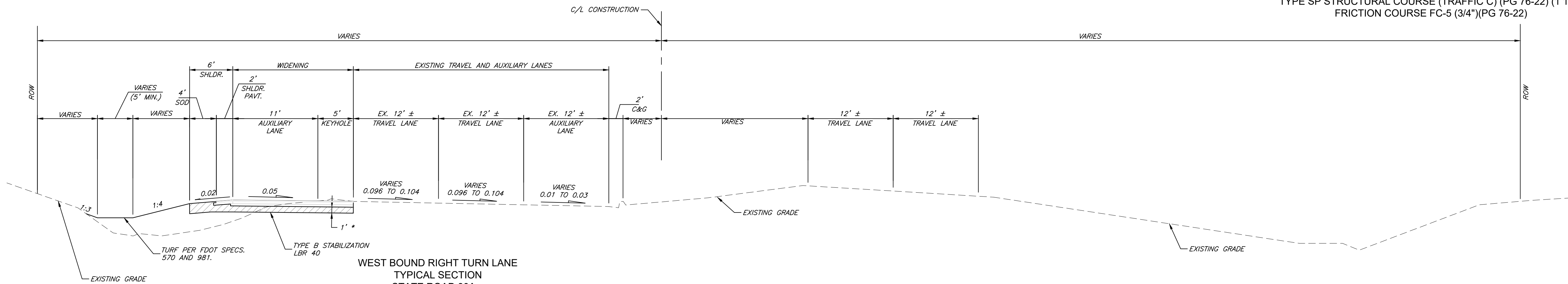
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EAST BOUND LEFT TURN LANE TYPICAL SECTION
STATE ROAD 30A
STA. 143+33.78 TO STA. 148+63.00
(LOOKING EAST)

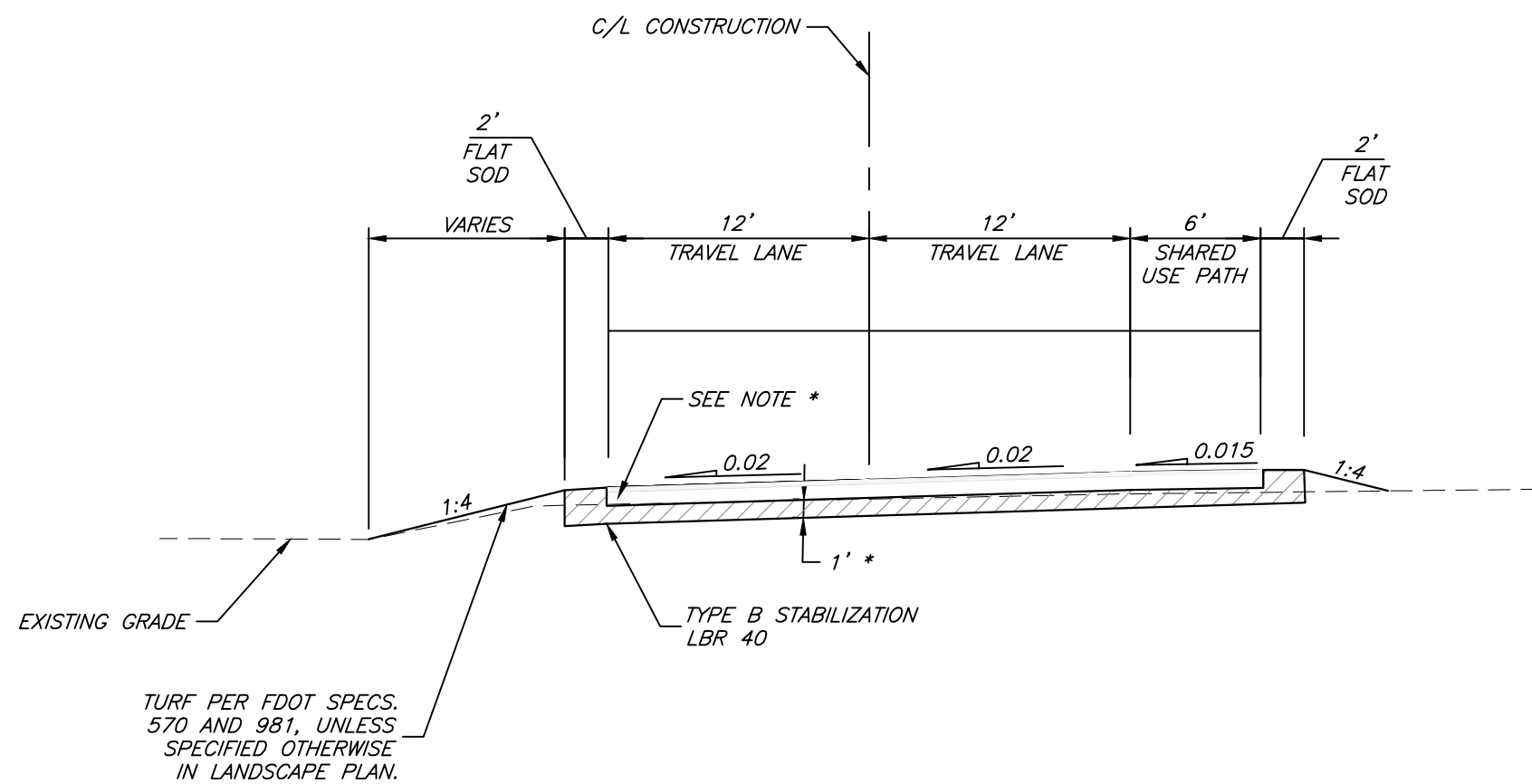
EAST AND WEST BOUND TURN LANES
OPTIONAL BASE GROUP 9
TYPE SP STRUCTURAL COURSE (TRAFFIC C) (PG 76-22) (3")
FRICTION COURSE FC-5 (3/4") (PG 76-22)

SHOULDER PAVEMENT
OPTIONAL BASE GROUP 1
TYPE SP STRUCTURAL COURSE (TRAFFIC C) (PG 76-22) (1 1/2")
FRICTION COURSE FC-5 (3/4") (PG 76-22)

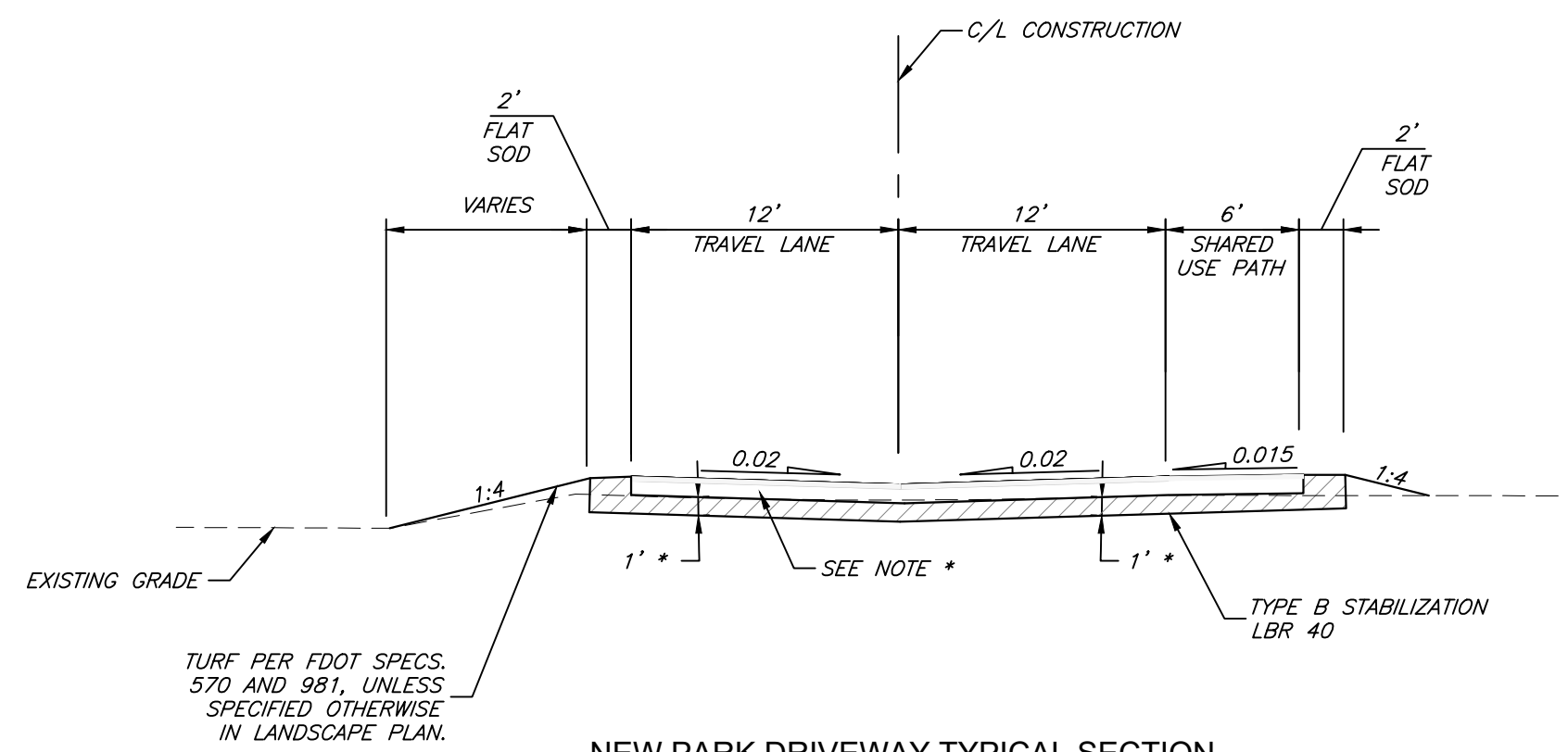


WEST BOUND RIGHT TURN LANE TYPICAL SECTION
STATE ROAD 30A
STA. 149+12.00 TO STA. 153+93.00
(LOOKING EAST)

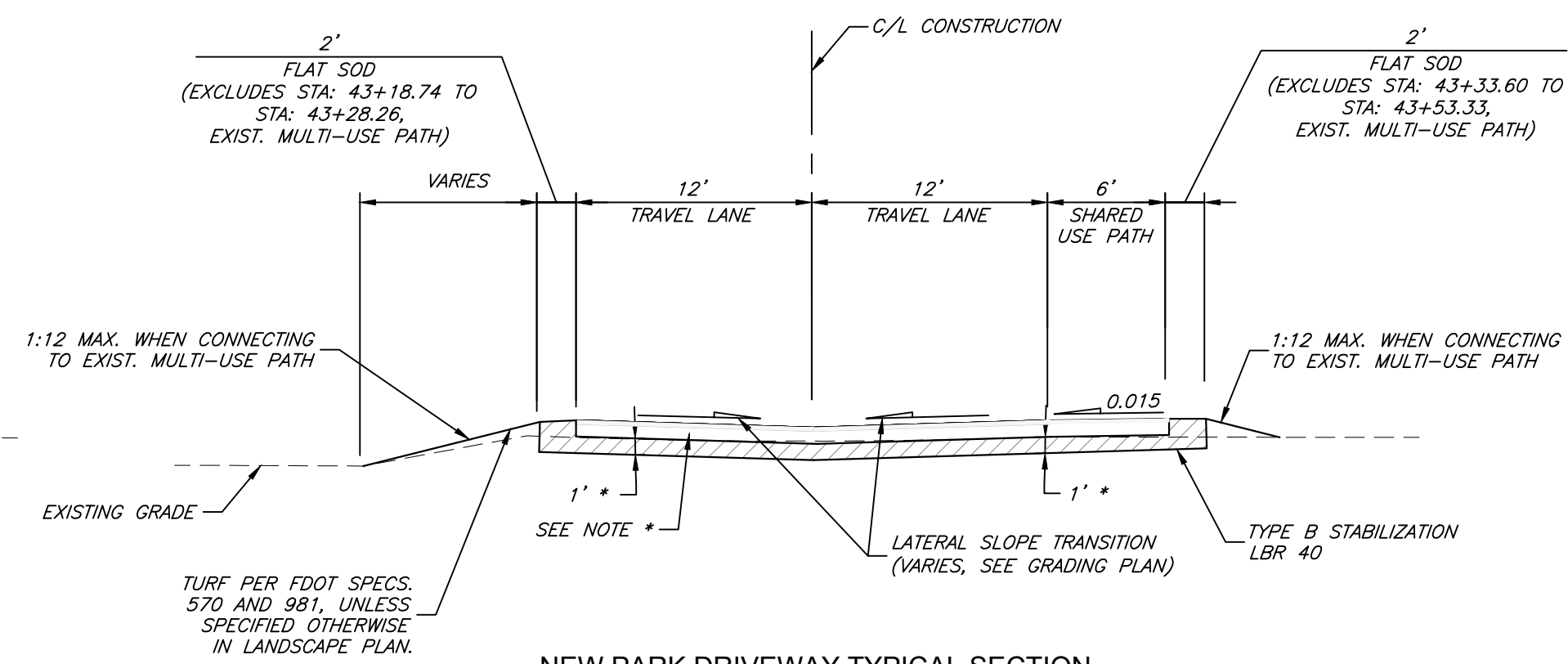
NOTE:
* DRIVEWAY AND PARKING AREA TO HAVE A SP 12.5 ASPHALTIC CONCRETE WEARING SURFACE WITH A MINIMUM THICKNESS OF 2 INCHES. BASE COURSE MATERIAL SHALL BE EITHER LIME ROCK OR GRADED AGGREGATE BASE (GAB) WITH A MINIMUM THICKNESS OF 6 INCHES. THE CONTRACTOR SHALL USE GAB IN LIEU OF LIME ROCK IN ALL AREAS WITHIN 24 INCHES OF WATER TABLE PER FINDINGS OF GEOTECH REPORT.



NEW PARK DRIVEWAY TYPICAL SECTION
OPTIONAL BASE GROUP 4
TYPE SP STRUCTURAL COURSE (TRAFFIC B) (2")
STA. 43+52.00 TO STA. 45+46.00



NEW PARK DRIVEWAY TYPICAL SECTION
OPTIONAL BASE GROUP 4
TYPE SP STRUCTURAL COURSE (TRAFFIC B) (2")
STA. 41+88.34 TO STA. 43+09.05
STA. 43+39.50 TO STA. 43+52.00



NEW PARK DRIVEWAY TYPICAL SECTION
OPTIONAL BASE GROUP 4
TYPE SP STRUCTURAL COURSE (TRAFFIC B) (2")
STA. 43+09.05 TO STA. 43+39.50

TYPICAL SECTIONS

NOT FOR CONSTRUCTION

DATE	REVISION	SYMBOL	DATE	REVISION	SYMBOL	ISSUE DATE: 11/11/2024	100% PLANS	COMP. FILE NO. 21-5436	STATE PROJECT NO. 61307C-N3903	DESIGNER: SMU	DRAWN BY: TJM	REVIEWED BY: JHP	CONSULTANT:
Department of Environmental Protection Division of Recreation and Parks Bureau of Design and Construction 3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157										George & Associates Consulting Engineers, Inc. 1907 Commonwealth Lane, Tallahassee, FL 32303 PHONE: 850/5210344 - FAX: 850/5210345			
CAMP HELEN STATE PARK										TYPICAL SECTIONS			
PARK IMPROVEMENT										PROJECT TITLE			
SHEET NO.										C005			

DEMO AND EROSION CONTROL NOTES:

1. THIS SITE MAY CONTAIN EXISTING UTILITY LINES, UTILITY STRUCTURES AND MISCELLANEOUS UTILITY EQUIPMENT THAT MAY NOT HAVE BEEN SURVEYED AND IN CONFLICT WITH PROPOSED CONSTRUCTION. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO LOCATE ALL UTILITIES WITHIN PROJECT AREA PRIOR TO CONSTRUCTION.
2. ALL UTILITIES MUST REMAIN IN OPERATION THROUGHOUT CONSTRUCTION ACTIVITIES FOR THIS PROJECT. FOR ANY ANTICIPATED DISRUPTION IN SERVICE, COORDINATE WITH OWNER AND UTILITY PROVIDER TWO WEEKS IN ADVANCE.
3. CONTRACTOR TO COORDINATE WITH BDC PROJECT MANAGER, UTILITY PROVIDER(S) AND CIVIL ENGINEER FOR ANY AND ALL UTILITIES THAT MAY BE IN CONFLICT WITH PROPOSED CONSTRUCTION ACTIVITIES.
4. WHERE EXISTING ITEMS SUCH AS ASPHALT, CONCRETE CURB AND GUTTER, ETC. ARE SHOWN TO BE REMOVED, THESE ITEMS SHALL BE SAWCUT.
5. CONTRACTOR TO VERIFY ALL DEPTHS AND LOCATIONS OF EXISTING UNDERGROUND UTILITIES PRIOR TO CONSTRUCTION.
6. CONTRACTOR RESPONSIBLE TO ADJUST ALL UTILITIES AND VALVE BOXES TO FINISH GRADE.
7. CONTRACTOR RESPONSIBLE TO DEFLECT ANY UTILITIES NECESSARY TO CONSTRUCT PROPOSED IMPROVEMENTS, PER MANUFACTURED RECOMMENDED TOLERANCES.
8. CONTRACTOR RESPONSIBLE FOR ANY DAMAGE TO EXISTING INFRASTRUCTURE, TREES, LANDSCAPE OR ANY OTHER MISC ITEMS THAT ARE TO REMAIN. CONTRACTOR SHALL RESTORE TO PRE-DEVELOPMENT CONDITION.
9. AN EFFORT HAS BEEN MADE TO IDENTIFY ALL UTILITIES IN THE AREA INCLUDING COORDINATING WITH UTILITY OWNERS. THE DEPICTED UTILITIES SHOULD NOT BE CONSIDERED THE EXTENT OF UTILITIES IN THE PROJECT AREA, AND ALL REQUIRED DUE CAUTION, SUCH AS AN 811 TICKET AND ADDITIONAL QUALITY LEVEL SUE 'A' SURVEY, SHOULD BE TAKEN PRIOR TO EXCAVATION TO VERIFY UTILITY EXTENTS.
10. ALL SIGNAGE WITHIN LIMITS OF CONSTRUCTION THAT WILL BE IMPACTED BY THE WORK SHALL BE REMOVED IN A MANNER THAT DOES NOT DAMAGE THE SIGNAGE OR POSTS. COORDINATE ALL REINSTATEMENT OF SIGNAGE AND LOCATION WITH BDC PROJECT MANAGER AND PARK MANAGER. SIGNAGE TO BE REUSED SHALL BE STORED IN A MANNER THAT IS SAFE AND DOES NOT DAMAGE THE SIGNS. ANY DAMAGED SIGNAGE PROPOSED FOR REUSE SHALL BE REPLACED IN-KIND BY THE CONTRACTOR. BDC PROJECT MANAGER AND PARK MANAGER SHALL APPROVE OF ALL SIGNAGE TO BE REPLACED AND THE PROPOSED LOCATION FOR SIGNAGE. SIGNAGE NOT APPROVED FOR REUSE OR CLAIMED BY THE PARK SHALL BECOME THE CONTRACTOR'S RESPONSIBILITY FOR PROPER DISPOSAL.
11. COORDINATE ALL DEMOLITION ACTIVITIES WITH BDC PROJECT MANAGER AND PARK STAFF. PARK SHALL RETAIN RIGHT OF REFUSAL FOR ANY MATERIAL CALLED OUT FOR DEMOLITION. RETURN IN GOOD WORKING ORDER ANY MATERIALS REQUESTED BY THE BDC PROJECT MANAGER OR PARK STAFF AS SALVAGED MATERIAL. LAWFULLY DISPOSE, AT EXPENSE OF THE CONTRACTOR, ALL REMAINING ITEMS CALLED OUT FOR DEMOLITION.

SEDIMENTATION and EROSION CONTROL LEGEND

SYMBOL	DESCRIPTION
Fr	FILTER RING
Sd1	SEDIMENT BARRIER
Sd2	INLET SEDIMENT TRAP
St	STORM DRAIN OUTLET PROTECTION
Co	CONSTRUCTION EXIT
Ds2	DISTURBED AREA STABILIZATION WITH SEEDING ONLY
Ds3	DISTURBED AREA STABILIZATION WITH PERMANENT VEGETATION
Ds4	DISTURBED AREA STABILIZATION WITH SODDING
Du	DUST CONTROL ON DISTURBED AREAS
Ch	CHANNEL STABILIZATION
Cr	CONSTRUCTION ROAD STABILIZATION

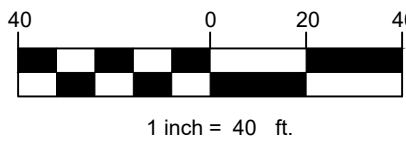
LEGEND

SB	SEDIMENT BARRIER	Tree to be removed
TB	TREE TRUNK PROTECTION	Tree to be remain/ receive protection
Floating Turbidity Barrier	DEMOLITION	Soil Boring Test Hole
DEMOLITION	DEMOLITION	
DEMOLITION	DEMOLITION	

DEMOLITION AND EROSION CONTROL PLAN

SCALE: 1" = 40'

NOT FOR CONSTRUCTION



DEMOLITION AND EROSION CONTROL PLAN

PARK IMPROVEMENT

CAMP HELEN STATE PARK

SHEET TITLE

PROJECT TITLE

SHEET NO.

C201

Department of Environmental Protection

Division of Recreation and Parks

Bureau of Design and Construction

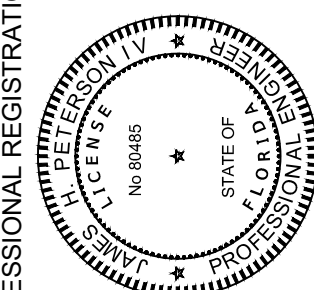
3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157

George & Associates

Consulting Engineers, Inc.

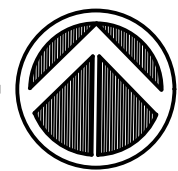
1907 Commonwealth Boulevard, Tallahassee, FL 32303

PHONE: 850/5210344 - FAX: 850/5210345



James H. Peterson, P.E. # 88405

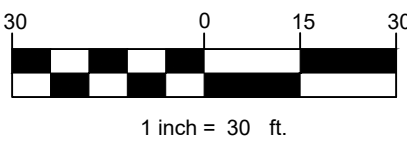
DD000 November 9, 2024 P:\Projects\21-5436 BSC Camp Helen State Park\Drawings\C202 Demolition and Erosion Control\Plan.dwg



DEMOLITION AND EROSION CONTROL PLAN

SCALE: 1" = 30'

NOT FOR CONSTRUCTION



LEGEND

SB

—

SEDIMENT BARRIER

TB

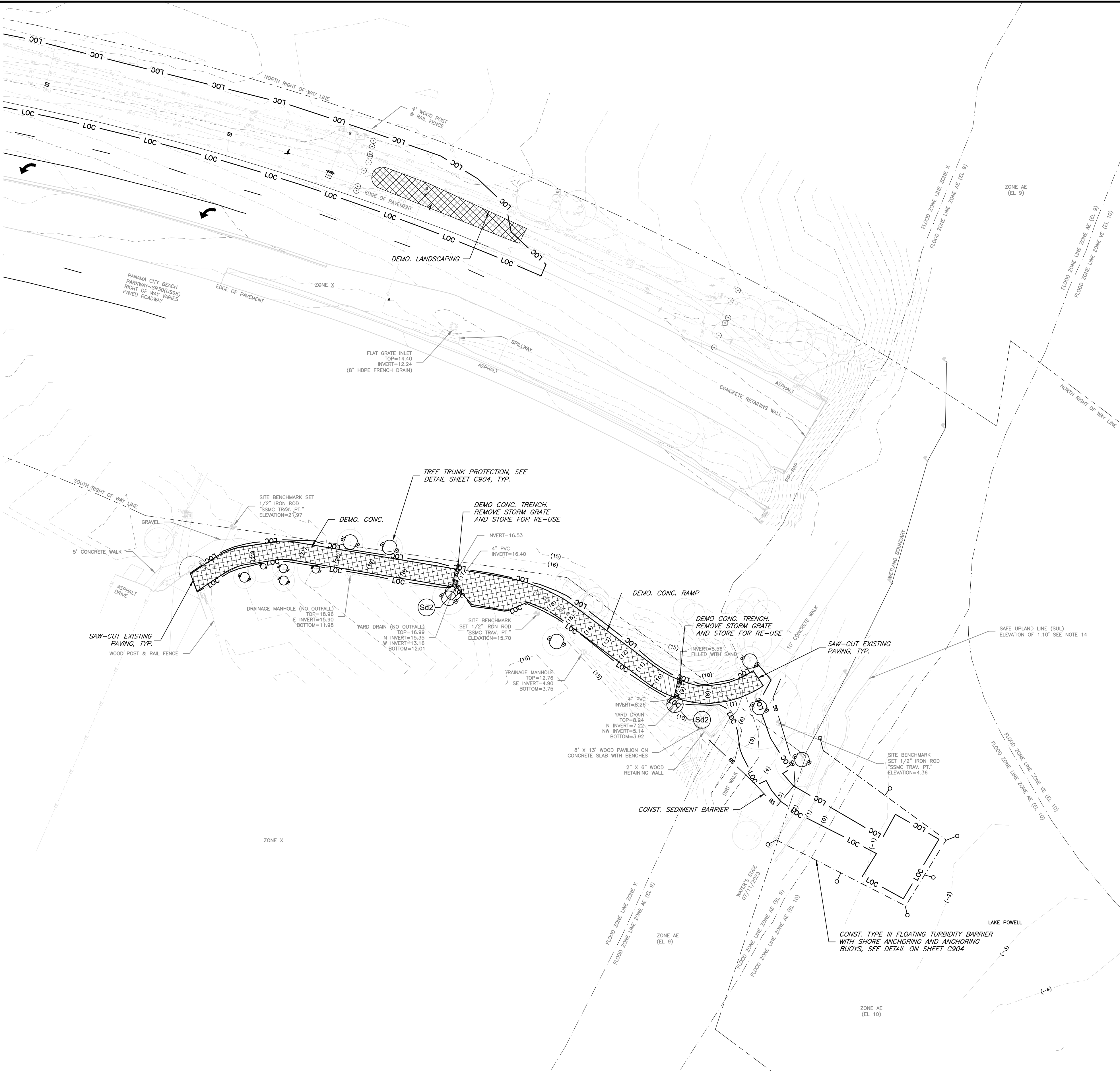
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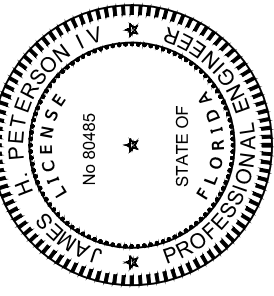
TREE TRUNK PROTECTION

—

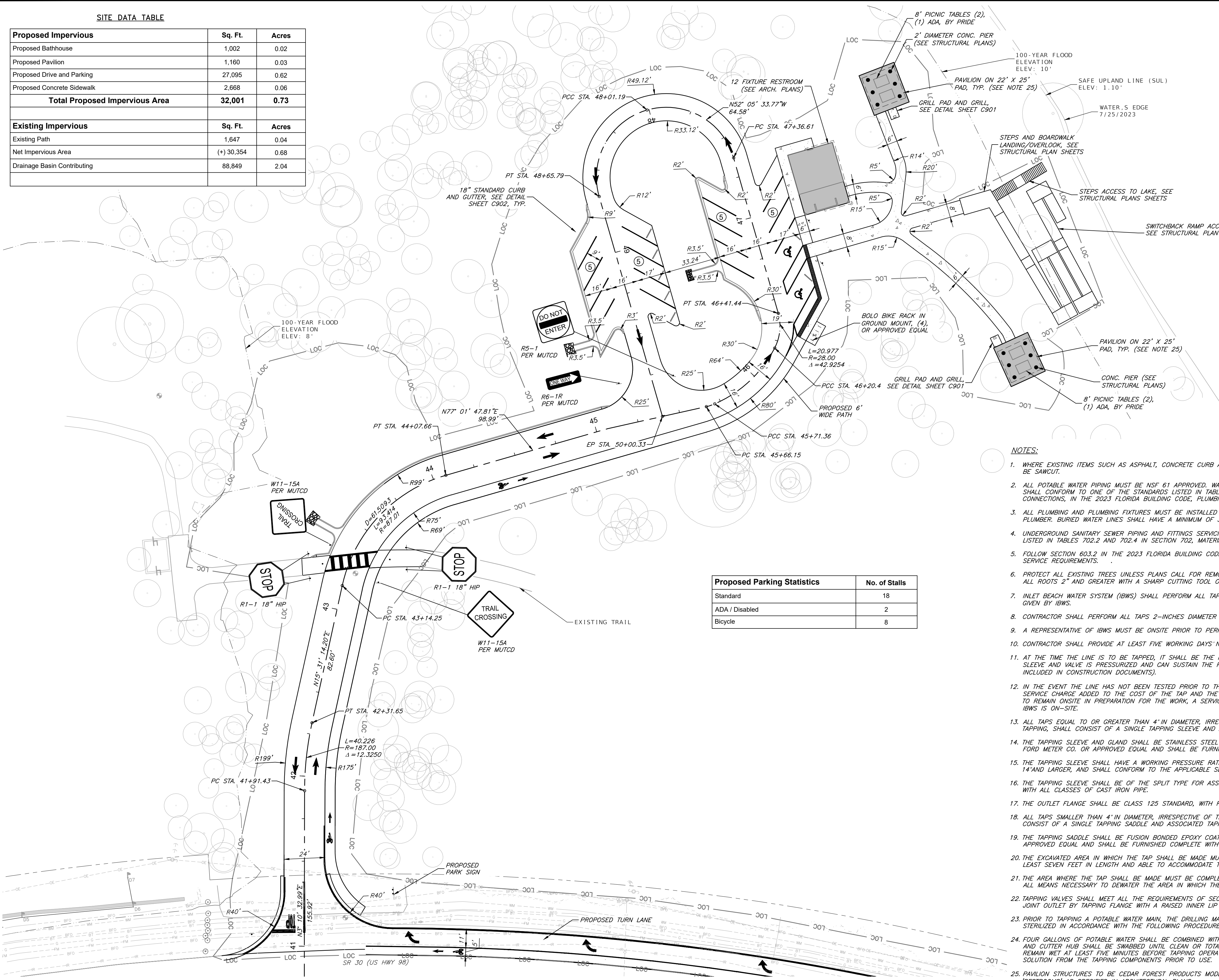
FLOATING TURBIDITY BARRIER

DEMO



CAMP HELEN STATE PARK												PROFESSIONAL REGISTRATION											
DEMOLITION AND EROSION CONTROL PLAN																							
SHEET TITLE												JAMES H. PETERSON IV State of Florida P.E. # 88485											
PROJECT TITLE												PARK IMPROVEMENT											
C202												George & Associates Consulting Engineers, Inc. ONE COMMONWEALTH LANE, SUITE 200 TALLAHASSEE, FLORIDA 32303 PHONE (850) 210-0344 - FAX (850) 210-0345											
SHEET NO.												CONSULTANT :											
DESIGNER : SMU												ISSUE DATE: 11/11/2024 100% PLANS											
DRAWN BY: TJM												COMP. FILE NO: 21-5436											
REVIEWED BY: JHP												STATE PROJECT NO: 61307C-N3803											
Department of Environmental Protection												Division of Recreation and Parks											
Bureau of Design and Construction												3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157											
DATE												REVISION											
SYMBOL												SYMBOL											

SITE DATA TABLE		
Proposed Impervious	Sq. Ft.	Acres
Proposed Bathhouse	1,002	0.02
Proposed Pavilion	1,160	0.03
Proposed Drive and Parking	27,095	0.62
Proposed Concrete Sidewalk	2,668	0.06
Total Proposed Impervious Area	32,001	0.73
Existing Impervious	Sq. Ft.	Acres
Existing Path	1,647	0.04
Net Impervious Area	(+) 30,354	0.68
Drainage Basin Contributing	88,849	2.04



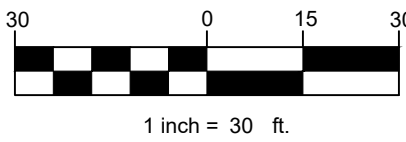
LEGEND

- PROPOSED ASPHALT PAVING
- PROPOSED CONCRETE SIDEWALK
- PROPOSED BUILDING
- SUE TEST HOLE
- YARD HYDRANT
- BACKFLOW PREVENTER
- VALVE
- REDUCER
- WATER METER
- VEHICLE PARKING COUNT

NOTES:

- WHERE EXISTING ITEMS SUCH AS ASPHALT, CONCRETE CURB AND GUTTER, ETC. ARE SHOWN TO BE REMOVED. THESE ITEMS SHALL BE SAWCUT.
- ALL POTABLE WATER PIPING MUST BE NSF 61 APPROVED. WATER SERVICE PIPING, DISTRIBUTION PIPING AND PLUMBING FIXTURES SHALL CONFORM TO ONE OF THE STANDARDS LISTED IN TABLES 605.3, 605.4, 605.5 IN SECTION 605, MATERIALS, JOINTS AND CONNECTIONS, IN THE 2023 FLORIDA BUILDING CODE, PLUMBING, 8TH EDITION.
- ALL PLUMBING AND PLUMBING FIXTURES MUST BE INSTALLED OR THE INSTALLATION MUST BE SUPERVISED BY A FLORIDA LICENSED PLUMBER. BURIED WATER LINES SHALL HAVE A MINIMUM OF 36" OF COVER.
- UNDERGROUND SANITARY SEWER PIPING AND FITTINGS SERVICING THE RESTROOM SHALL CONFORM TO ONE OF THE STANDARDS LISTED IN TABLES 702.2 AND 702.4 IN SECTION 702, MATERIALS, IN THE 2023 FLORIDA BUILDING CODE, PLUMBING, 8TH EDITION.
- FOLLOW SECTION 603.2 IN THE 2023 FLORIDA BUILDING CODE, PLUMBING, 8TH EDITION FOR SEPARATION OF SEWER AND WATER SERVICE REQUIREMENTS.
- PROTECT ALL EXISTING TREES UNLESS PLANS CALL FOR REMOVAL. IF TREE ROOTS ARE ENCOUNTERED DURING EXCAVATION CUT ALL ROOTS 2" AND GREATER WITH A SHARP CUTTING TOOL OR SAW. DO NOT DAMAGE THE TREE TRUNK OR BARK.
- INLET BEACH WATER SYSTEM (IBWS) SHALL PERFORM ALL TAPS GREATER THAN 2" IN DIAMETER, UNLESS WRITTEN PERMISSION IS GIVEN BY IBWS.
- CONTRACTOR SHALL PERFORM ALL TAPS 2-INCHES DIAMETER AND LESS.
- A REPRESENTATIVE OF IBWS MUST BE ONSITE PRIOR TO PERFORMING ANY AND ALL TAPS.
- CONTRACTOR SHALL PROVIDE AT LEAST FIVE WORKING DAYS' NOTICE TO IBWS PRIOR TO PERFORMING THE WORK.
- AT THE TIME THE LINE IS TO BE TAPPED, IT SHALL BE THE RESPONSIBILITY OF CONTRACTOR TO ENSURE THAT THE TAPPING SLEEVE AND VALVE IS PRESSURIZED AND CAN SUSTAIN THE PRESSURE TEST (SEE SECTION 6.3.7 OF IBWS SPECIFICATION, INCLUDED IN CONSTRUCTION DOCUMENTS).
- IN THE EVENT THE LINE HAS NOT BEEN TESTED PRIOR TO THE ARRIVAL OF IBWS AT THE JOB SITE, THERE SHALL BE A \$50.00 SERVICE CHARGE ADDED TO THE COST OF THE TAP AND THE TAP SHALL BE RESCHEDULED. SHOULD CONTRACTOR PREFER IBWS TO REMAIN ONSITE IN PREPARATION FOR THE WORK, A SERVICE CHARGE EQUAL TO \$50.00 AN HOUR SHALL APPLY SO LONG AS IBWS IS ON-SITE.
- ALL TAPS EQUAL TO OR GREATER THAN 4" IN DIAMETER, IRRESPECTIVE OF THE DIAMETER OF THE LINE TO WHICH YOU ARE TAPPING, SHALL CONSIST OF A SINGLE TAPPING SLEEVE AND ASSOCIATED TAPPING VALVE.
- THE TAPPING SLEEVE AND GLAND SHALL BE STAINLESS STEEL WRAPAROUND 'FAST STYLE', AND SHALL BE AS MANUFACTURED BY FORD METER CO. OR APPROVED EQUAL AND SHALL BE FURNISHED COMPLETE WITH ALL NECESSARY ACCESSORIES.
- THE TAPPING SLEEVE SHALL HAVE A WORKING PRESSURE RATING OF 200 PSI FOR SIZES 4" THROUGH 12" AND 150 PSI FOR SIZES 14" AND LARGER, AND SHALL CONFORM TO THE APPLICABLE SECTIONS OF ANWIA STANDARD C110 OF LATEST REVISION.
- THE TAPPING SLEEVE SHALL BE OF THE SPLIT TYPE FOR ASSEMBLY ON THE PIPE AND THE SLEEVE SHALL BE SIZED FOR USE WITH ALL CLASSES OF CAST IRON PIPE.
- THE OUTLET FLANGE SHALL BE CLASS 125 STANDARD, WITH RECESS FOR STANDARD TAPPING VALVES.
- ALL TAPS SMALLER THAN 4" IN DIAMETER, IRRESPECTIVE OF THE DIAMETER OF THE LINE TO WHICH YOU ARE TAPPING, SHALL CONSIST OF A SINGLE TAPPING SADDLE AND ASSOCIATED TAPPING VALVE.
- THE TAPPING SADDLE SHALL BE FUSION BONDED EPOXY COATED, AND SHALL BE AS MANUFACTURED BY FORD METER CO. OR APPROVED EQUAL AND SHALL BE FURNISHED COMPLETE WITH ALL NECESSARY ACCESSORIES.
- THE EXCAVATED AREA IN WHICH THE TAP SHALL BE MADE MUST BE A MINIMUM OF 4' BELOW THE BOTTOM OF THE VALVE, AT LEAST SEVEN FEET IN LENGTH AND ABLE TO ACCOMMODATE TWO PEOPLE WORKING.
- THE AREA WHERE THE TAP SHALL BE MADE MUST BE COMPLETELY DRY. IT IS THE RESPONSIBILITY OF CONTRACTOR TO PURSUE ALL MEANS NECESSARY TO DEWATER THE AREA IN WHICH THE TAP IS TO BE MADE.
- TAPPING VALVES SHALL MEET ALL THE REQUIREMENTS OF SECTION 6.3 OF IBWS SPECIFICATIONS AND SHALL BE A MECHANICAL JOINT OUTLET BY TAPPING FLANGE WITH A RAISED INNER LIP FOR ALIGNMENT WITH THE TAPPING SLEEVE.
- PRIOR TO TAPPING A POTABLE WATER MAIN, THE DRILLING MACHINE'S PILOT DRILL, SHELL CUTTER AND CUTTER HUB SHALL BE STERILIZED IN ACCORDANCE WITH THE FOLLOWING PROCEDURE:
 - FOUR GALLONS OF POTABLE WATER SHALL BE COMBINED WITH 8 OZ. OF SODIUM HYPOCHLORITE; THE PILOT DRILL, SHELL CUTTER AND CUTTER HUB SHALL BE SWABBED UNTIL CLEAN OR TOTALLY IMMERSER IN THE STERILIZING SOLUTION AND ALLOWED TO REMAIN WET AT LEAST FIVE MINUTES BEFORE TAPPING OPERATION COMMENCES. IT IS NOT NECESSARY TO RINSE THE STERILIZING SOLUTION FROM THE TAPPING COMPONENTS PRIOR TO USE.
- PAVILION STRUCTURES TO BE CEDAR FOREST PRODUCTS MODEL #LB2020 OR APPROVED EQUAL. METAL ROOFING SHALL MATCH 'RESTROOMS' AS SPECIFIED IN ARCHITECTURAL PLANS.

Proposed Parking Statistics	No. of Stalls
Standard	18
ADA / Disabled	2
Bicycle	8



NOT FOR CONSTRUCTION



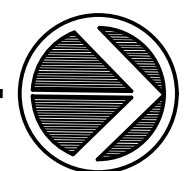
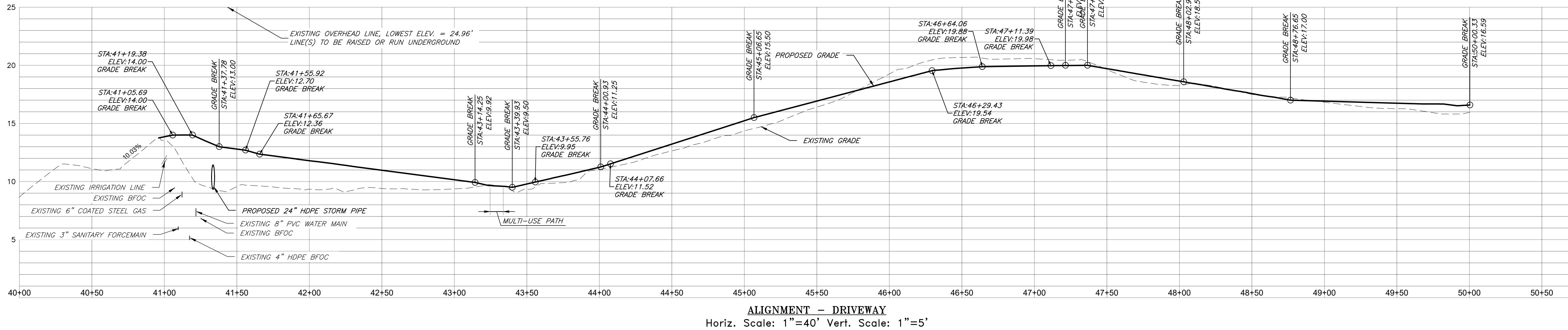
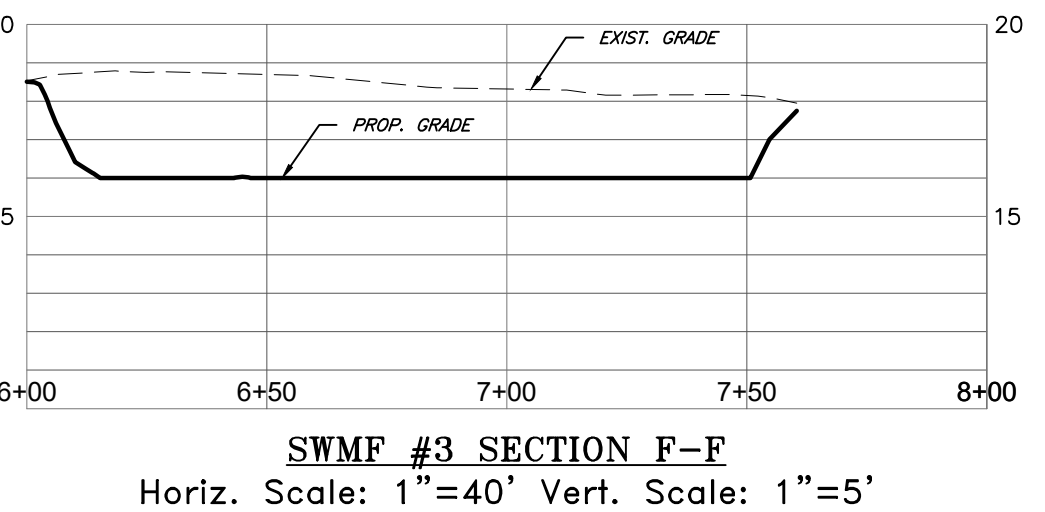
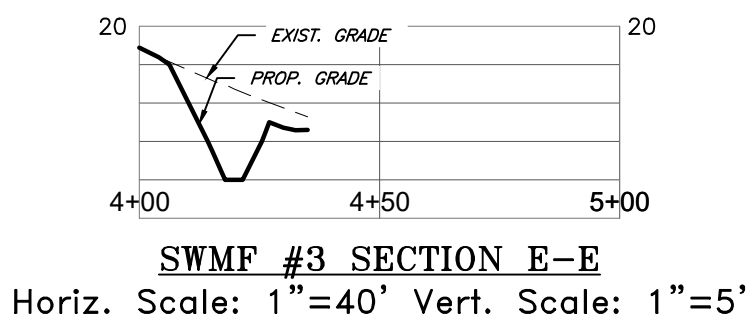
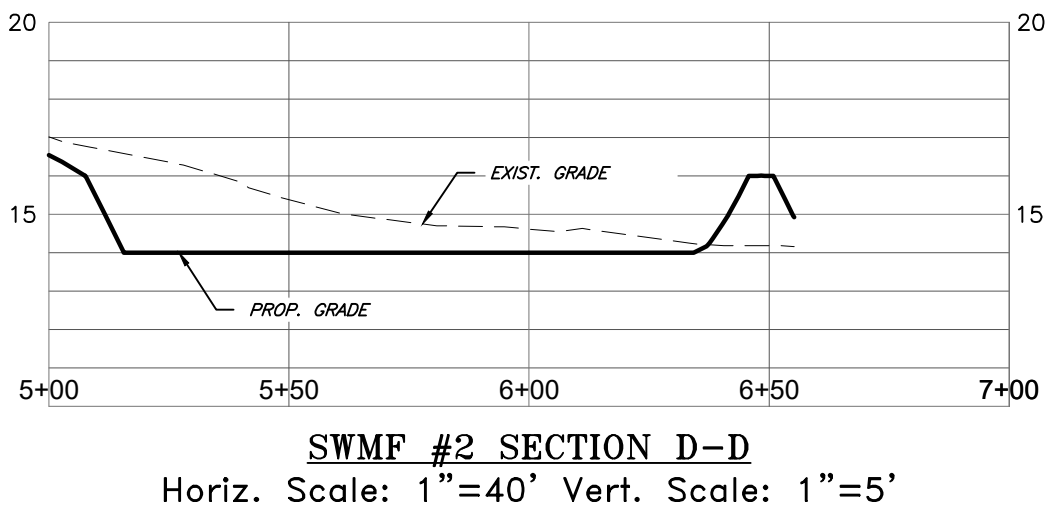
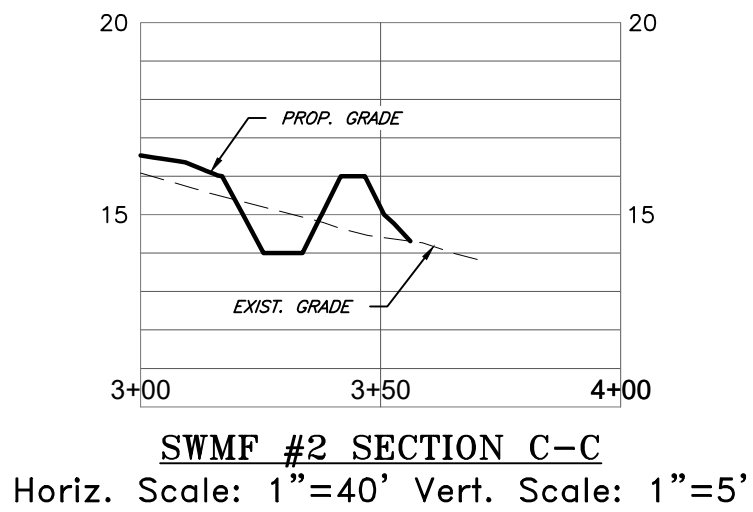
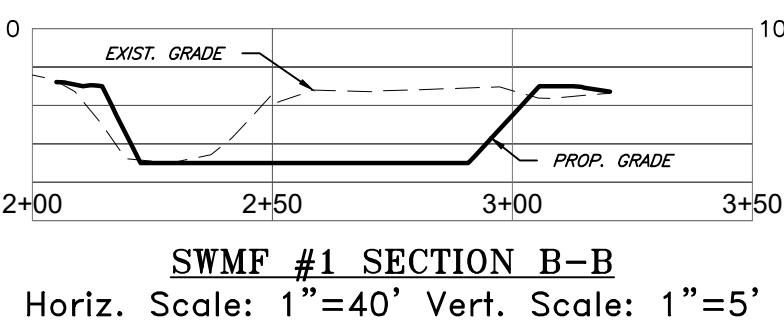
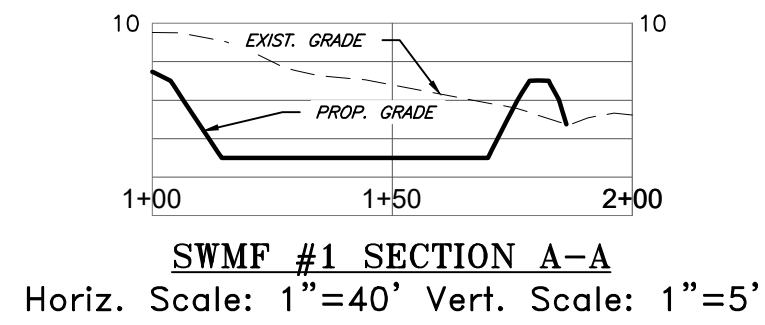
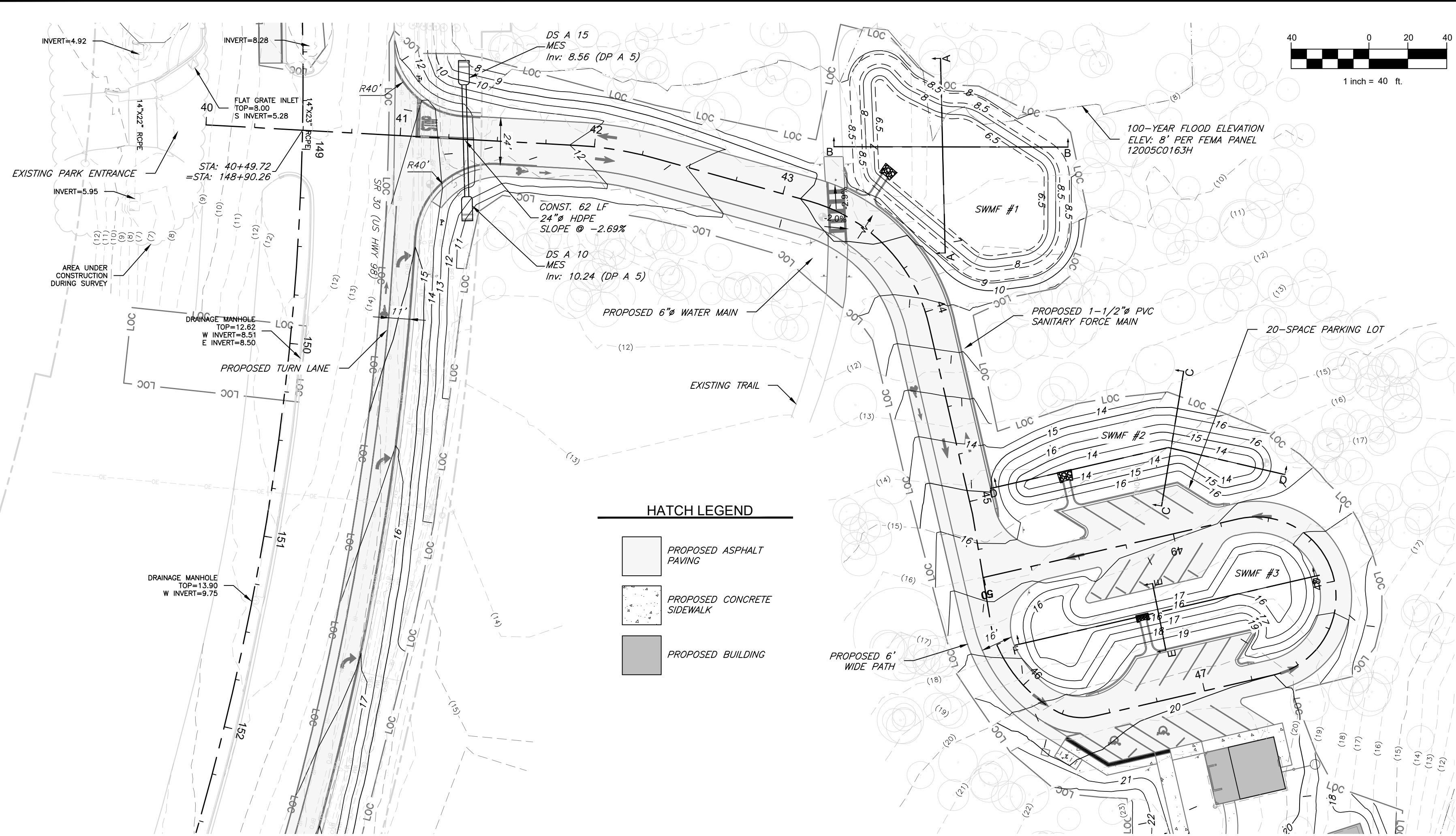
SITE PLAN NORTH SIDE PICNIC AREA

SCALE: 1" = 30'

J:\PROJECTS\2024\15_2024_P\Progress\2-5-2024_BDC Camp Helen State Park\Drawings\Civil\5 Site Plan - Plan and Profile\C301 Site Plan North Side Picnic Area.dwg

DATE	REVISION	SYMBOL	DATE	REVISION	SYMBOL	ISSUE DATE: 11/11/2024	100% PLANS	DESIGNER: SMU	PROFESSIONAL REGISTRATION	CAMP HELEN STATE PARK	SHEET TITLE	SHEET NO.
						COMP. FILE No.: 21-5436		DRAWN BY: SMU		SITE PLAN NORTH SIDE PICNIC AREA	PROJECT TITLE	C301
						STATE PROJECT No.: 61307C-N3903	REVIEWED BY: JHP	CONSULTANT: George & Associates Consulting Engineers, Inc. 3900 Commonwealth Boulevard, Tallahassee, FL 32303 PHONE: 850/5210334 FAX: 850/5210335				

S:\SAMSER November 11, 2024 P:\projects\21-5436 BDC Camp Helen State Park\Drawings\Consult\Site Plan - Plan and Profile\C303 Driveway Plan and Profile.dwg



DRIVEWAY PLAN AND PROFILE

SCALE: 1" = 40'

NOT FOR CONSTRUCTION

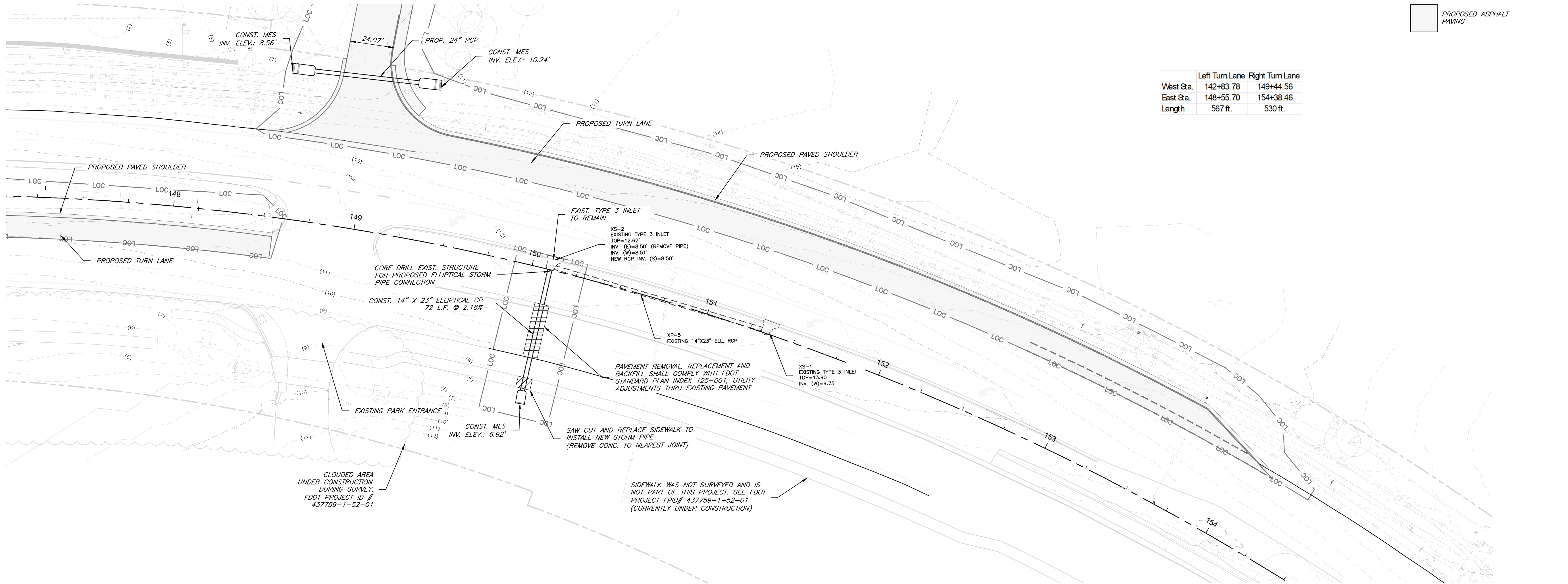
DATE	REVISION	SYMBOL	DATE	REVISION	SYMBOL	ISSUE DATE: 11/11/2024 100% PLANS	COMP. FILE NO. 21-5436	STATE PROJECT NO. 61307C-N3903	DESIGNER: SWU	DRAWN BY: TJM	REVIEWED BY: JHP	CONSULTANT:
Department of Environmental Protection Division of Recreation and Parks Bureau of Design and Construction 3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157									George & Associates Consulting Engineers, Inc. ONE FORTYSEVEN AVENUE, SUITE 200, TALLAHASSEE, FL 32303 PHONE: 850/5210334 - FAX: 850/5210345			
CAMP HELEN STATE PARK									DRIVEWAY PLAN AND PROFILE			
SHEET TITLE									PARK IMPROVEMENT			
SHEET NO.									C303			

D:\C300\ November 8, 2024 P:\Projects\21-5438 BDC Camp Helen State Park\Drawings\Civil\Site Plan - Plan and Profile\C300 Site Plan Turn Lanes.dwg



EAST BOUND LEFT TURN LANE PLAN

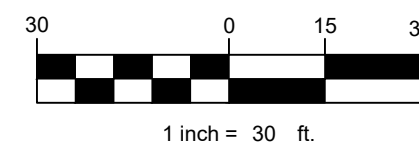
SCALE: 1" = 30'



WEST BOUND RIGHT TURN LANE PLAN

SCALE: 1" = 30'

NOT FOR CONSTRUCTION



CAMP HELEN STATE PARK

SITE PLAN TURN LANES

PARK IMPROVEMENT

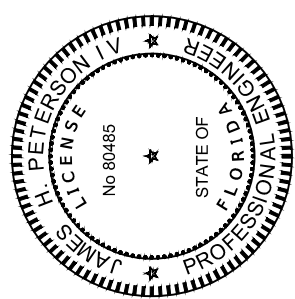
SHEET TITLE

PROJECT TITLE

SHEET NO.

C304

PROFESSIONAL REGISTRATION



JAMES H. PETERSON P.E. # 88485

DESIGNER: SMU

DRAWN BY: SMU

REVIEWED BY: JHP

CONSULTANT:

George & Associates
Consulting Engineers, Inc.
1907 Commonwealth Lane, Suite 200, Tallahassee, FL 32303
PHONE: 850/5210344 - FAX: 850/5210345

ISSUE DATE: 11/11/2024

COMP. FILE NO.: 21-5438

STATE PROJECT NO.: 61307C-N3803

SYMBOL

SYMBOL

REVISION

REVISION

DATE

DATE

SYMBOL

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REVISION

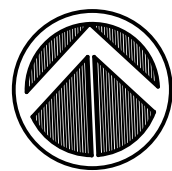
REVISION

DATE

DATE

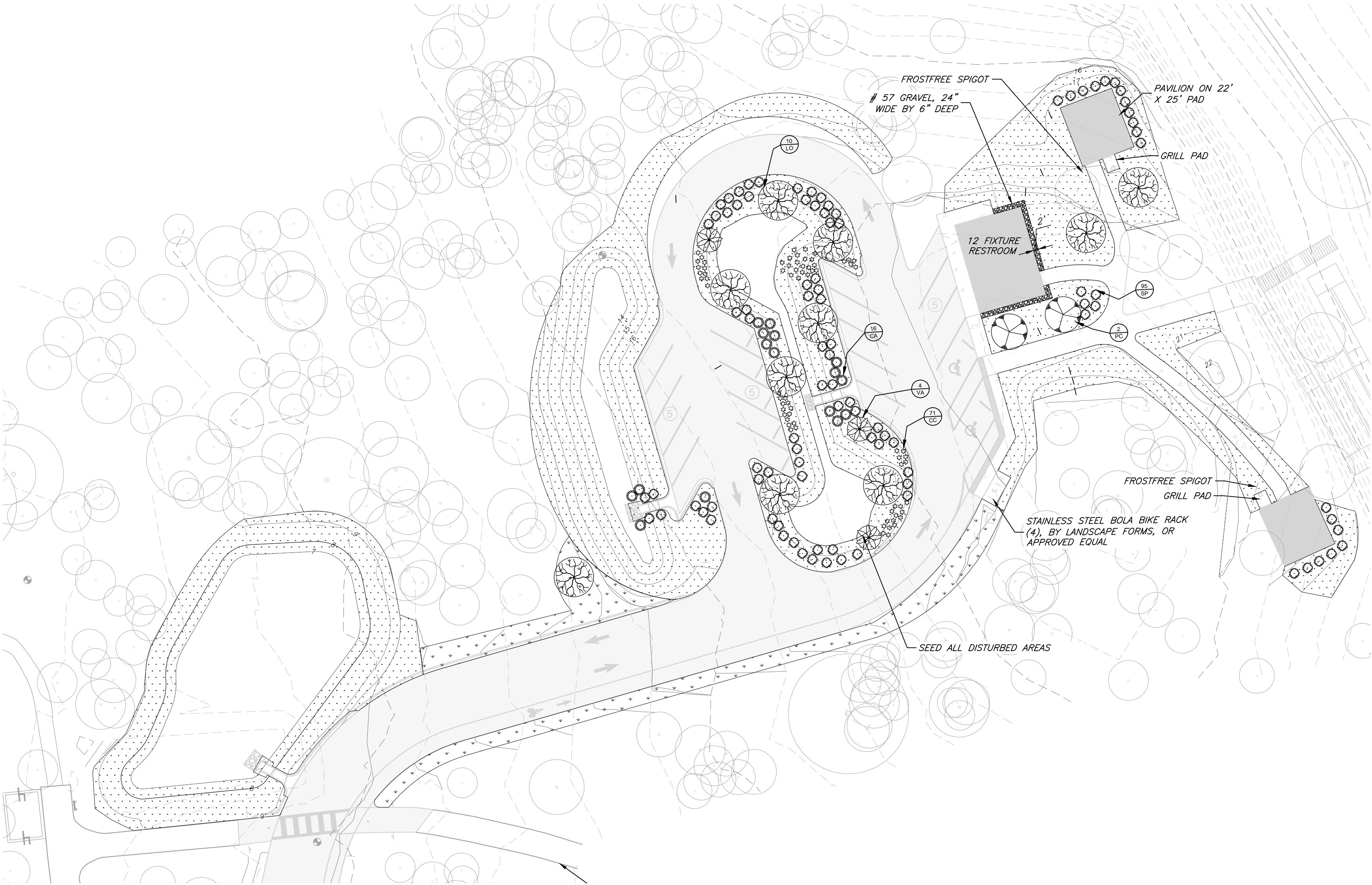
Department of Environmental Protection
Division of Recreation and Parks
Bureau of Design and Construction
3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157

S:\LSA\MER_October 31, 2024_P\Project\02-15436 BDC Camp Helen State Park\Drawings\CHS\05 Site Plan - Plant and Profile\02061 Landscape Plan.dwg



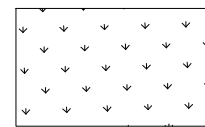
LANDSCAPE PLAN

SCALE: 1" = 30'

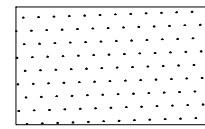


Symbol	I.D.	Quantity	Scientific Name	Common Name	Installed Size	Spacing	Remarks
	LO	10	Quercus geminata	Sand Live Oak	30 GAL	Per Plan	1.75"-2" Cal., 8'-9', 6' Min. clearance from paved surfaces and 10' from buildings, measured from the center of the plant.
	PC	2	Pinus clausa	Sand Pine	30 GAL	Per Plan	2"-2.25" Cal., 9'-10', 6' Min. clearance from paved surfaces and 10' from buildings, measured from the center of the plant.
	VA	3	Vaccinium arboreum	Sparkleberry	7 GAL	Per Plan	
	SP	95	Serenoa repens	Saw Palmetto	7 GAL	Per Plan	Plant in natural drifts, 3' Min. clearance from paved surfaces, measured from the center of the plant.
	CC	71	Conradina canescens	False Rosemary	1 GAL	Per Plan	Plant in natural drifts, 1.5' Min. clearance from paved surfaces, measured from the center of the plant.
	CA	16	Callicarpa americana	American beautyberry	7 GAL	Per Plan	Plant in natural drifts, 3' Min. clearance from paved surfaces, measured from the center of the plant.

LEGEND



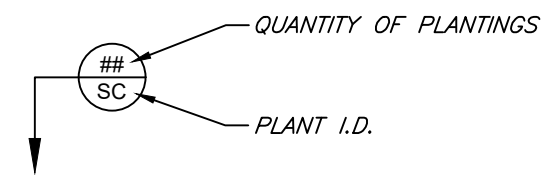
GRASS SEED MIX - OVER 50% PENSACOLA BAHIA SEED



FLORIDA UPLAND MEADOW MIX, ERNST SEEDS ITEM #ERNMX-601, OR APPROVED EQUAL.*

*WILDFLOWER MIX MUST BE COMBINED WITH A COVER CROP OF BROWN TOP MILLET AT A RATE OF 10 LBS PER ACRE FROM APRIL TO SEPT OR ANNUAL RYE AT A RATE OF 30 LBS/ACRE FROM OCT-MARCH. FL UPLAND MIX TO BE APPLIED AT A RATE OF 15 LBS PER ACRE. SEE MANUFACTURERS INSTRUCTIONS FOR MORE DETAILS.

REFERENCE LEGEND

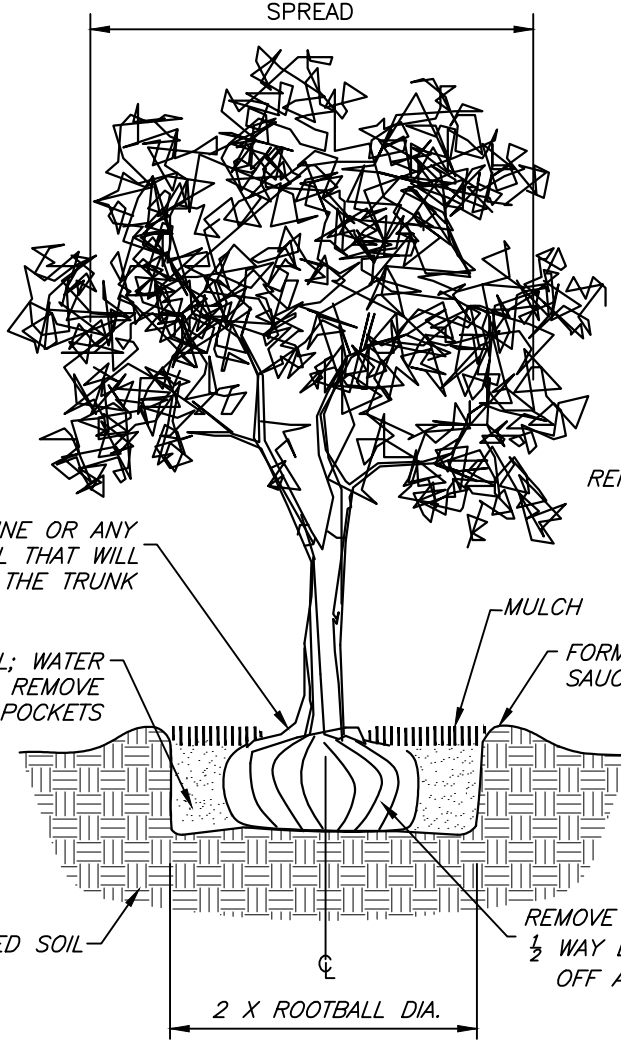


LANDSCAPING NOTES

- LANDSCAPE CONTRACTOR SHALL VERIFY SIZE, LOCATIONS OF ALL PLANTING AREAS AND APPROPRIATE PLANT QUANTITIES NEEDED PRIOR TO INSTALLATION. NOTIFY ENGINEER OF RECORD OF DETECTED DISCREPANCIES.
- PERFORM ALL WORK IN STRICT ACCORDANCE WITH SOUND HORTICULTURAL PRACTICES.
- CLEARANCES OF 7 1/2" SHALL BE MAINTAINED TO THE FRONT AND SIDES AND 4' TO THE REAR OF ALL FIRE APPLIANCES (I.E., HYDRANTS, BACKFLOW PREVENTERS, POST INDICATORS, VALVES, FIRE DEPARTMENT CONNECTIONS).
- MULCH NON-SEEDED DISTURBED AREAS ADJACENT TO IMPERVIOUS AREAS WITH 3" OF FINE STRAW.
- STAKE TREES AS NECESSARY.
- INSTALL TREES AND PLANTS GRADED FLORIDA #1 OR BETTER AS DESCRIBED IN THE MOST RECENT EDITION OF "GRADES AND STANDARDS FOR NURSERY PLANTS", STATE OF FLORIDA.
- IF SPECIFIED SIZE OR SPECIES IS UNAVAILABLE, SUBMIT PROPOSED REPLACEMENT PLANT(S) TO THE ENGINEER OF RECORD FOR APPROVAL, PRIOR TO PURCHASING.
- PLANT TREES, SHRUBS AND PERENNIALS IN A NATURAL MANNER. PLANTING IS TO LOOK SIMILAR TO THE SURROUNDING UNDISTURBED AREAS. AVOID EVEN SPACING AND PLANTING IN STRAIGHT LINES.
- FERTILIZE ALL TREES WITH AGRIFORM 21 GRAM TABLETS, SLOW RELEASE 20-10-5 (OR APPROVED EQUAL) WITH ONE TABLET PER 1/2" OF TRUNK DIAMETER.
- FERTILIZE GROUNDCOVER PERENNIALS AND SHRUBS WITH A SLOW RELEASE FERTILIZER SUCH AS OSMOCOTE 15-9-12 AT A RATE OF 1 TABLESPOON PER 1 GAL PLANT.
- BACKFILL ALL PLANTING WITH A MIXTURE OF 1/2 ON SITE SOIL AND 1/2 CLEAN FRIABLE TOPSOIL.
- PLANTING HOLES SHOULD BE TWICE THE DIAMETER OF THE ROOT BALL AND 2"-4" DEEPER THAN THE ROOT BALL HEIGHT.
- ONCE PLANTED, PLANTS SHOULD BE AT THE SAME LEVEL IN RELATION TO THE GROUND AS THEY WERE PRIOR TO TRANSPLANTING.
- RESTORE ALL DISTURBED AREAS WITH SPECIFIED SEED OR 3" OF FINE STRAW. DISTURBED SOIL SHALL NOT BE LEFT EXPOSED AND VULNERABLE TO EROSION FROM STORM WATER.
- LANDSCAPE IMPROVEMENTS SHALL BE INSTALLED BY THE CONTRACTOR PER FDOT STANDARD SPECIFICATION 580 AND INDEX 544.
- CONTRACTOR SHALL BE RESPONSIBLE FOR TEMPORARY IRRIGATION.
- THE WARRANTY SHALL BEGIN AFTER THE INITIAL LANDSCAPE INSPECTION AND ACCEPTANCE, OR AS PER THE CONTRACT DOCUMENTS.
- INSPECTION SHALL BE MADE BY THE OWNER OR OWNERS REPRESENTATIVE WITHIN 1 WEEK OF WRITTEN NOTIFICATION FROM THE LANDSCAPE CONTRACTOR THAT INSTALLATION IS COMPLETE.
- TREES AND SHRUBS SHALL HAVE A 1 YEAR WARRANTY.
- PLANTS ARE GUARANTEED TO BE HEALTHY AND FLOURISHING FOR 1 YEAR FROM INITIAL INSPECTION ACCEPTANCE.
- REPLACEMENT PLANTS MUST BE THE SAME SIZE AS THE ORIGINAL.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR WATERING AND MAINTAINING THE LANDSCAPING FOR THE WARRANTY PERIOD WHICH IS 1 YEAR.
- CONTRACTOR SHALL NOT COMPACT POND BOTTOMS. SEE POND SIDES ONLY.

UTILITY NOTES

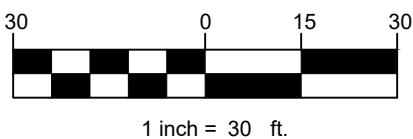
- THE LOCATION(S) OF UTILITIES SHOWN ON THE PLANS SHALL BE CONSIDERED APPROXIMATE.
- CONTRACTOR SHOULD CONTACT THE SUNSHINE STATE 811 ONE CALL SYSTEM 1-800-432-4770 PRIOR TO ANY DIGGING SO THAT UNDERGROUND UTILITIES MAY BE FIELD LOCATED.




PLANT SO THAT TOP OF ROOT FLARE IS 1" ABOVE THE FINISHED GRADE PURSUANT TO A.A.N. STANDARDS CALIPER MEASUREMENTS SHALL BE MADE 6 INCHES ABOVE GROUND LEVEL (ROOTBALL) UP TO AND INCLUDING 4 INCH CALIPER; 12 INCHES ABOVE GROUND LEVEL FOR LARGER SIZES.

TREE PLANTING DETAIL

SCALE: NTS



NOT FOR CONSTRUCTION

CAMP HELEN STATE PARK										PROFESSIONAL REGISTRATION									
LANDSCAPE PLAN																			
SHEET TITLE										SHEET NO.									
PROJECT TITLE										JAMES H. PETERSON IV State of Florida P.E. # 88485									
George & Associates Consulting Engineers, Inc. C.E. - PROFESSIONAL ENGINEERS - LICENSE NO. 27079 EXPIRATION DATE 12/31/2025 1967 Commonwealth Lane, Suite 200 Tallahassee, FL 32303 PHONE: 850-5210348 - FAX 850-5210345										CONSULTANT :									
ISSUE DATE: 11/11/2024 100% PLANS										DESIGNER: SMU									
COMP. FILE NO.: 21-5436										DRAWN BY: SMU									
STATE PROJECT NO.: 61307C-N3803										REVIEWED BY: JHP									
Department of Environmental Protection Division of Recreation and Parks Bureau of Design and Construction 3900 Commonwealth Boulevard, Tallahassee, FL 32389 (850) 245-2157										SYMBOL									
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Department of Environmental Protection
Division of Recreation and Parks
Bureau of Design and Construction
3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157

George & Associates
Consulting Engineers Inc.
CIVIL ENGINEERING, LANDSCAPE ARCHITECTURE, SURVEYING, LAND USE
1907 Commonwealth Lane, Tallahassee, FL 32303
PHONE: 850/5210344 - FAX: 850/5210345

State of Florida P.E. # 88485

Approved
3/24/2025 09:13:00036
Lisa Ward
1/16/2025

C306

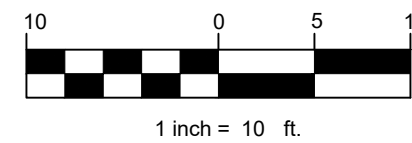
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NORTH PICNIC AREA GRADING PLAN

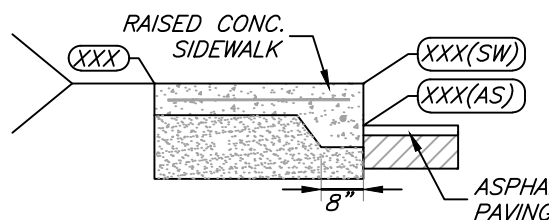
SCALE: 1" = 10'

NOT FOR CONSTRUCTION



SPOT ELEVATION LEGEND

- XXX EXISTING SPOT ELEVATION
- XXX(AS) PROPOSED SPOT ELEVATION FOR ASPHALT PAVING WITH RAISED CONC. SIDEWALK
- XXX(SW) PROPOSED SPOT ELEVATION FOR RAISED CONC. SIDEWALK
- XXX PROPOSED TYPICAL SPOT ELEVATION



CAMP HELEN STATE PARK

NORTH PICNIC AREA GRADING PLAN

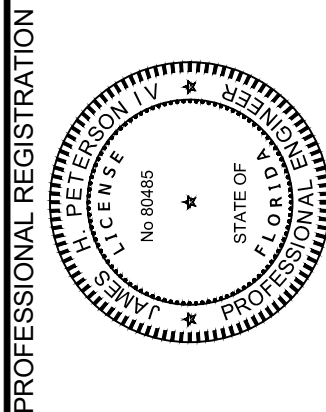
PARK IMPROVEMENT

SHEET NO.

C401

SHEET TITLE

PROJECT TITLE



PROFESSIONAL REGISTRATION

DESIGNER: SWU

DRAWN BY: TJM

REVIEWED BY: JHP

ISSUE DATE: 11/11/2024

COMP. FILE NO.: 21-5439

STATE PROJECT NO.: 61307C-N3903

DATE

REVISION

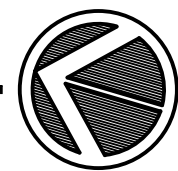
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DATE

Department of Environmental Protection
Division of Recreation and Parks
Bureau of Design and Construction
3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157

George & Associates
Consulting Engineers, Inc.
CONSULTING ENGINEER
1907 Commonwealth Lane, Tallahassee, FL 32303
PHONE: 850/5210344 - FAX: 850/5210345

DR2010 November 15, 2024, P:\Projects\21-5436 BDC Camp Helen State Park\Drawings\Camp Helen State Park\Grading\Grading Plan.dwg



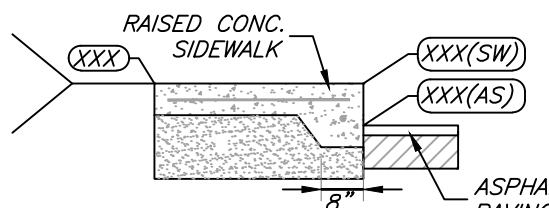
NORTH PARKING LOT GRADING PLAN

SCALE: 1" = 10'

NOT FOR CONSTRUCTION

SPOT ELEVATION LEGEND

- XXX - EXISTING SPOT ELEVATION
- XXX(AS) - PROPOSED SPOT ELEVATION FOR ASPHALT PAVING WITH RAISED CONC. SIDEWALK
- XXX(SW) - PROPOSED SPOT ELEVATION FOR RAISED CONC. SIDEWALK
- XXX - PROPOSED TYPICAL SPOT ELEVATION



CAMP HELEN STATE PARK

NORTH PARKING LOT GRADING PLAN

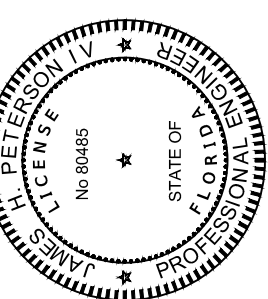
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SHEET TITLE

SHEET NO.

C402

PROFESSIONAL REGISTRATION



JAMES H. PETERSON, P.E.
No. 88485
State of Florida P.E. # 88485

DESIGNER: SWU

DRAWN BY: TJM

REVIEWED BY: JHP

CONSULTANT:

George & Associates

Consulting Engineers, Inc.

1907 Commonwealth Lane, Suite 200, Tallahassee, FL 32303

PHONE: 904/521-0344 - FAX: 904/521-0345

ISSUE DATE: 11/11/2024

COMP. FILE NO.: 21-5436

STATE PROJECT NO.: 61307C-N3903

REVISION

SYMBOL

DATE

REVISION

SYMBOL

DATE

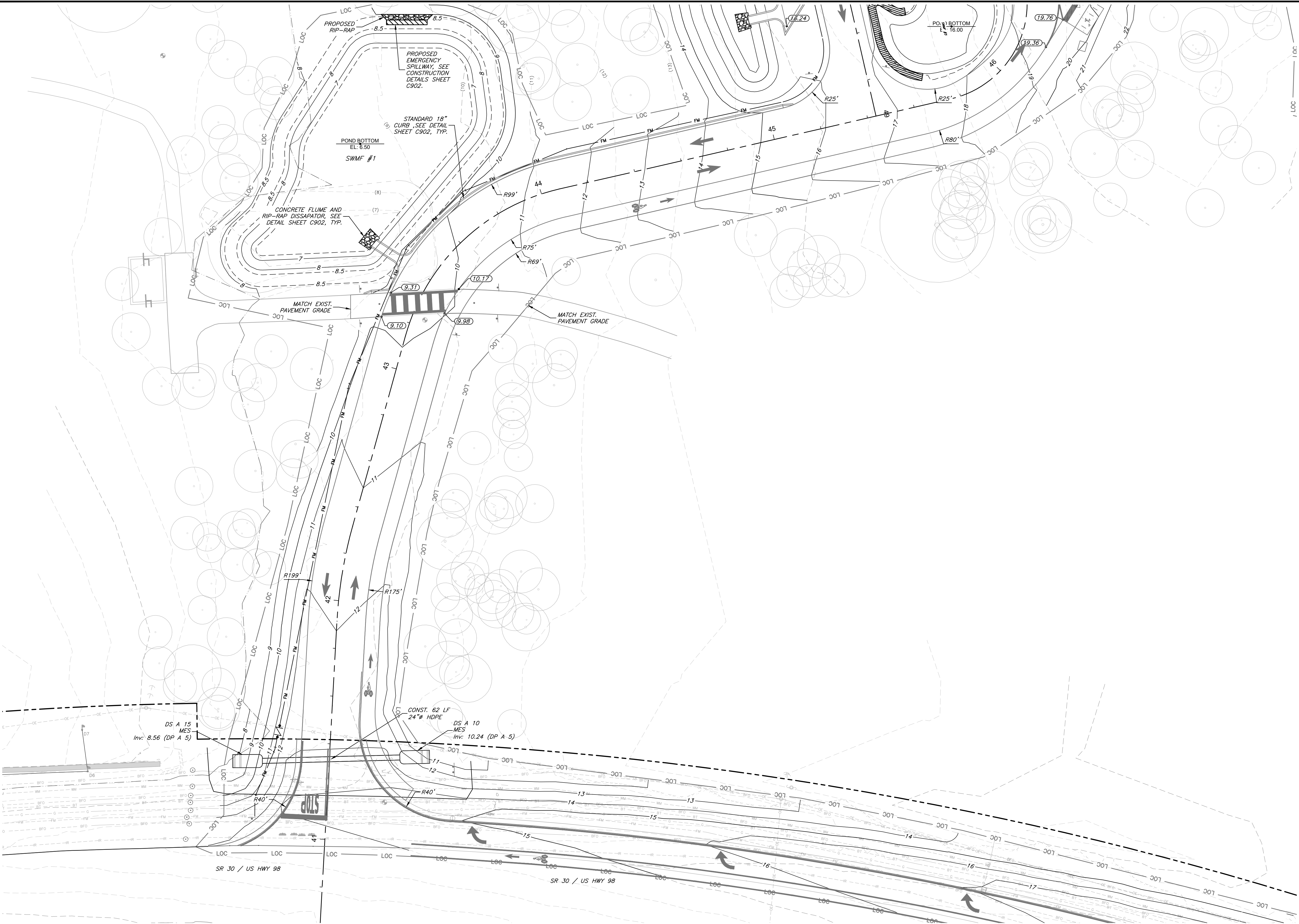
Department of Environmental Protection

Division of Recreation and Parks

Bureau of Design and Construction

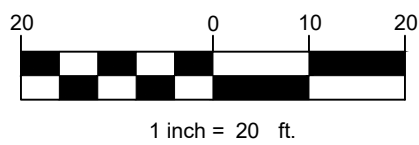
3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157

D:\PROJECTS\2023\11\11\2024\BDC\Camp Helen State Park\Drawings\CA006 Cross Section\CA003 North Driveway Grading Plan.dwg



NORTH DRIVEWAY GRADING PLAN

SCALE: 1" = 20'



NOT FOR CONSTRUCTION

CAMP HELEN STATE PARK

NORTH DRIVEWAY GRADING PLAN

PARK IMPROVEMENT

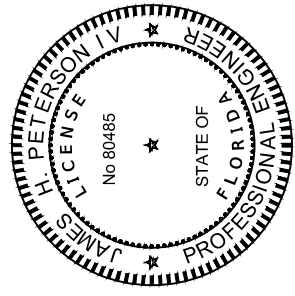
SHEET TITLE

PROJECT TITLE

SHEET NO.

C403

PROFESSIONAL REGISTRATION



JAMES H. PETERSON IV
State of Florida P.E. # 88485

DESIGNER: SWU

DRAWN BY: TJM

REVIEWED BY: JHP

Consultant:

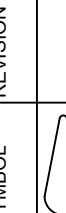
GA
George & Associates
Consulting Engineers, Inc.
Civil, Environmental, Infrastructure, Water Planning, Land Use
1907 Commonwealth Boulevard, Tallahassee, FL 32303
PHONE: 850.521.0344 - FAX: 850.521.0345

ISSUE DATE: 11/11/2024

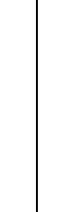
COMP. FILE NO.: 21-5486

STATE PROJECT NO.: 61307C-N3803

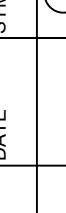
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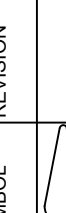
REVISION



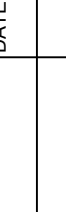
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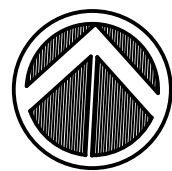


REVISION



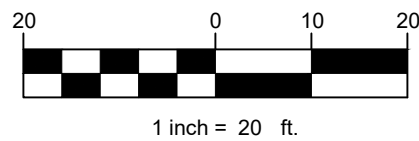
Department of Environmental Protection
Division of Recreation and Parks
Bureau of Design and Construction
3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157

S:\SAMSER - October 25, 2024 - P:\Project\501-5408 BDC Camp Helen State Park\Drawings\CH408 Cross Sections\CH408 ADA Kayak Launch Grading Plan.dwg

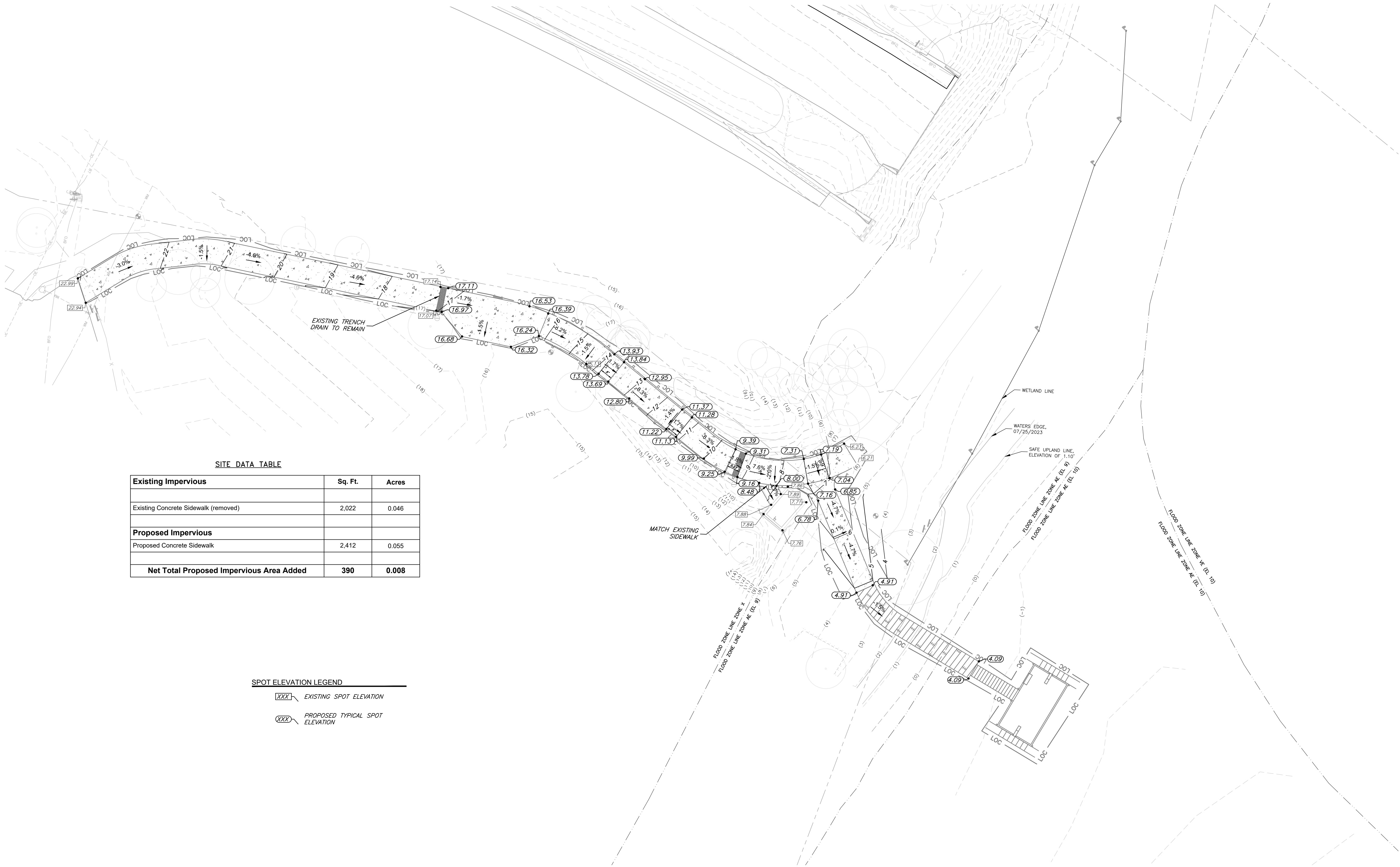


ADA KAYAK LAUNCH GRADING PLAN

SCALE: 1" = 20'



NOT FOR CONSTRUCTION



SITE DATA TABLE

Existing Impervious	Sq. Ft.	Acres
Existing Concrete Sidewalk (removed)	2,022	0.046
Proposed Impervious		
Proposed Concrete Sidewalk	2,412	0.055
Net Total Proposed Impervious Area Added	390	0.008

SPOT ELEVATION LEGEND

- EXISTING SPOT ELEVATION
- PROPOSED TYPICAL SPOT ELEVATION

CAMP HELEN STATE PARK

ADA KAYAK LAUNCH GRADING PLAN

PARK IMPROVEMENT

DESIGNER: SMU

DRAWN BY: TJM

REVIEWED BY: JHP

ISSUE DATE: 11/11/2024

COMP. FILE NO.: 21-5408

STATE PROJECT NO.: 61307C-N3903

100% PLANS

SYMBOL

REVISION

DATE

SYMBOL

REVISION

DATE

Department of Environmental Protection
Division of Recreation and Parks
Bureau of Design and Construction
3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157

George & Associates
Consulting Engineers, Inc.
Civil, Environmental, Mechanical, Electrical, Structural, and Surveying
1907 Commonwealth Lane, Tallahassee, FL 32303
PHONE: 850/5210344 - FAX: 850/5210345

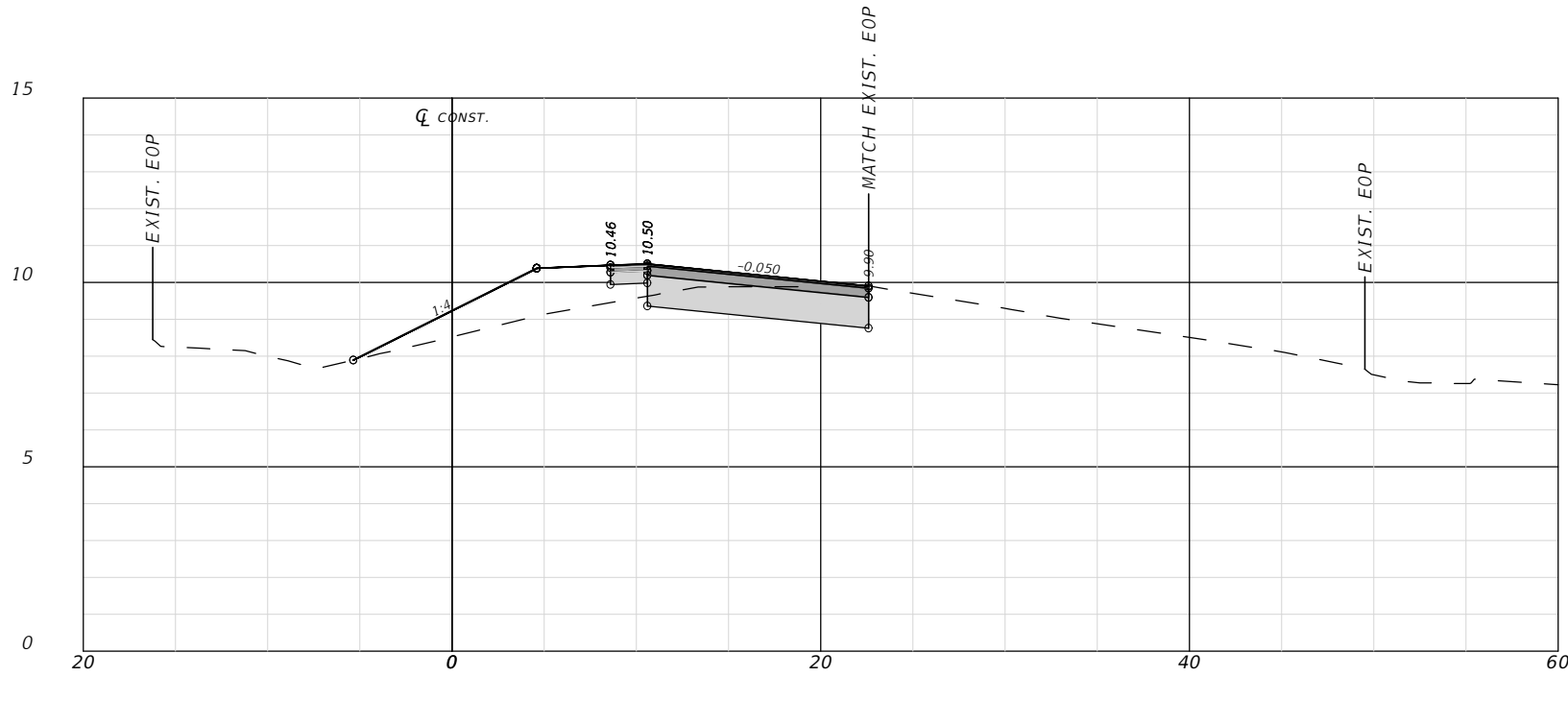
PROFESSIONAL REGISTRATION

JAMES H. PETERSON IV
State of Florida P.E. # 88485

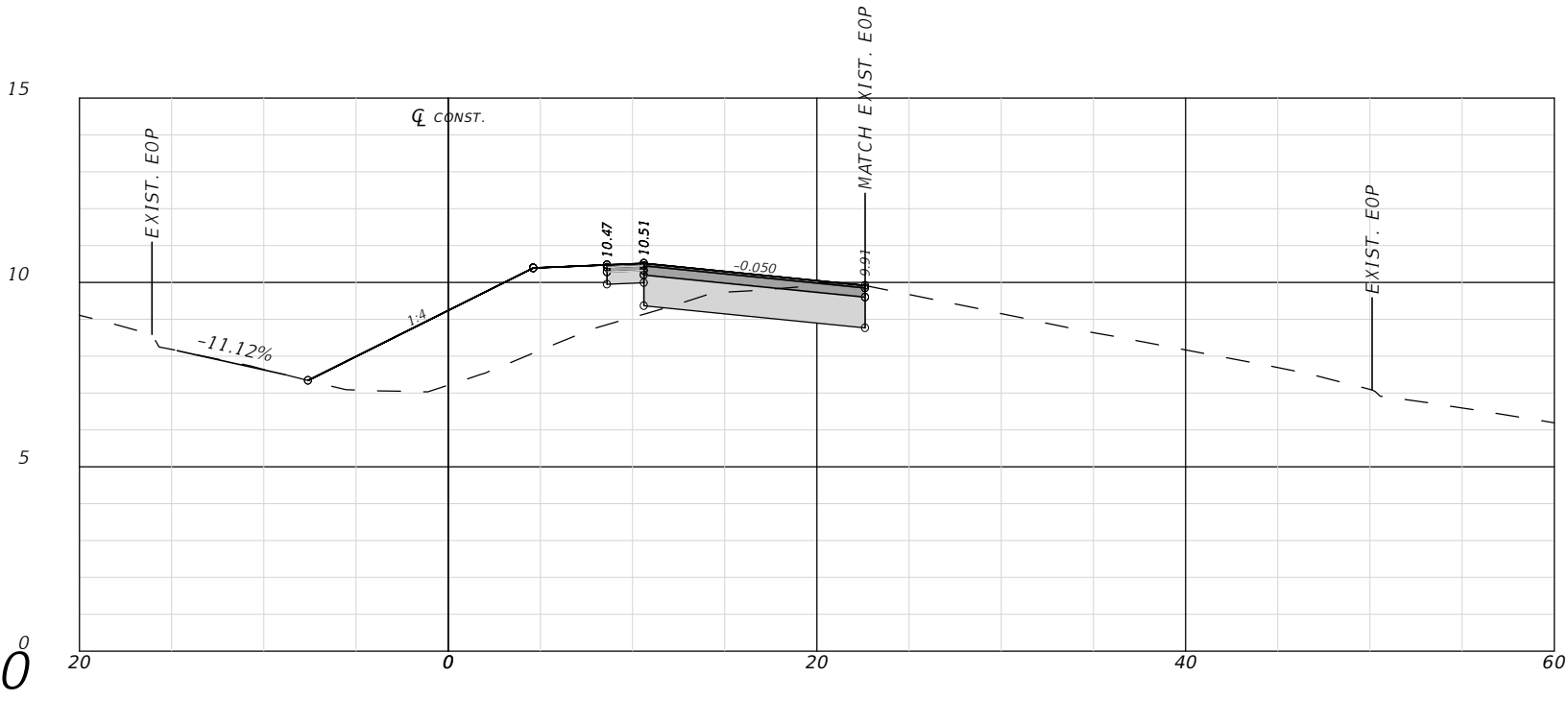
J.PETERSON, November 1, 2024, P:\Projects\21-5436 BDC Camp Helen State Park\Drawings\Civil\06 Cross Sections\CA06 North Turn Lane Cross Sections.dwg

EAST BOUND TURN LANE CROSS SECTIONS

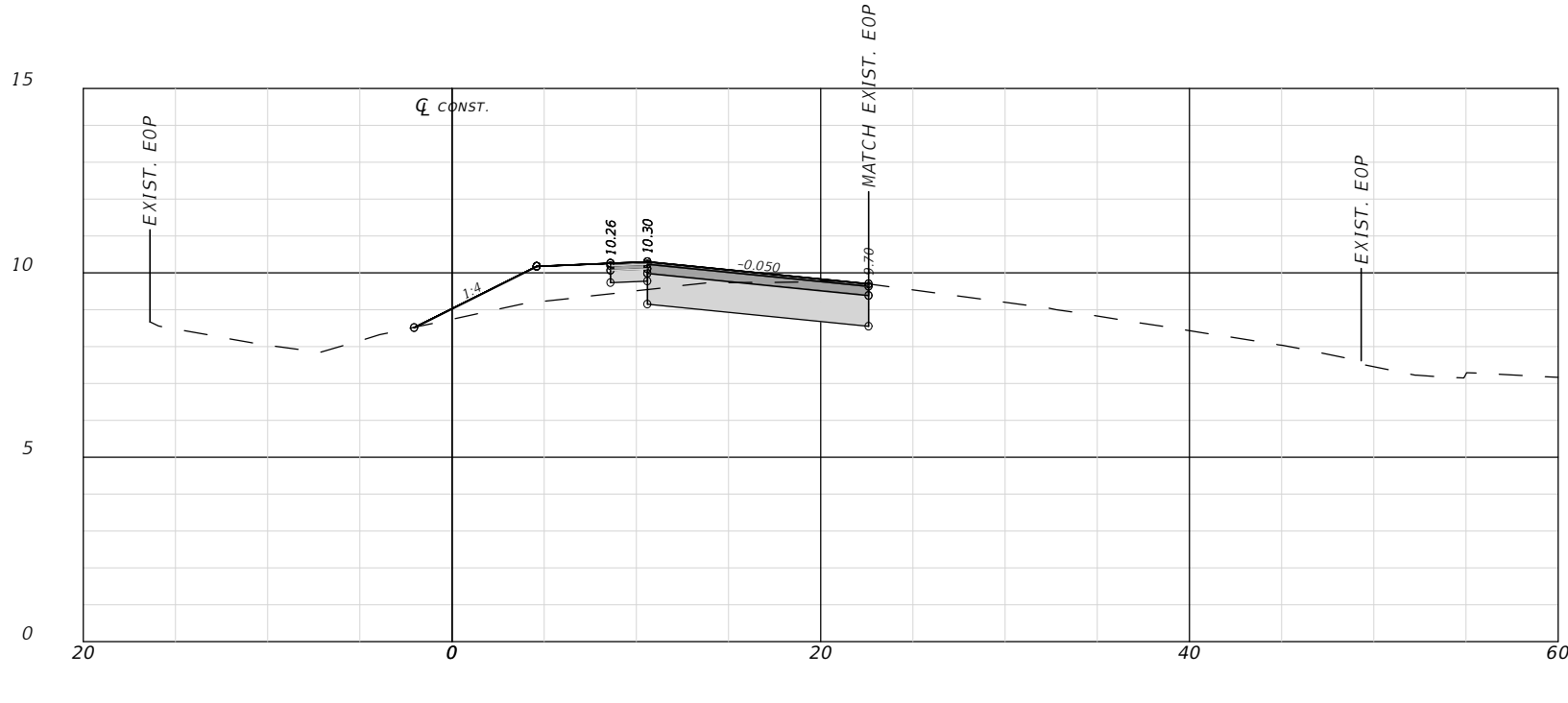
HORIZ. SCALE: 1" = 10' VERT. SCALE: 1" = 5'



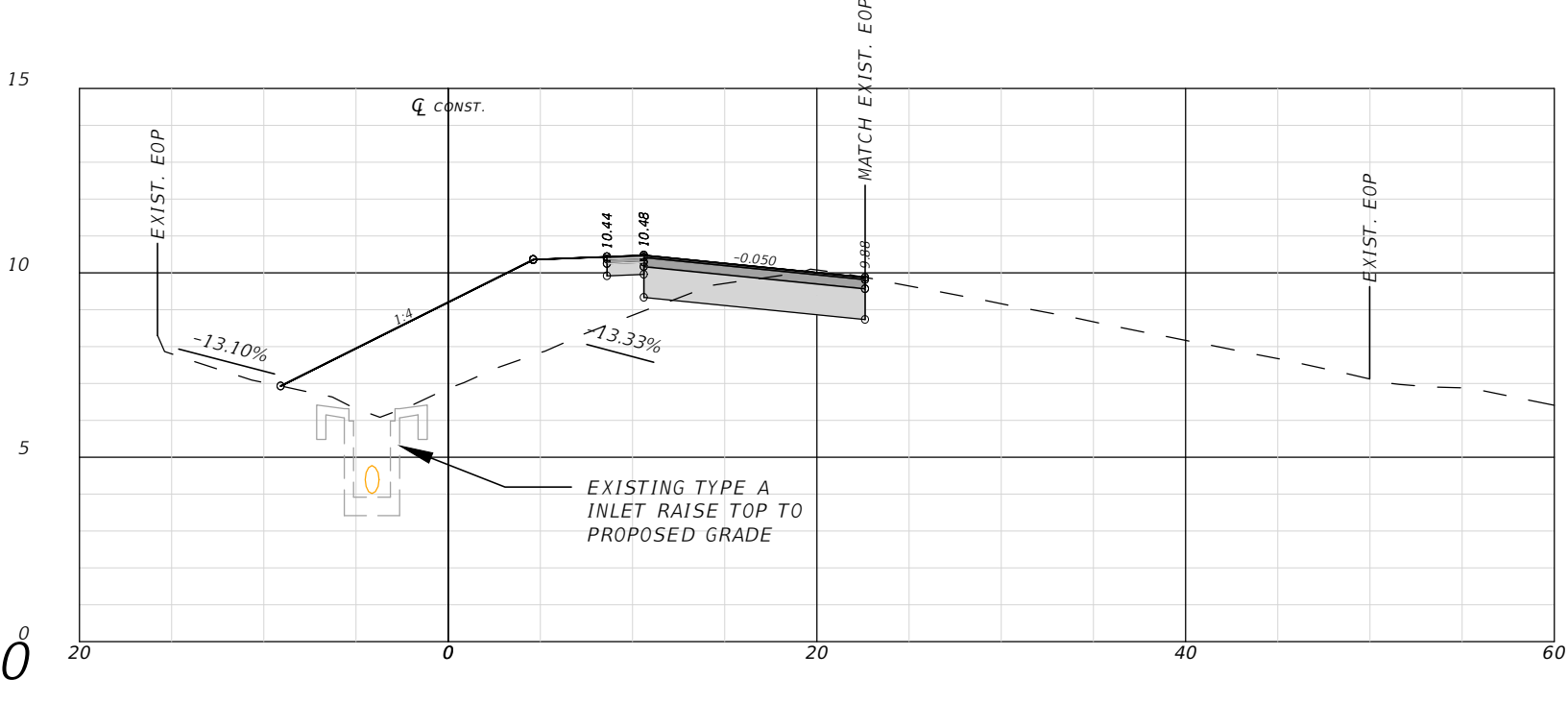
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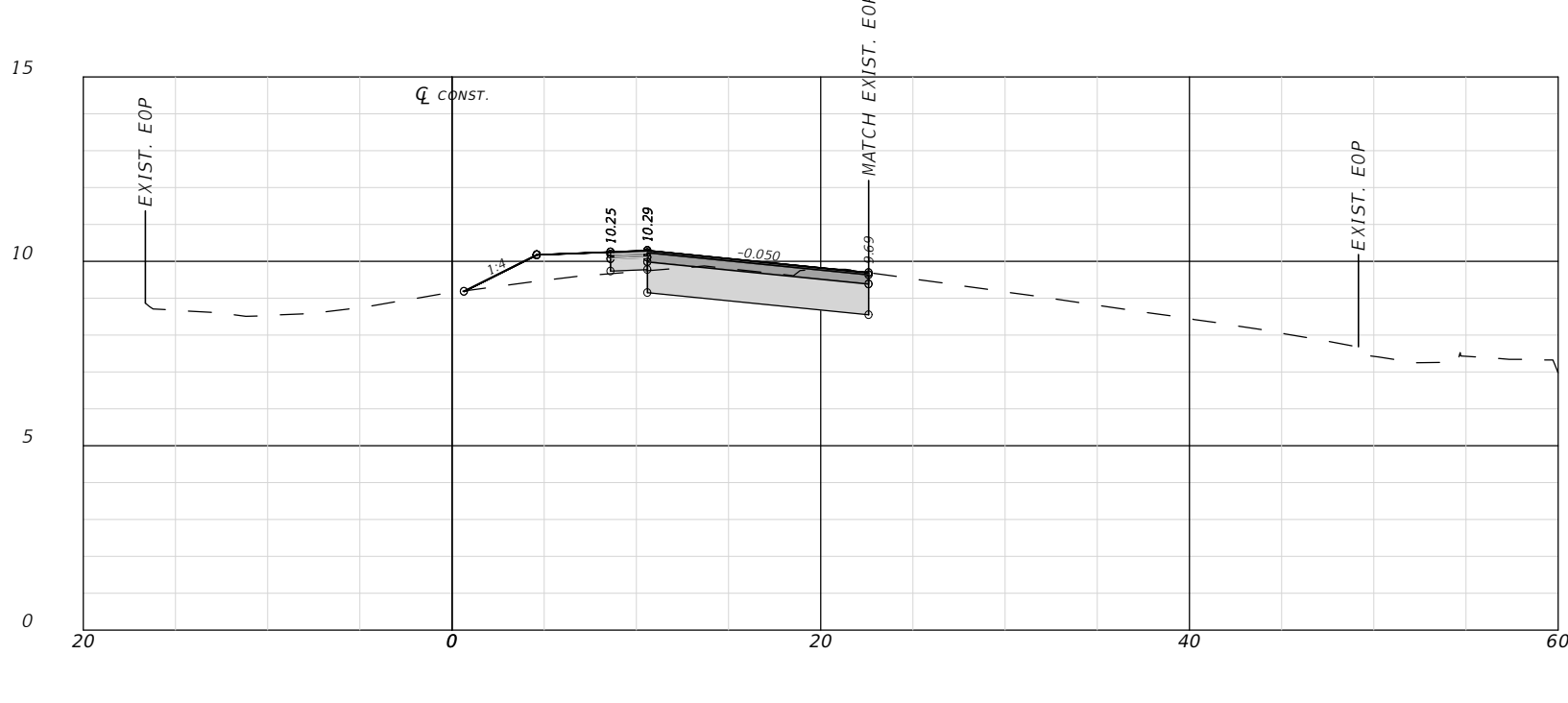
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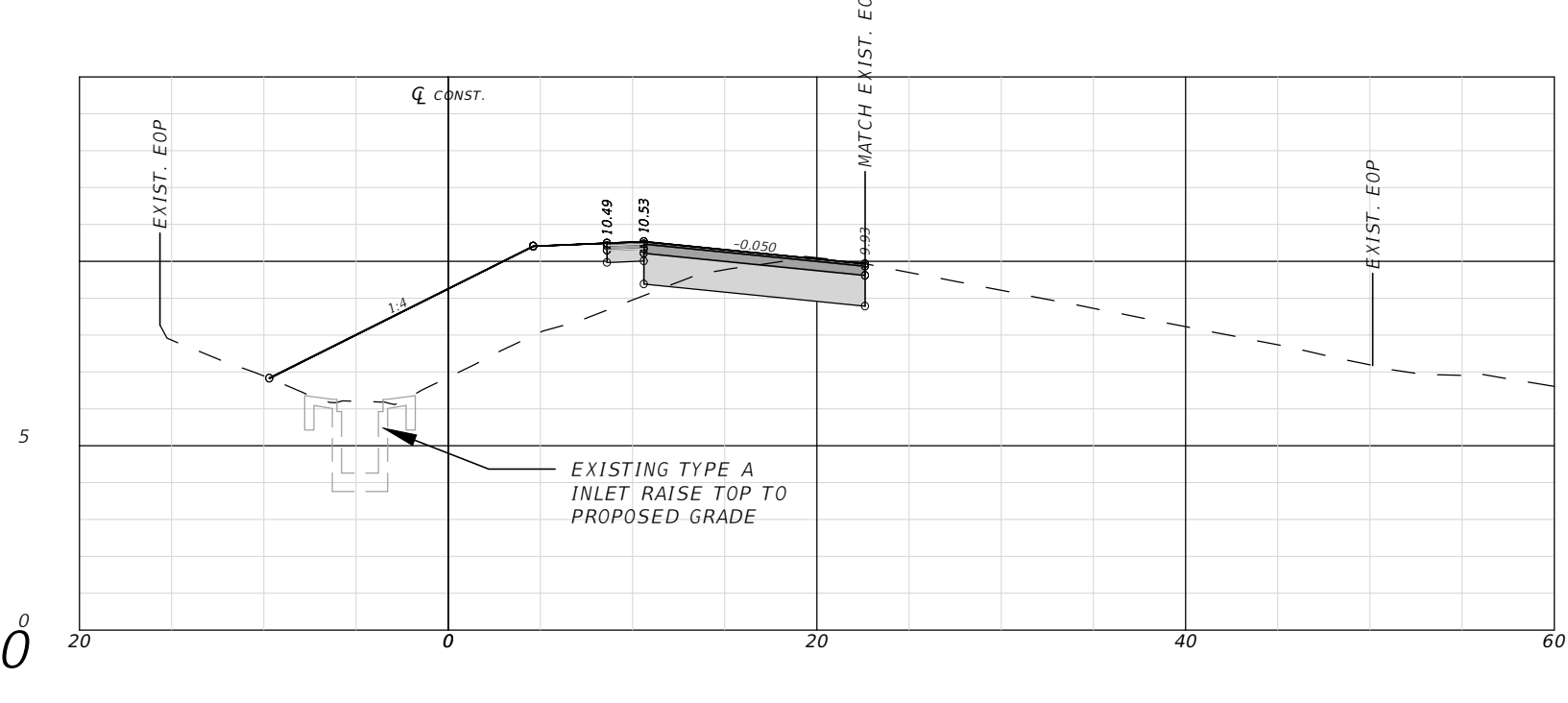
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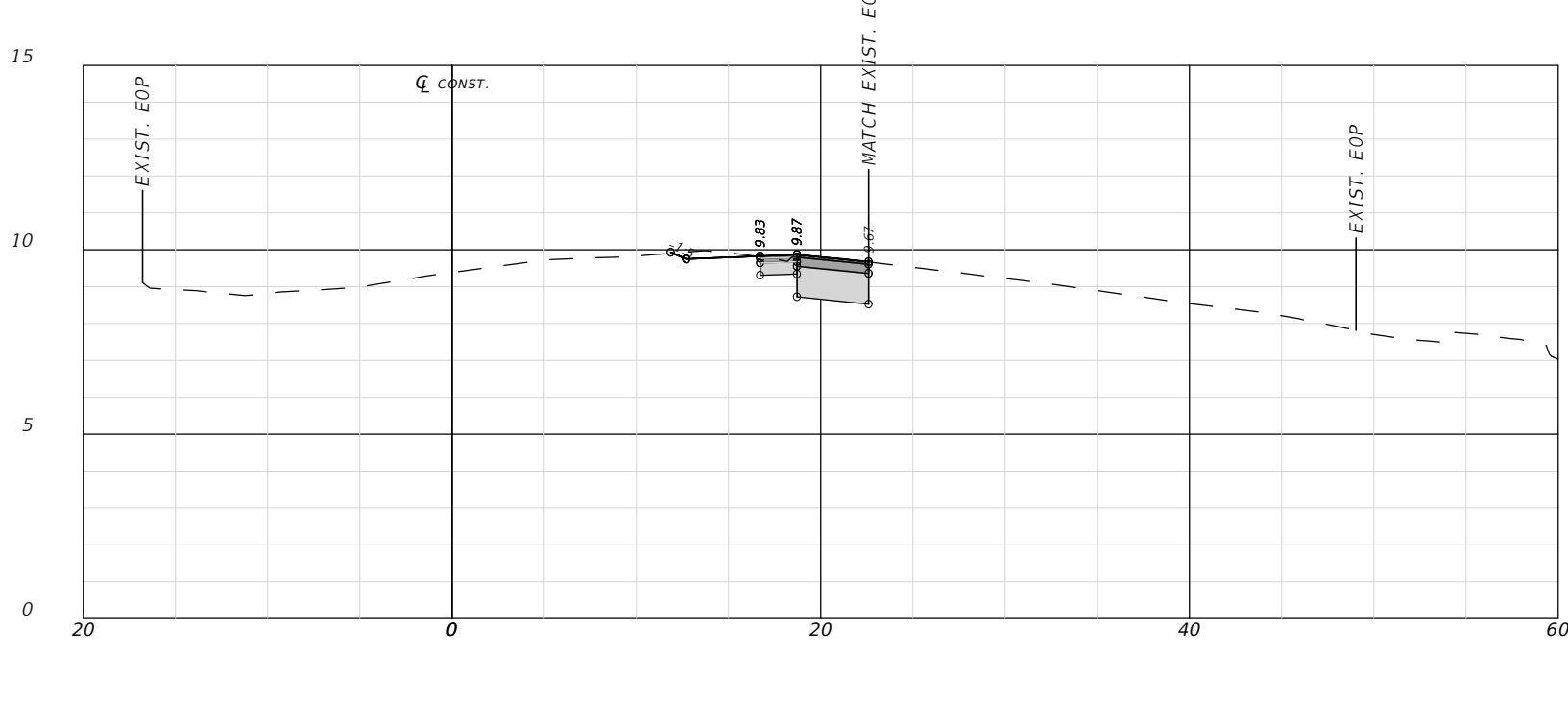
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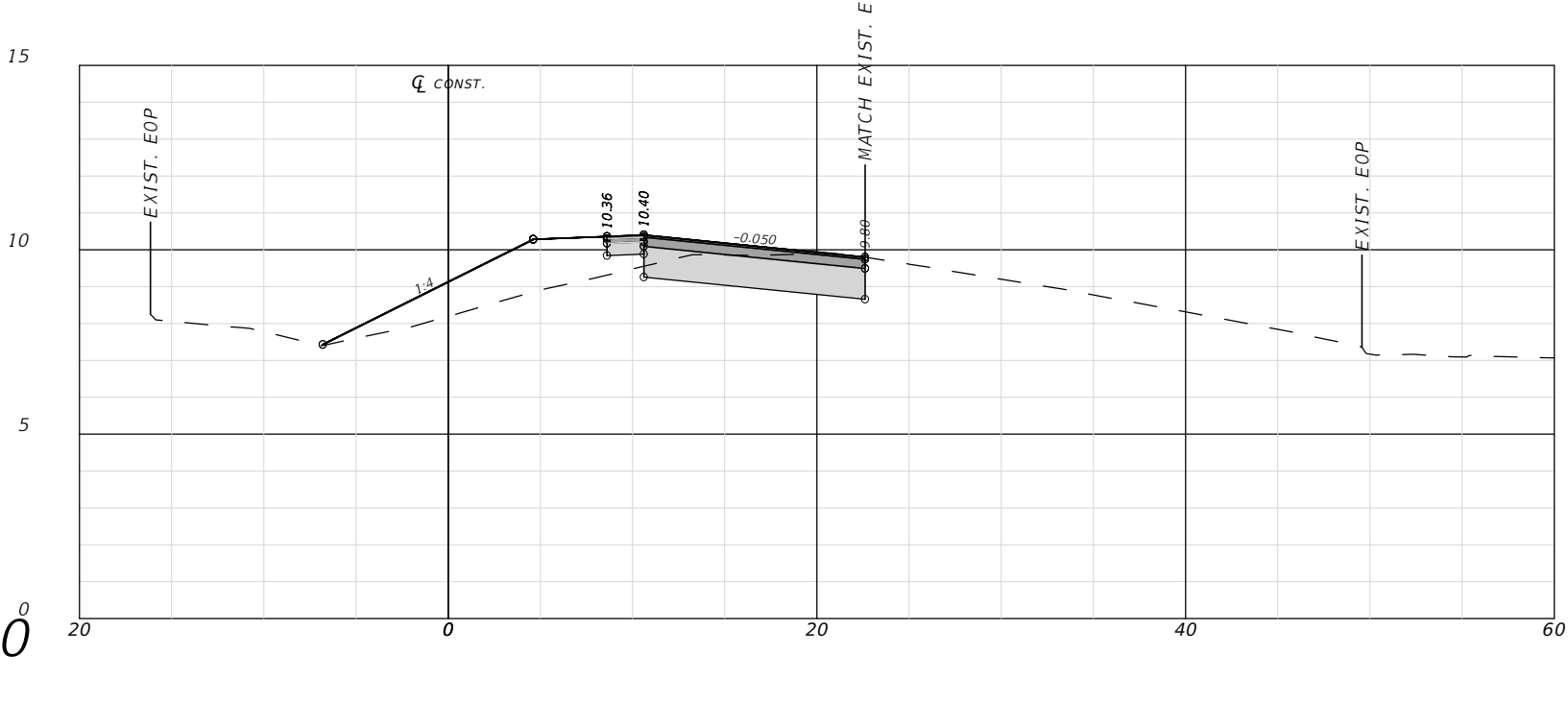
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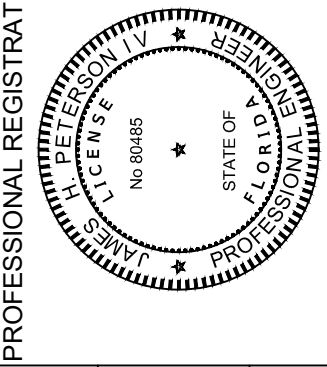
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145+00.00

NOT FOR CONSTRUCTION

CAMP HELEN STATE PARK		DESIGNER: SMU	ISSUE DATE: 11/11/2024	REVISION	SYMBOL	DATE
EAST BOUND TURN LANE CROSS SECTIONS		DRAWN BY: TJM	COMP. FILE NO.: 21-5436			
PARK IMPROVEMENT		REVIEWED BY: JHP	STATE PROJECT NO. 61307C-N3803			
SHEET NO.		Department of Environmental Protection Division of Recreation and Parks Bureau of Design and Construction 3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157				

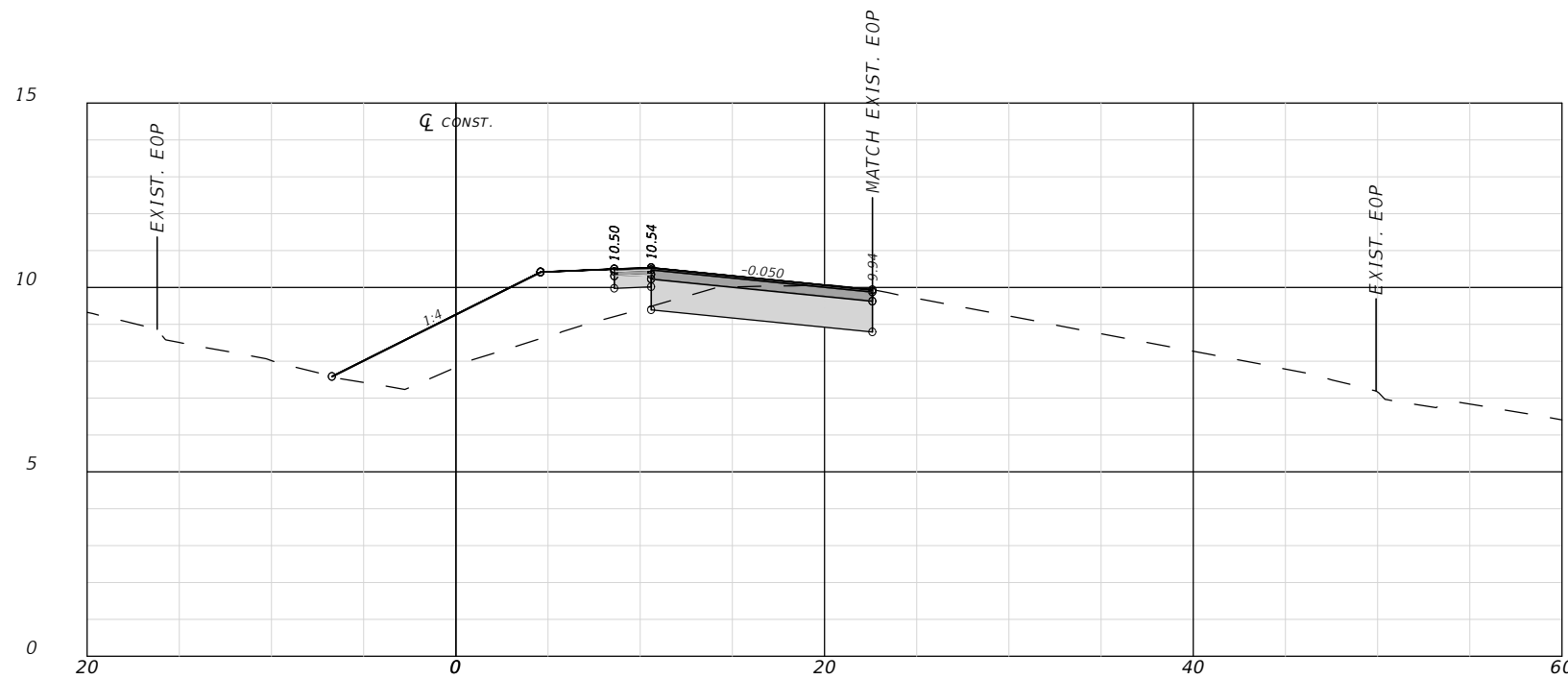


JAMES H. PETERSON IV
State of Florida P.E. # 84485

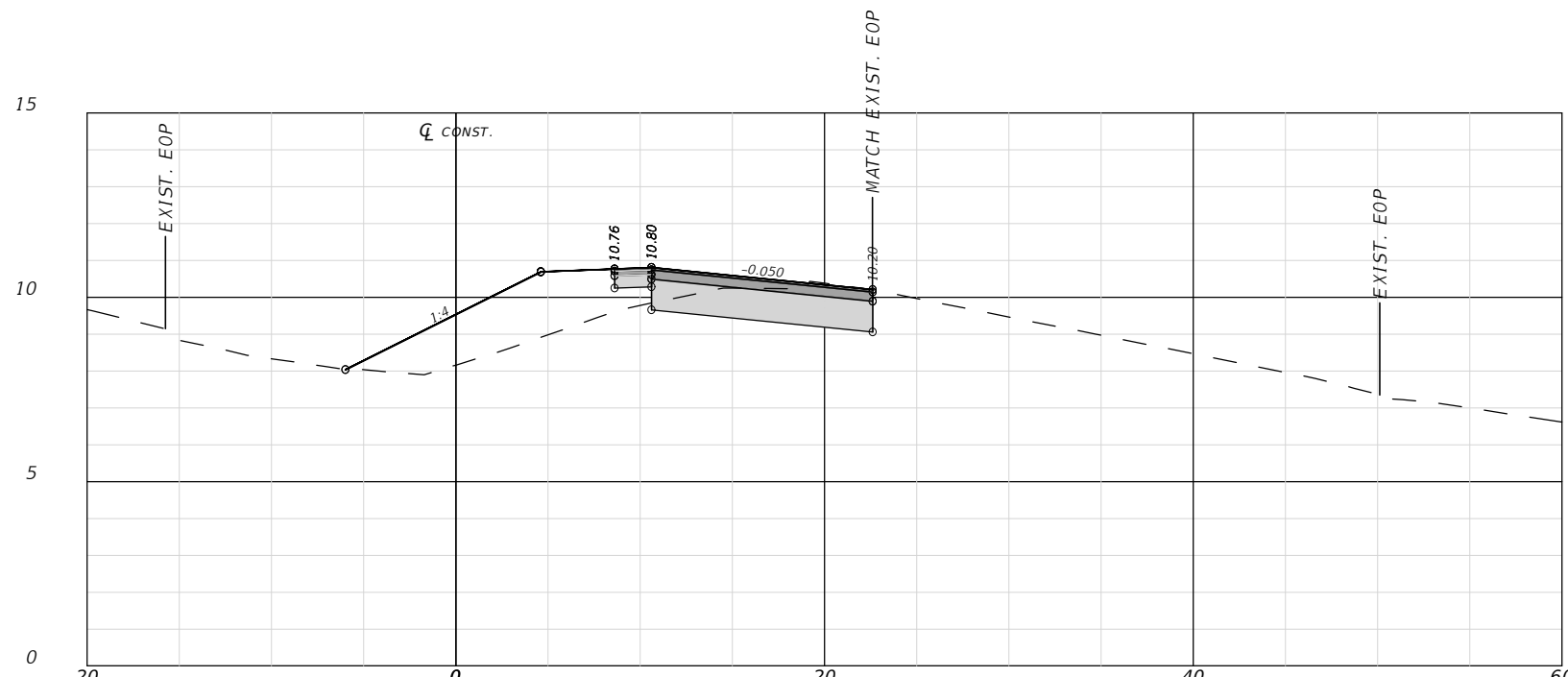
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Approved
11/16/2025
11/16/2025

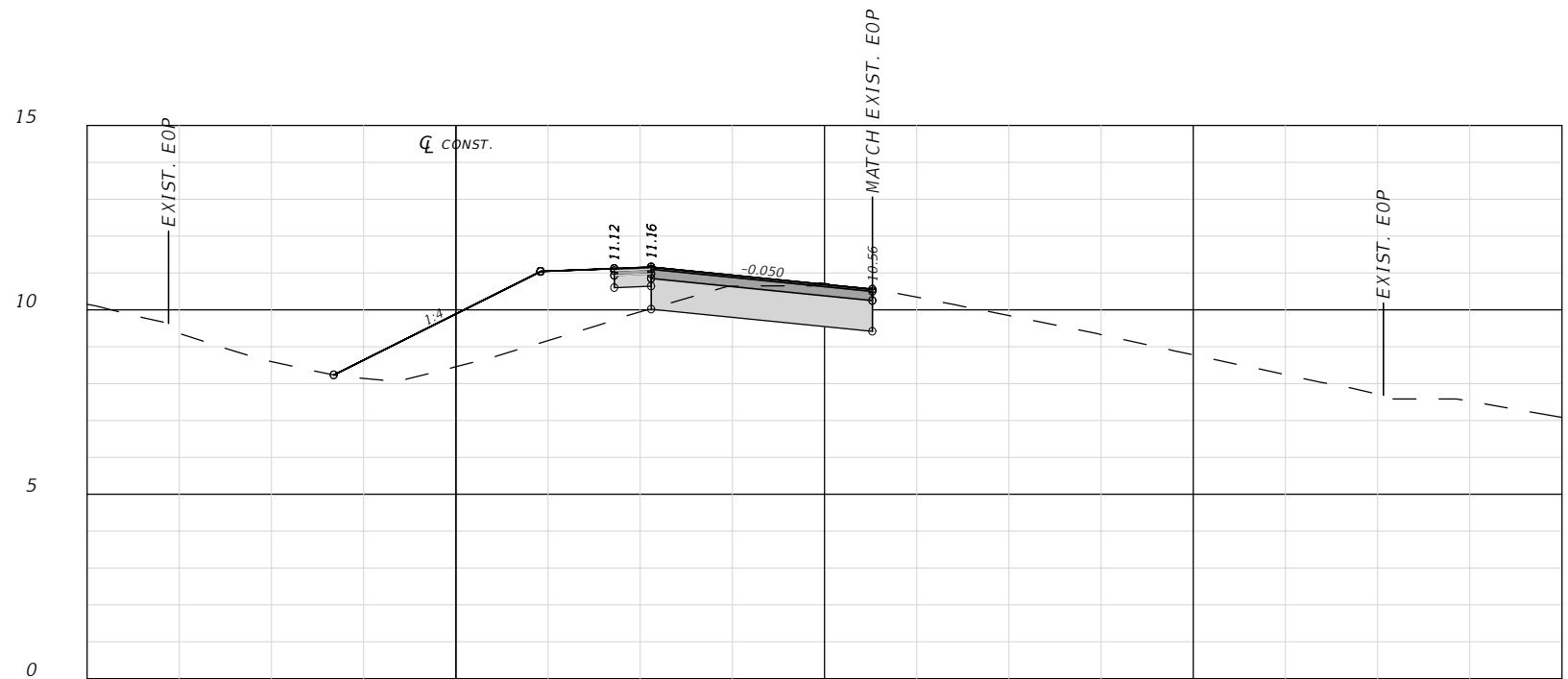
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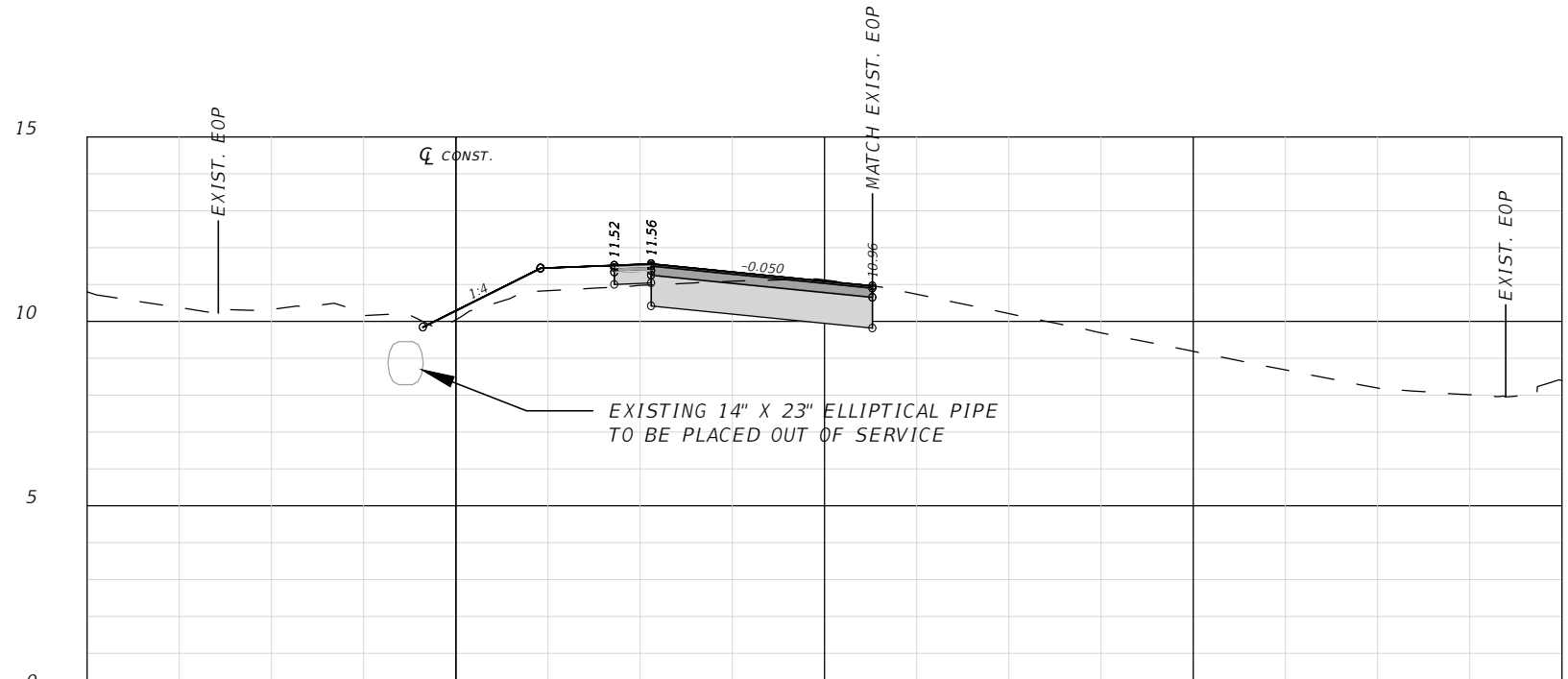
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148+00.00



148+52.98

EAST BOUND TURN LANE CROSS SECTIONS

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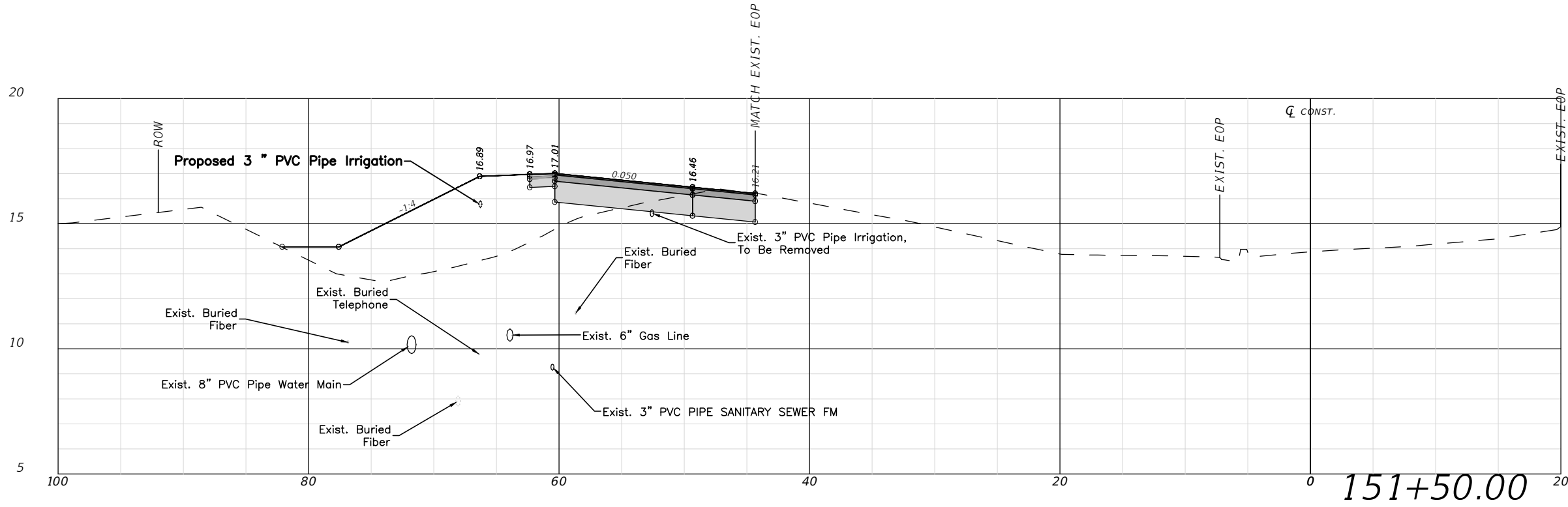
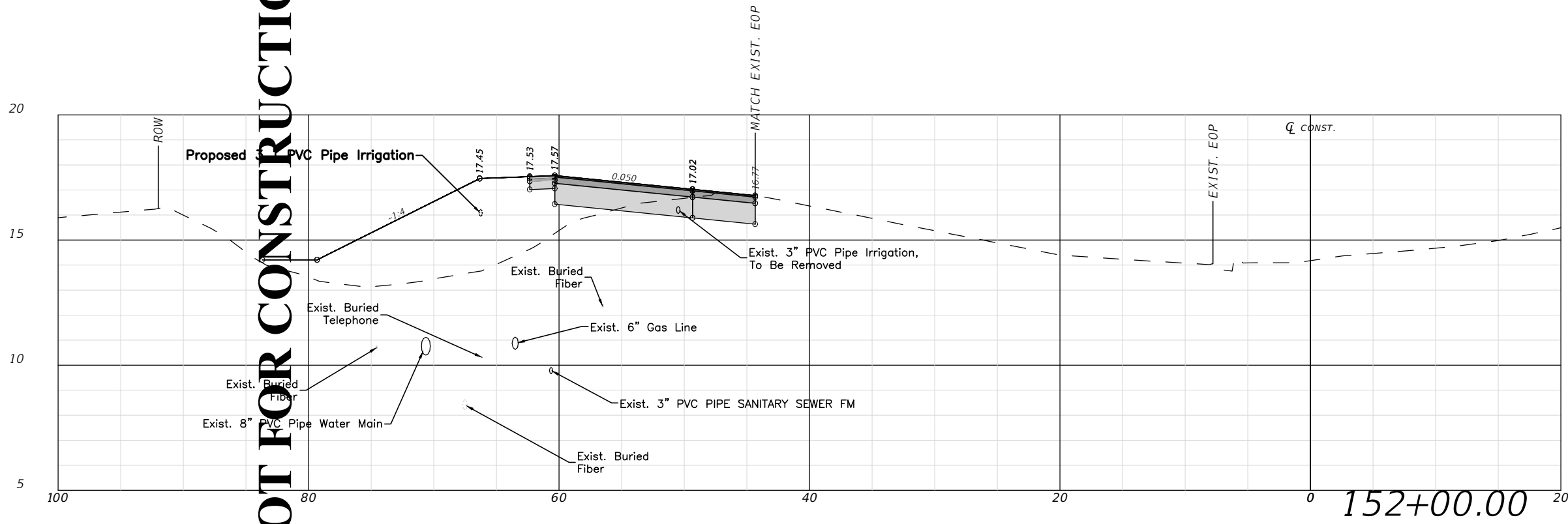
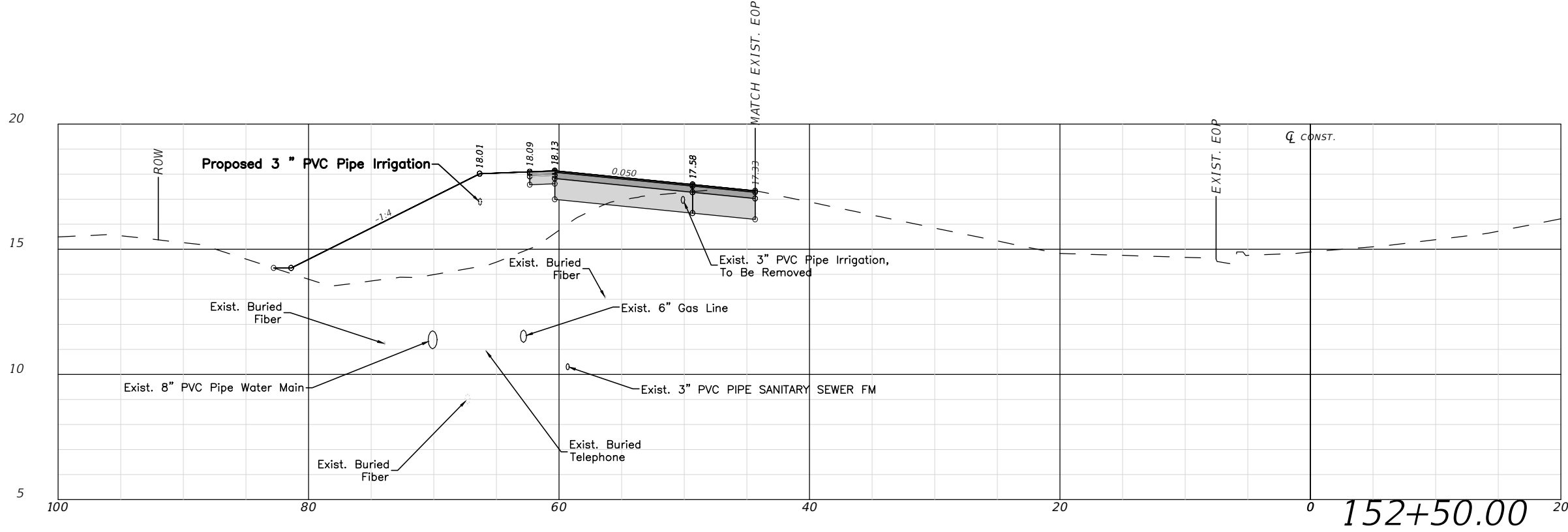
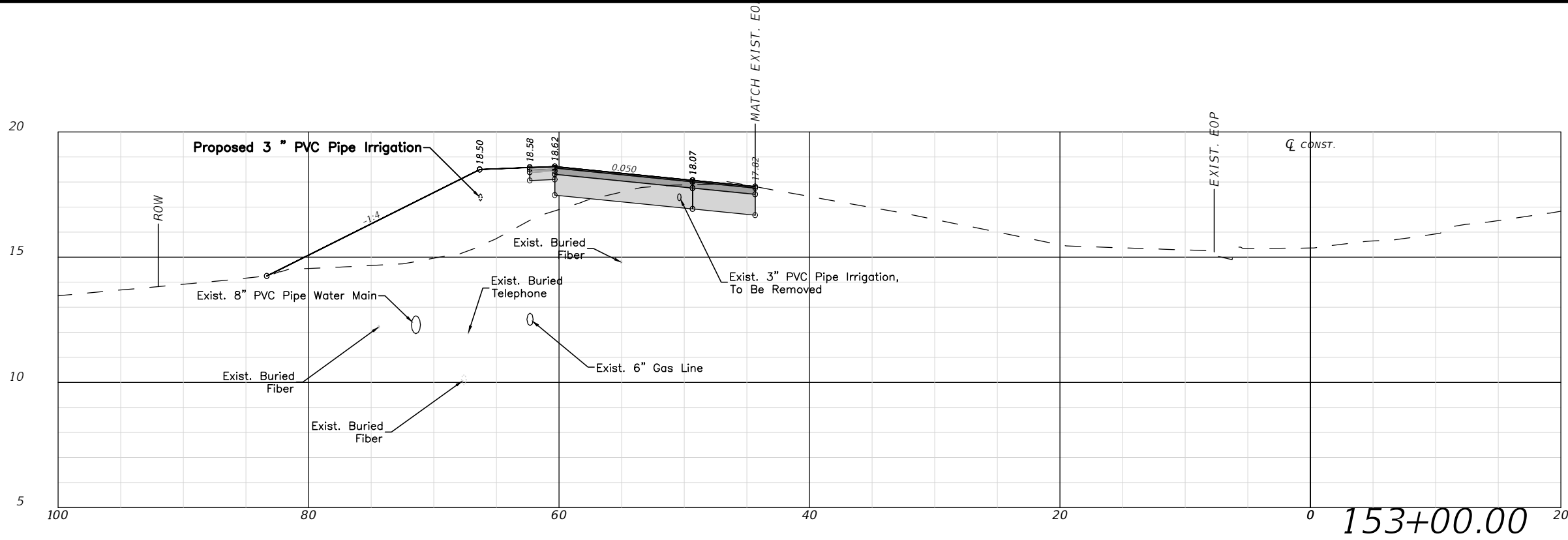
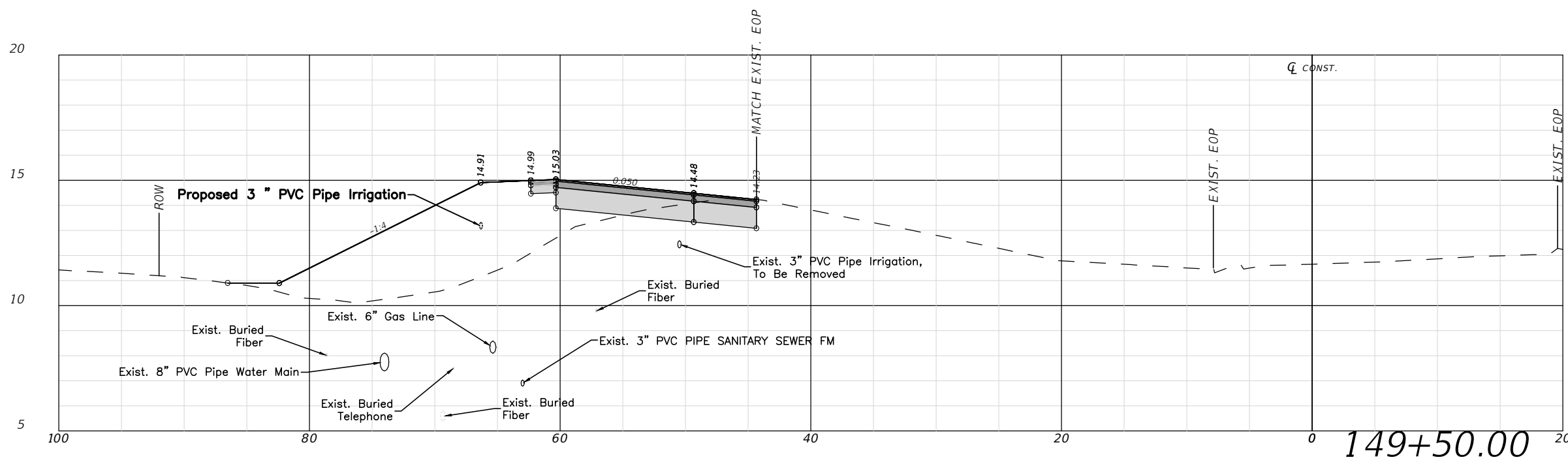
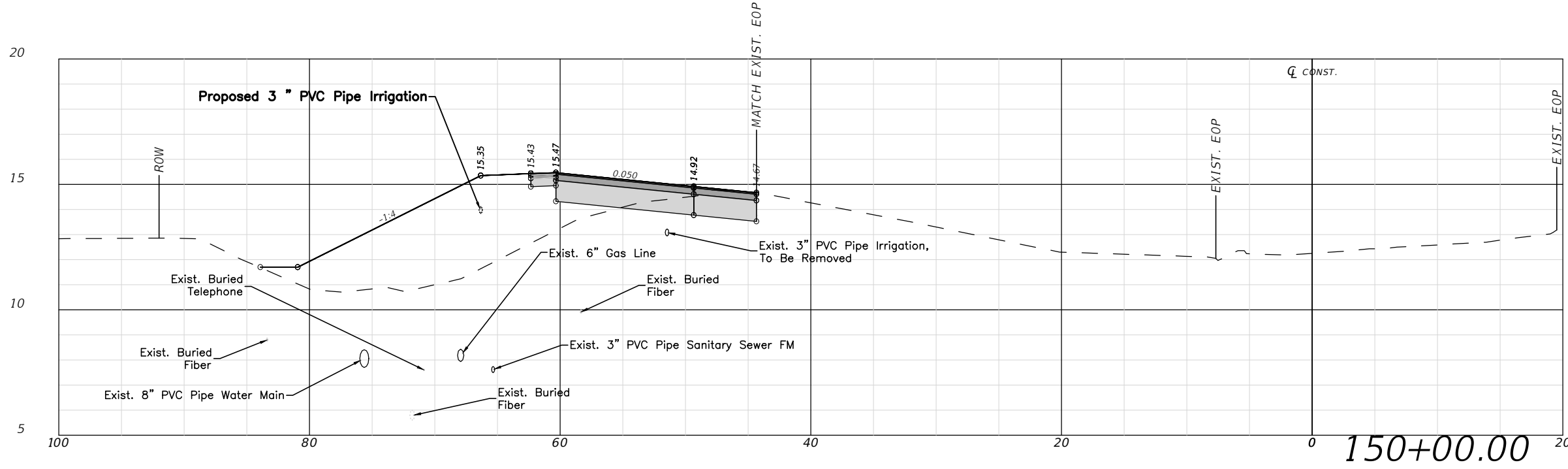
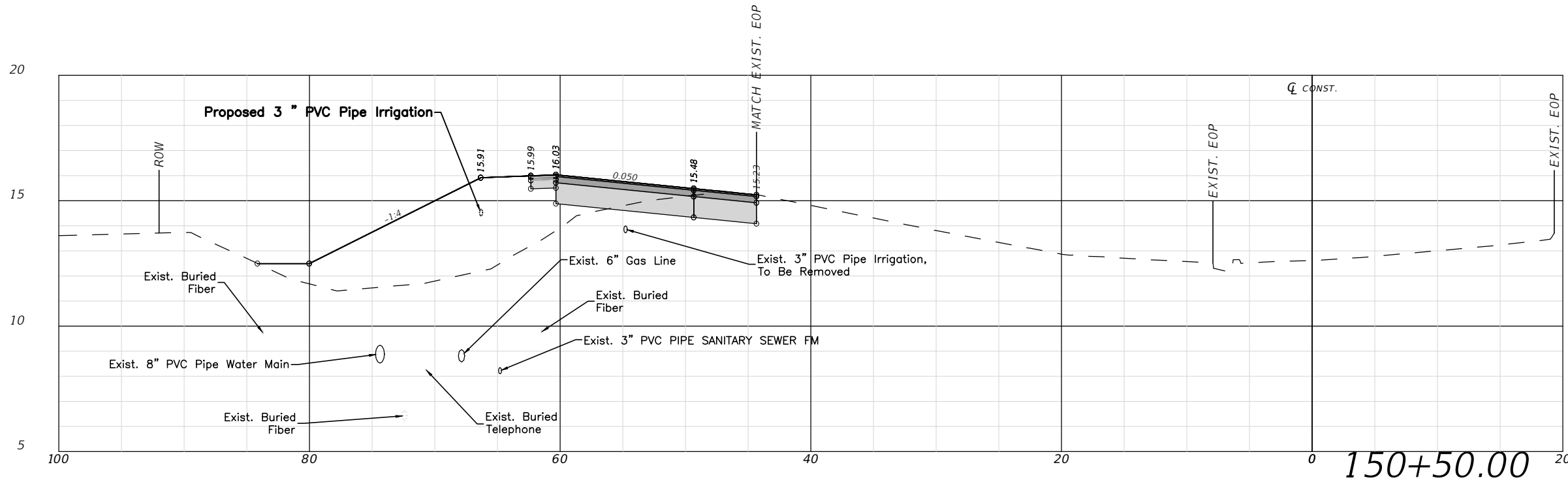
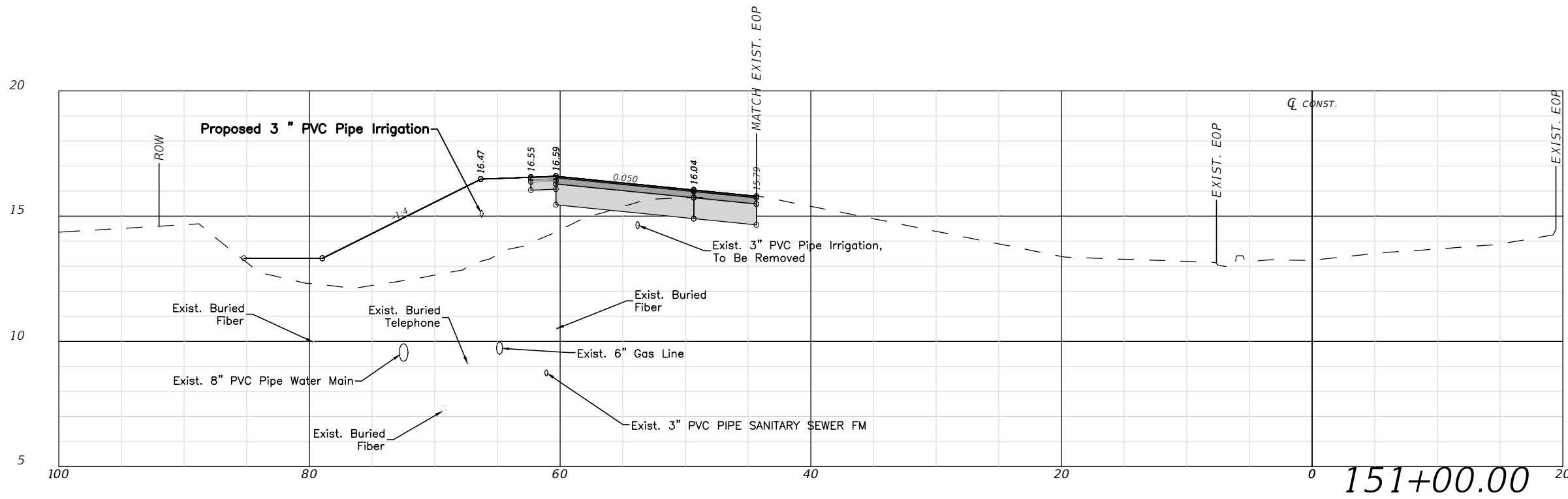
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EAST BOUND TURN LANE CROSS SECTIONS		REVIEWED BY: JHP		STATE PROJECT No: 61307C-N3803		SYMBOL		REVISION		DATE	
PROJECT TITLE		Consultant:		George & Associates Consulting Engineers, Inc. 1987 Commonwealth Lane Tallahassee, FL 32303 PHONE: 850/5210344 - FAX: 850/5210345		SYMBOL		REVISION		DATE	
PARK IMPROVEMENT		Professional Registration		James H. Peterson IV Professional Engineer No. 80485 State of Florida		SYMBOL		REVISION		DATE	
SHEET NO.		C406		Approved		SYMBOL		REVISION		DATE	
C406		Approved		11/16/2025		SYMBOL		REVISION		DATE	
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J. PETERSON November 1, 2024, P:\Projects\21-5488 BDC Camp Helen State Park\Drawings\Civil\08 Cross Sections\08 North Turn Lane Cross Sections.dwg

WEST BOUND TURN LANE CROSS SECTIONS

HORIZ SCALE: 1" = 10' VERT. SCALE: 1" = 5'



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CAMP HELEN STATE PARK		DESIGNER: SMU	REVISION	SYMBOL	REVISION	DATE
WEST BOUND TURN LANE CROSS SECTIONS		DRAWN BY: SMU	SYMBOL	SYMBOL	SYMBOL	DATE
PARK IMPROVEMENT		REVIEWED BY: JHP	SYMBOL	SYMBOL	SYMBOL	DATE
SHEET NO.		ISSUE DATE: 11/11/2024 100% PLANS				
PROJECT TITLE		COMP. FILE NO.: 21-5488				
		STATE PROJECT NO.: 61307C-N3803				
		George & Associates Consulting Engineers, Inc. ENGINEERING LICENSE NO. 20767 1987 Commonwealth of Florida - FL 32503 PHONE 850.521.0344 - FAX 850.521.0345				
		Department of Environmental Protection Division of Recreation and Parks Bureau of Design and Construction 3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157				
		Professional Registration JAMES H. PETERSON IV No. 80485 State of Florida P.E. # 80485				

C407
Approved
4/24/2025
Lisa Word
1/16/2025

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WEST BOUND TURN LANE CROSS SECTIONS

HORIZ SCALE: 1" = 10' VERT. SCALE: 1" = 5'

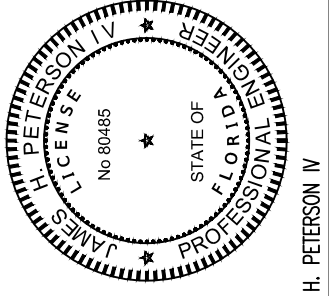
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CAMP HELEN STATE PARK		DESIGNER: SMU		ISSUE DATE: 11/11/2024 100% PLANS		SYMBOL		REVISION		DATE	
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PROJECT TITLE		Department of Environmental Protection Division of Recreation and Parks Bureau of Design and Construction 3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157									

		<p>George & Associates Consulting Engineers, Inc. ONE UNIVERSITY CENTER DRIVE, SUITE 100 TALLAHASSEE, FLORIDA 32303 TEL: (904) 241-1111 FAX: (904) 241-1112 E-MAIL: GANDASSOCIATES@GANDASSOCIATES.COM 1967 Commonwealth Lane, Suite 200, Tallahassee, FL 32303 PHONE: (904) 521-0334 - FAX: (904) 521-0345</p>		ISSUE DATE: 11/11/2024 100% PLANS		SYMBOL		REVISION		DATE	
CAMP HELEN STATE PARK		CONSULTANT:		COMP. FILE NO.: 21-5436		SYMBOL		SYMBOL		DATE	
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PROJECT TITLE		Department of Environmental Protection Division of Recreation and Parks Bureau of Design and Construction 3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157									

CAMP HELEN STATE PARK		DESIGNER: SMU		ISSUE DATE: 11/11/2024 100% PLANS		SYMBOL		REVISION		DATE	
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PROJECT TITLE		Department of Environmental Protection Division of Recreation and Parks Bureau of Design and Construction 3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157									

PROFESSIONAL REGISTRATION




STATE OF FLORIDA

PROFESSIONAL ENGINEER

JAMES H. PETERSON IV

No. 80485

CONSULTANT



George & Associates
Consulting Engineers, Inc.
1927 Commonwealth Lane
Tallahassee, FL 32303
PHONE: 850.521.0344 FAX: 850.521.0345

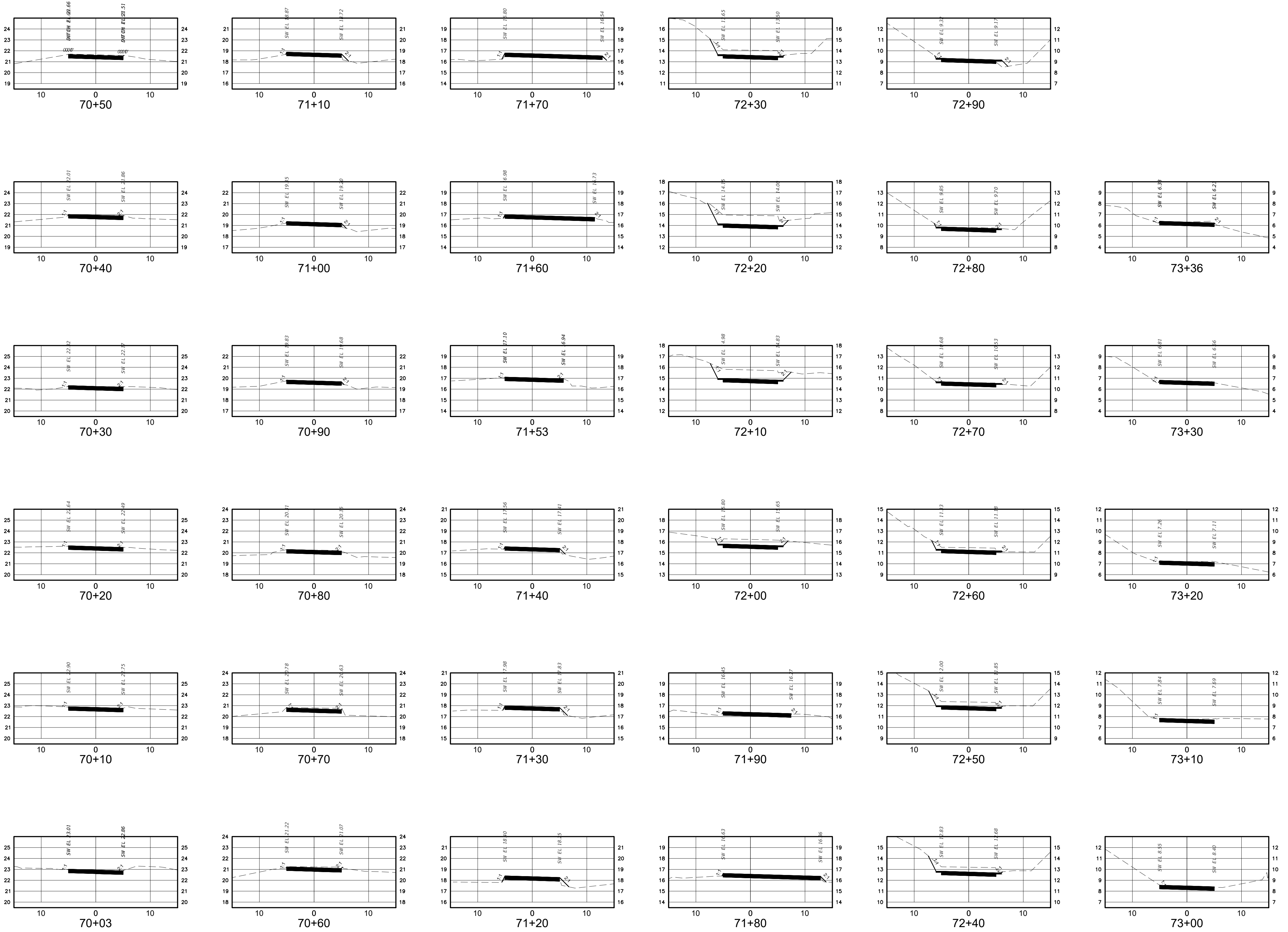
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Approved
4/24/2025 11:30:0036
Lisa Ward
1/16/2025

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MULTI-USE PATH CROSS SECTIONS

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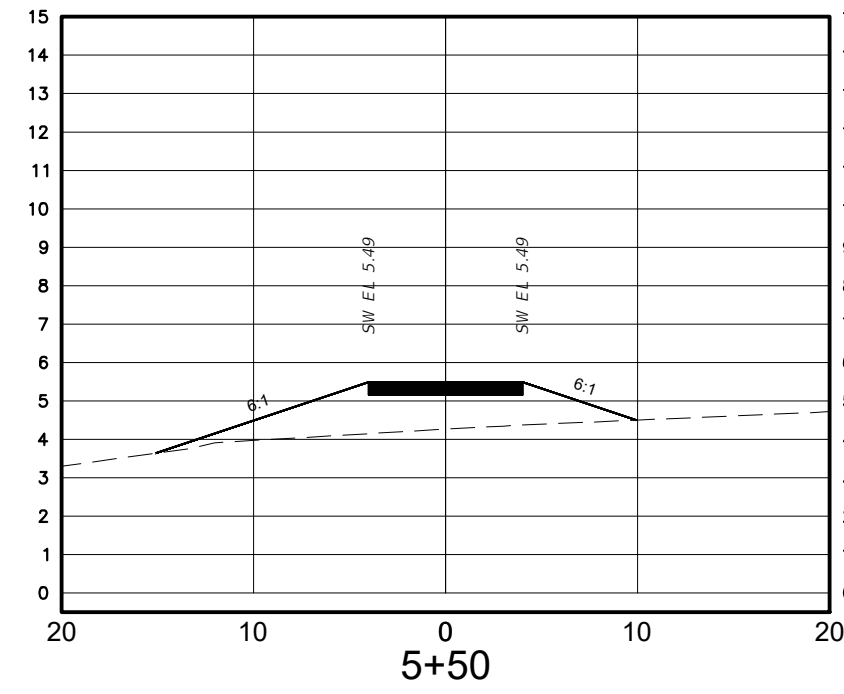
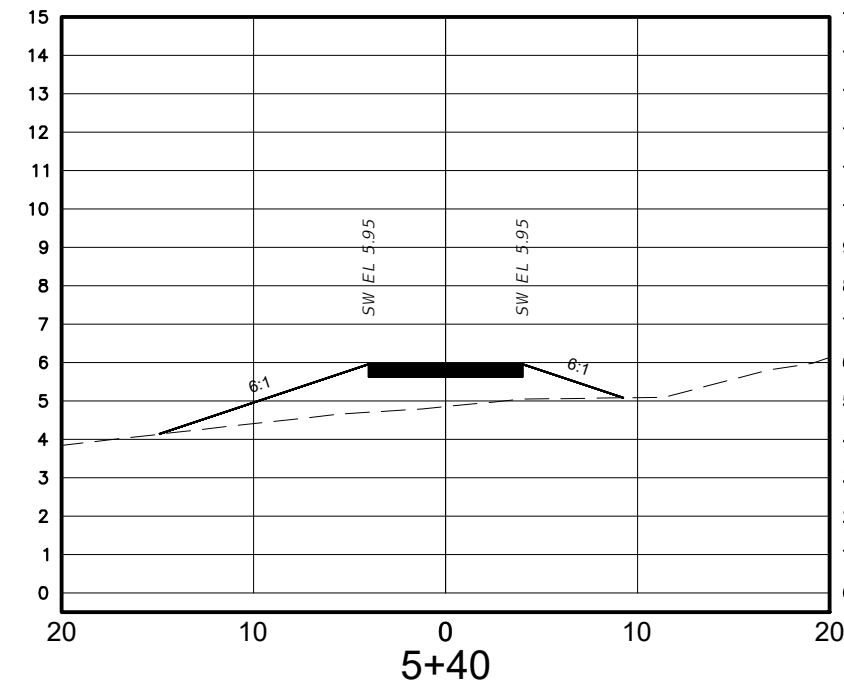
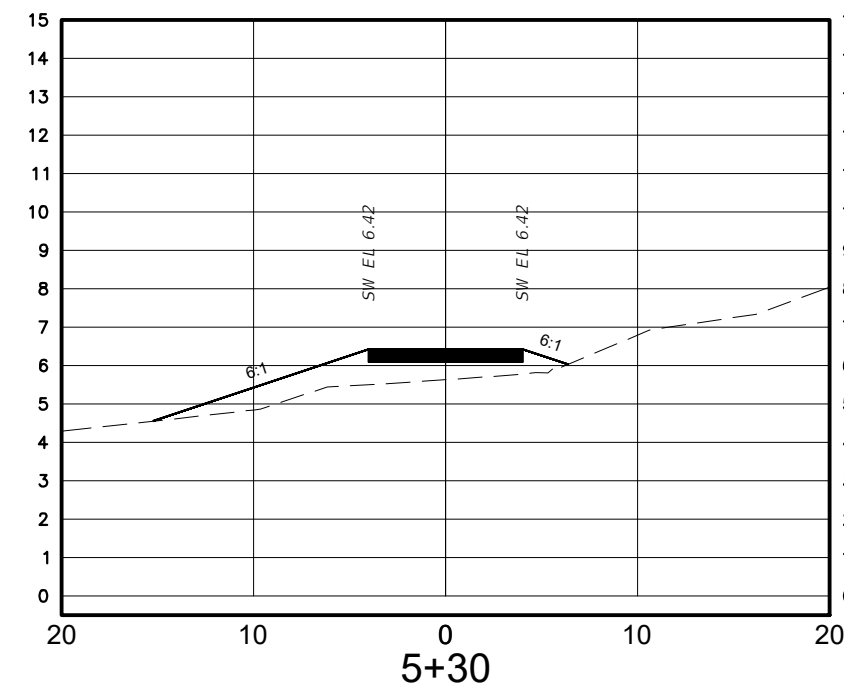
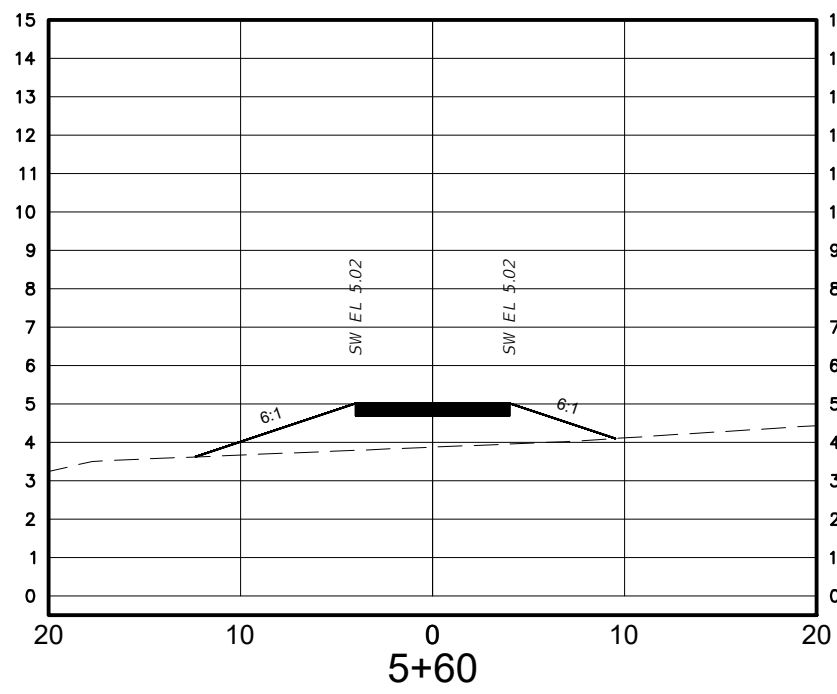
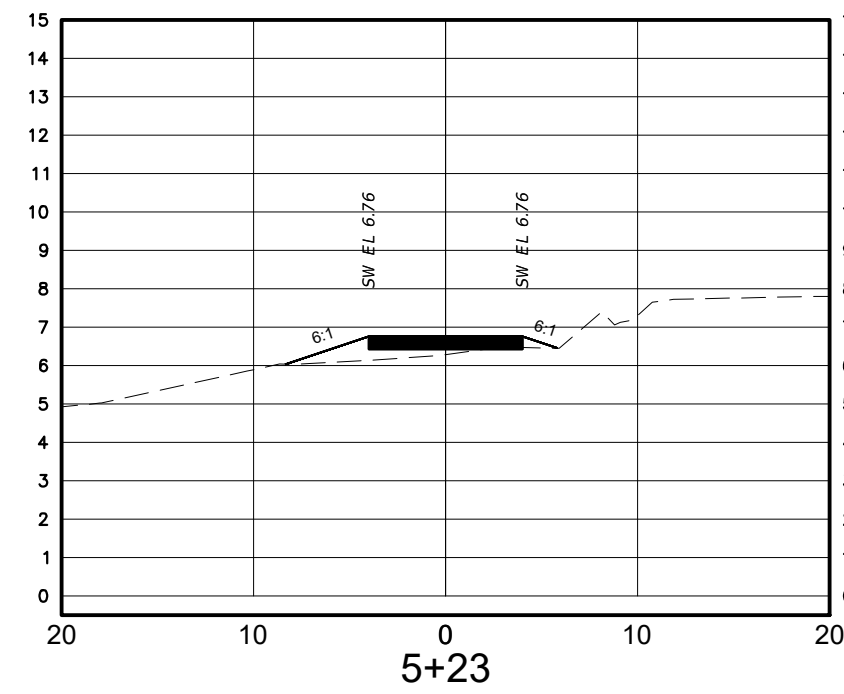


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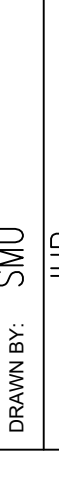




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PROJECT TITLE		MULTI-USE PATH CROSS SECTIONS		APPROVED		JAMES H. PETERSON IV		No. 80485		STATE OF FLORIDA		P.E. # 80485	
PROJECT TITLE		PARK IMPROVEMENT		APPROVED		JAMES H. PETERSON IV		No. 80485		STATE OF FLORIDA		P.E. # 80485	
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CONCRETE PATH EXTENSION CROSS SECTIONS

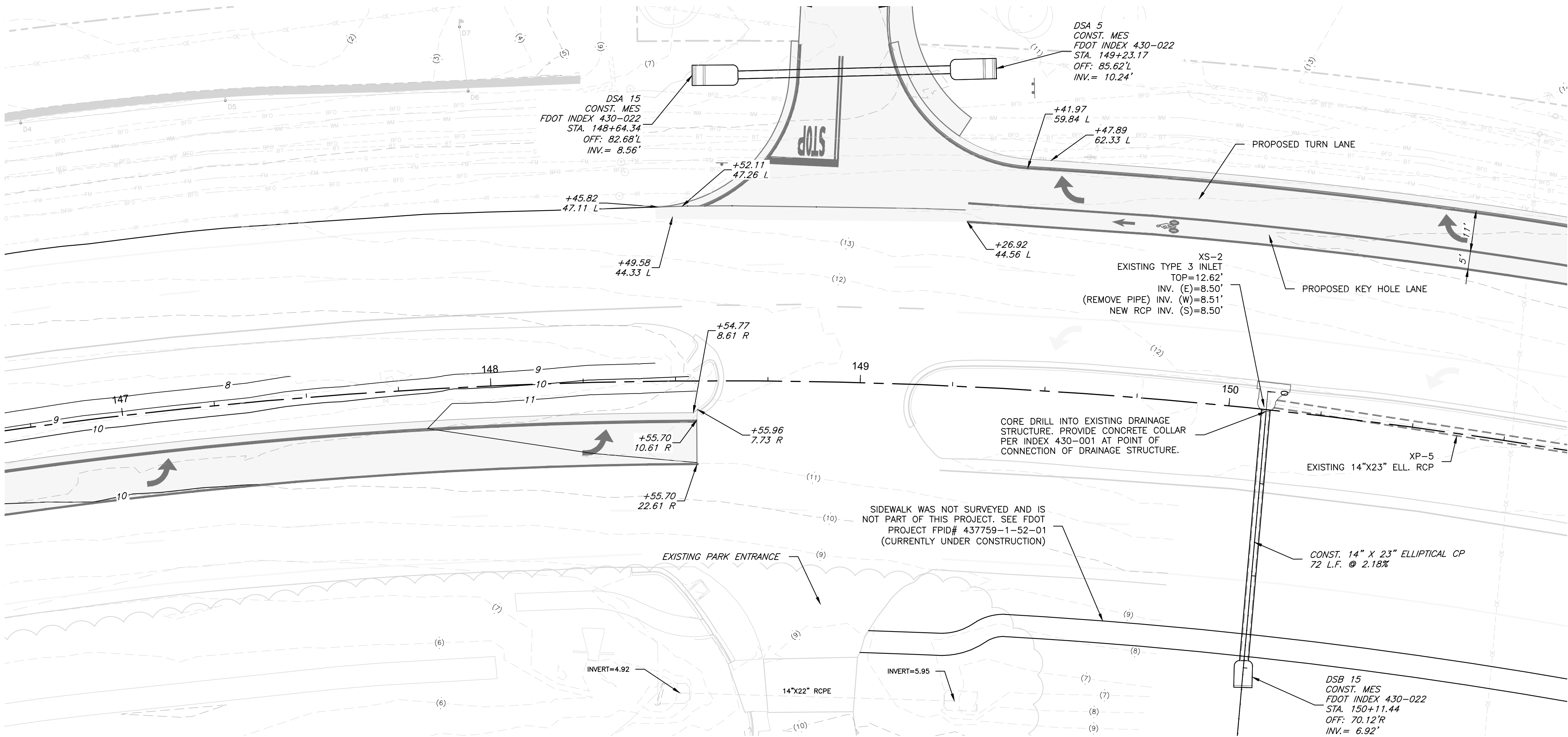
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NOT FOR CONSTRUCTION

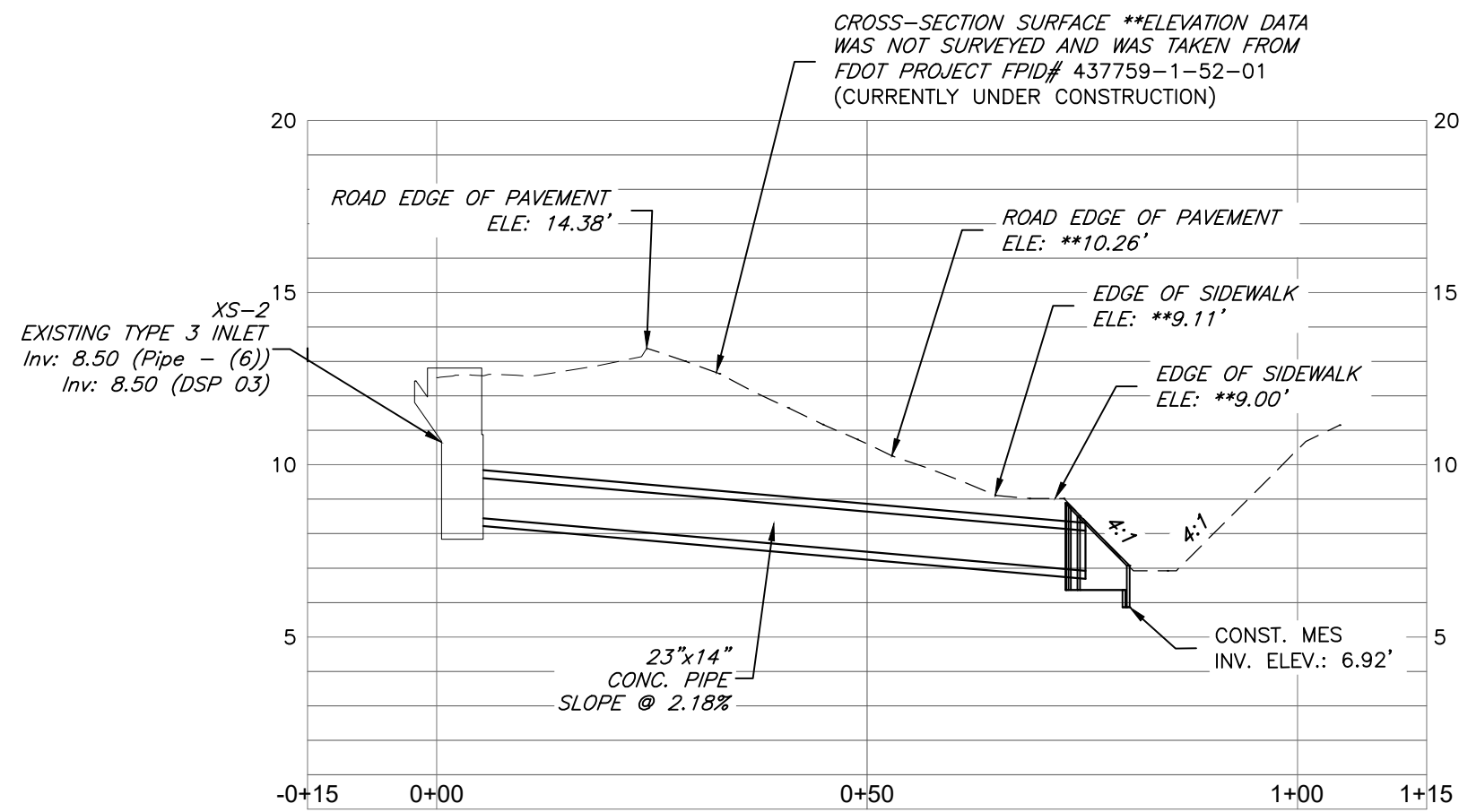
SHEET NO.		CAMP HELEN STATE PARK		PROFESSIONAL REGISTRATION		<div><div>George & Associates Consulting Engineers, Inc. <small>ONE - COMMERCIAL UNIVERSITY CENTER BUILDING, SUITE 102 1967 Commonwealth Lane, Suite 200, Tallahassee, FL 32303 PHONE: 850.5210344 - FAX: 850.5210345</small></div><div></div></div>										<div><div>Department of Environmental Protection Division of Recreation and Parks Bureau of Design and Construction 3900 Commonwealth Boulevard, Tallahassee, FL 32309 (850) 245-2157</div></div>									
SHEET TITLE		CONCRETE PATH EXTENSION CROSS SECTIONS				DESIGNER: SMU		ISSUE DATE: 11/11/2024		100% PLANS		SYMBOL		REVISION		DATE		SYMBOL		REVISION		DATE			
						DRAWN BY: SMU		COMP. FILE NO.: 21-5436																	
PROJECT TITLE		PARK IMPROVEMENT		JAMES H. PETERSON IV State of Florida P.E. # 89485		REVIEWED BY: JHP		STATE PROJECT NO.: 61307C-N3803																	

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DRAINAGE PLAN TURN LANE

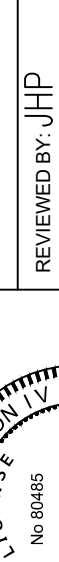
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DRAINAGE OUTFALL PROFILE

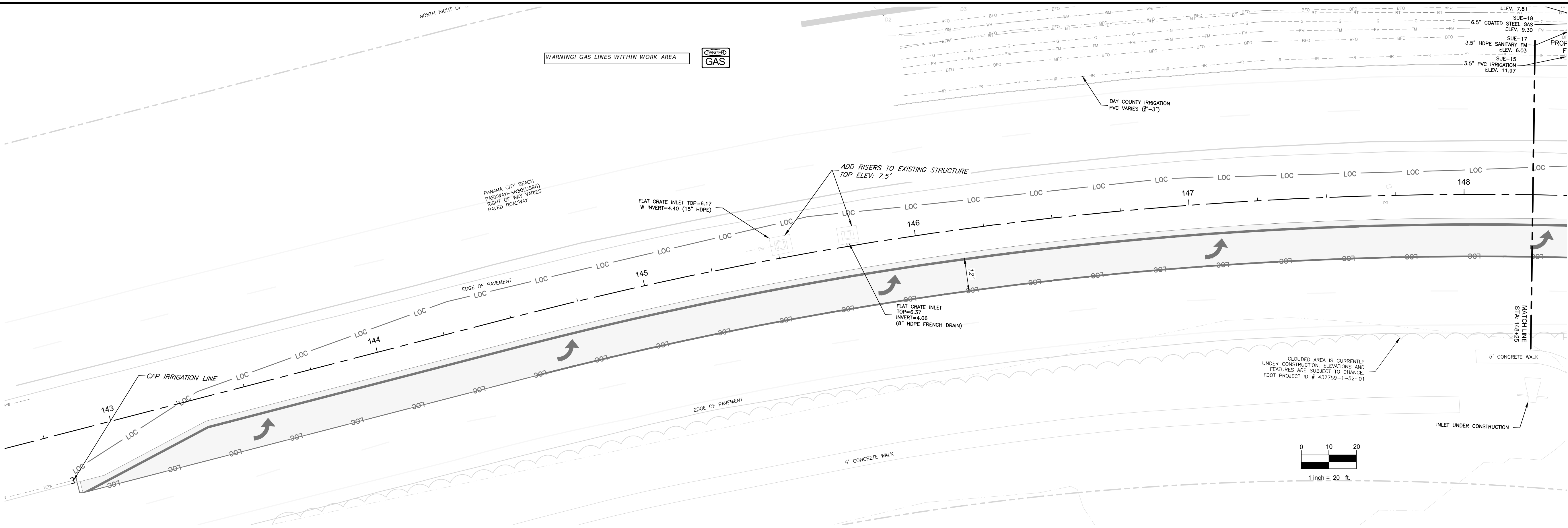
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NOT FOR CONSTRUCTION

PROFESSIONAL REGISTRATION									
									
JAMES H. PETERSON IV State of Florida P.E. # 88485									
PROFESSIONAL ENGINEER									
STATE OF FLORIDA									
JAMES H. PETERSON IV State of Florida P.E. # 88485									
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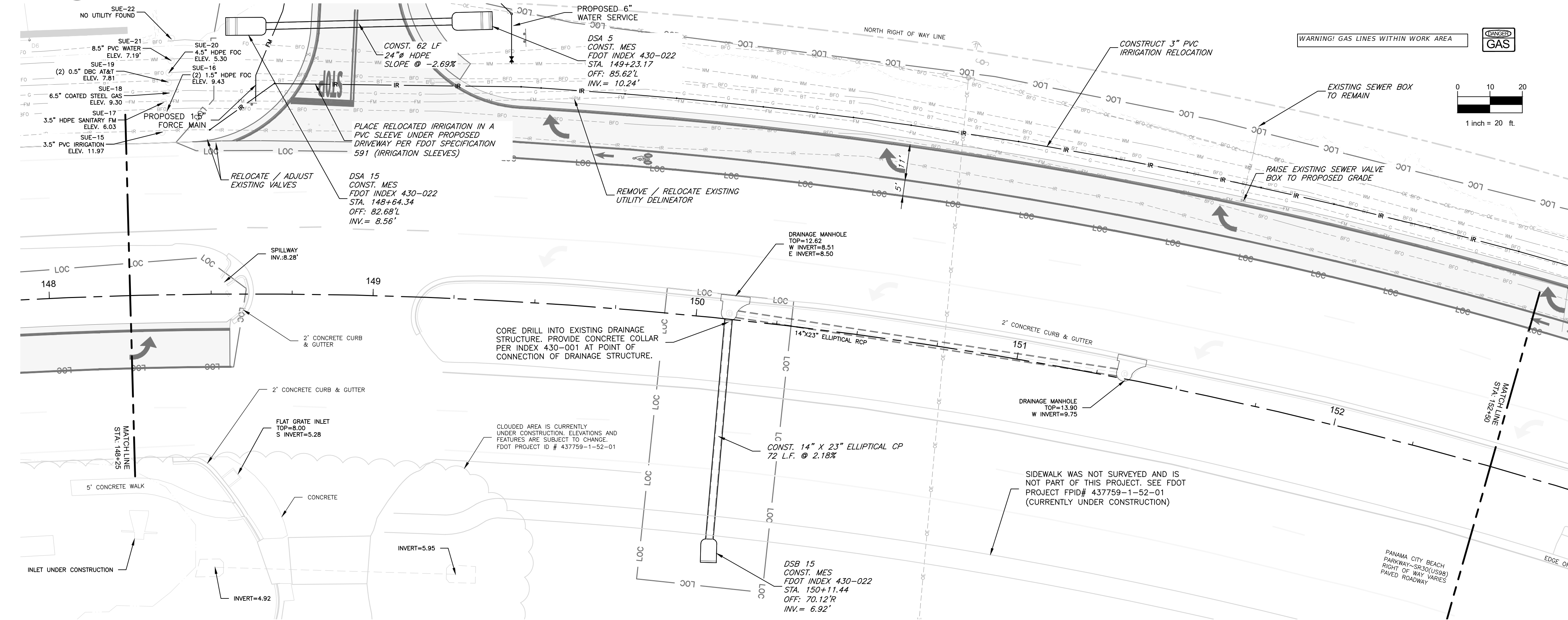
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11/16/2025

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TURN LANE UTILITY PLAN

SCALE: 1" = 20'



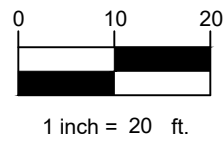
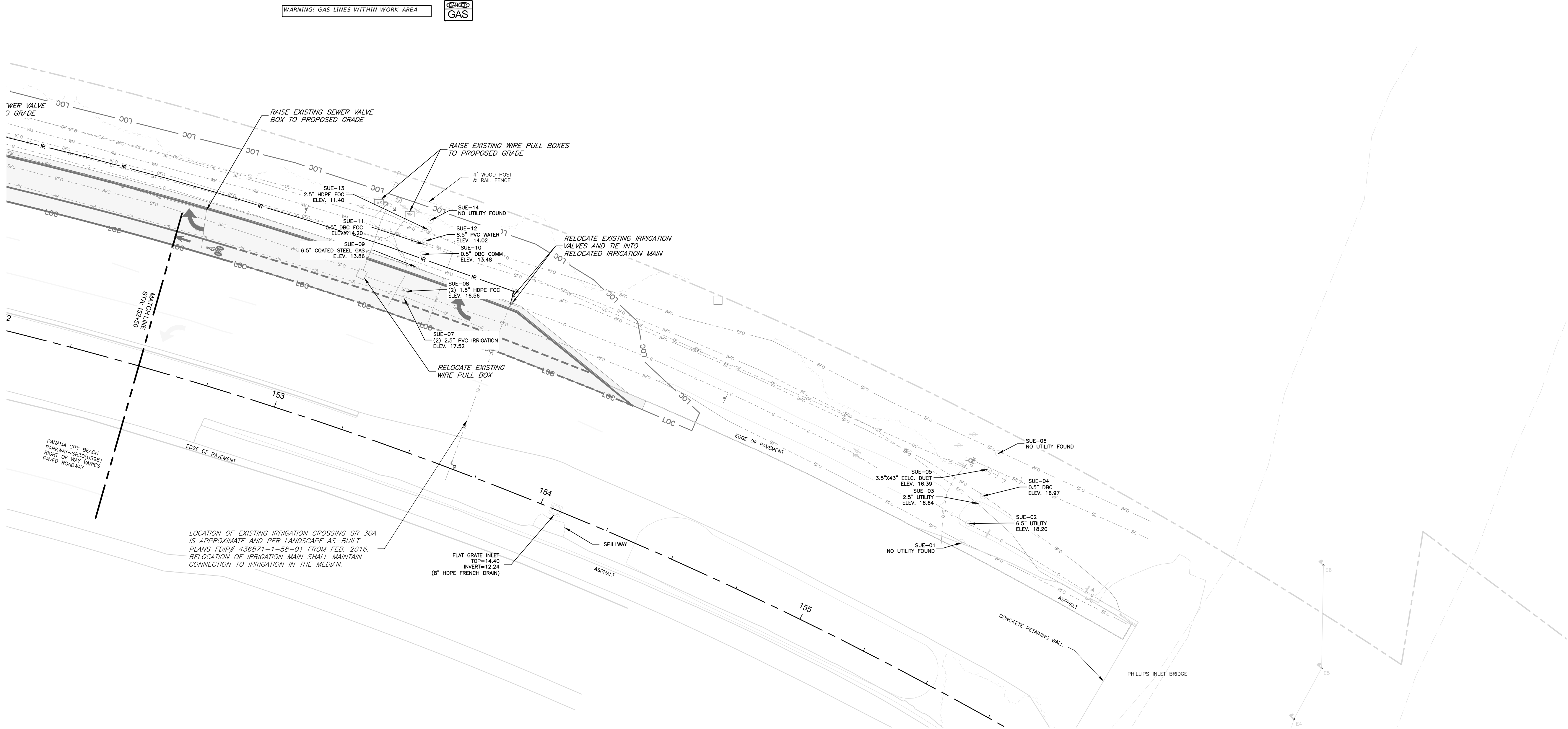
TURN LANE UTILITY PLAN

SCALE: 1" = 20'

NOT FOR CONSTRUCTION

DATE	REVISION	SYMBOL	DATE	REVISION	SYMBOL
Department of Environmental Protection Division of Recreation and Parks Bureau of Design and Construction 3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157					
George & Associates Consulting Engineers, Inc. 1907 Commonwealth Lane, Tallahassee, FL 32303 PHONE: 850/5210344 - FAX: 850/5210345					
PROFESSIONAL REGISTRATION JAMES H. PETERSON IV No. 88465 State of Florida P.E. # 88465					
CAMP HELEN STATE PARK TURN LANE UTILITY PLAN PARK IMPROVEMENT					
SHEET TITLE PROJECT TITLE SHEET NO.					
ISSUE DATE: 11/11/2024 100% PLANS COMP. FILE NO.: 21-5438 STATE PROJECT NO.: 61307C-N3803					
DESIGNER: SMU DRAWN BY: SMU REVIEWED BY: JHP					
Approved 10/24/2024 10/24/2024 11/16/2025					

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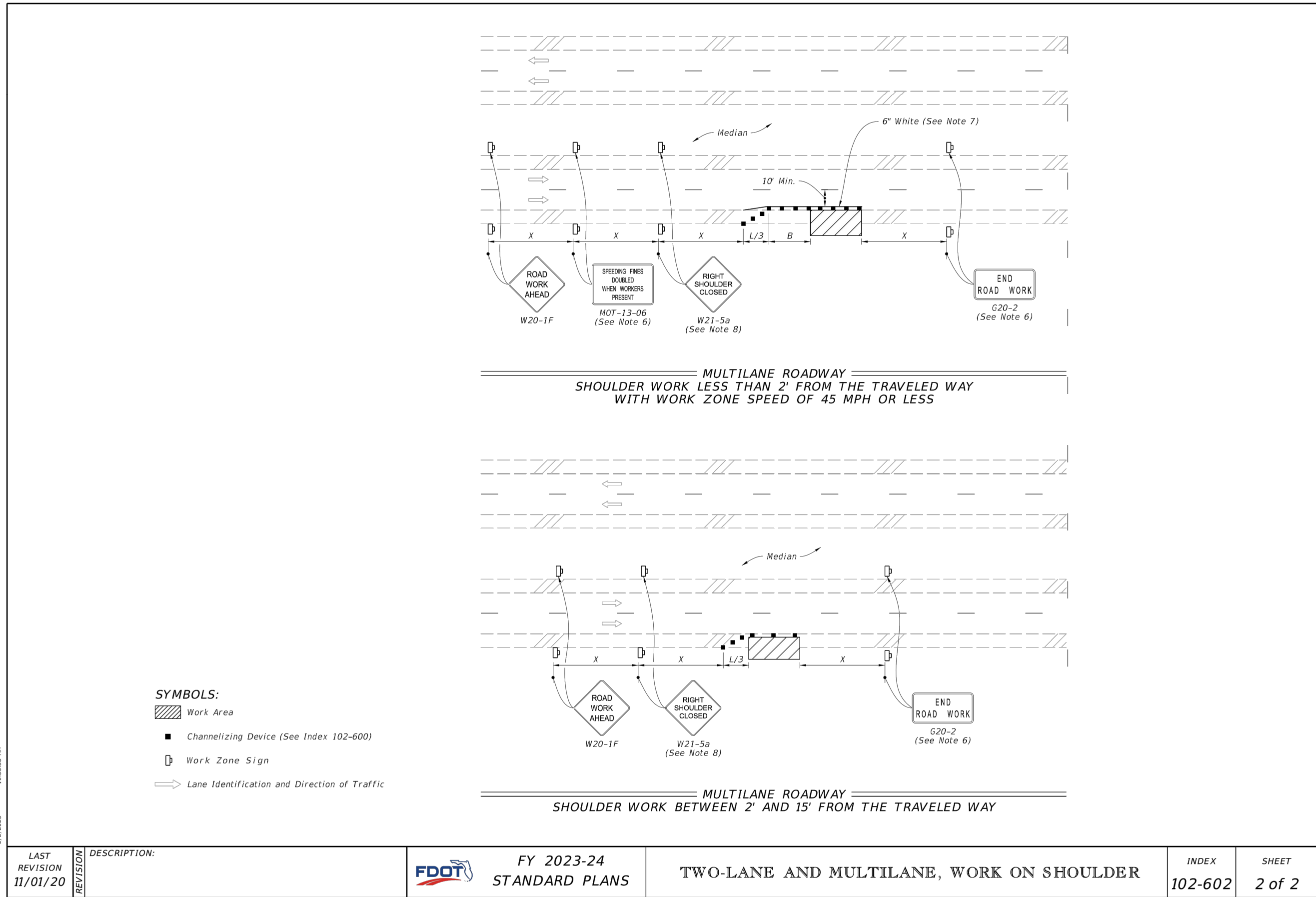
CAMP HELEN STATE PARK		DESIGNER: SMU	ISSUE DATE: 11/11/2024	REVISION	SYMBOL	DATE
TURN LANE UTILITY PLAN		DRAWN BY: SMU	COMP. FILE NO.: 21-5436			
PARK IMPROVEMENT		REVIEWED BY: JHP	STATE PROJECT NO.: 61307C-N3803			
SHEET NO.		Department of Environmental Protection Division of Recreation and Parks Bureau of Design and Construction 3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157				
PROJECT TITLE		George & Associates Consulting Engineers, Inc. C.E. - PROFESSIONAL ENGINEERING LICENSE NO. 27070, FL 32303 1987 Commonwealth Lane, Tallahassee, FL 32303 PHONE: 850/5210344 - FAX: 850/5210345				
PROFESSIONAL REGISTRATION		 JAMES H. PETERSON, P.E. # 88485 State of Florida, P.E. #				

Approved
10/24/2024 09:13:00036
11/16/2025

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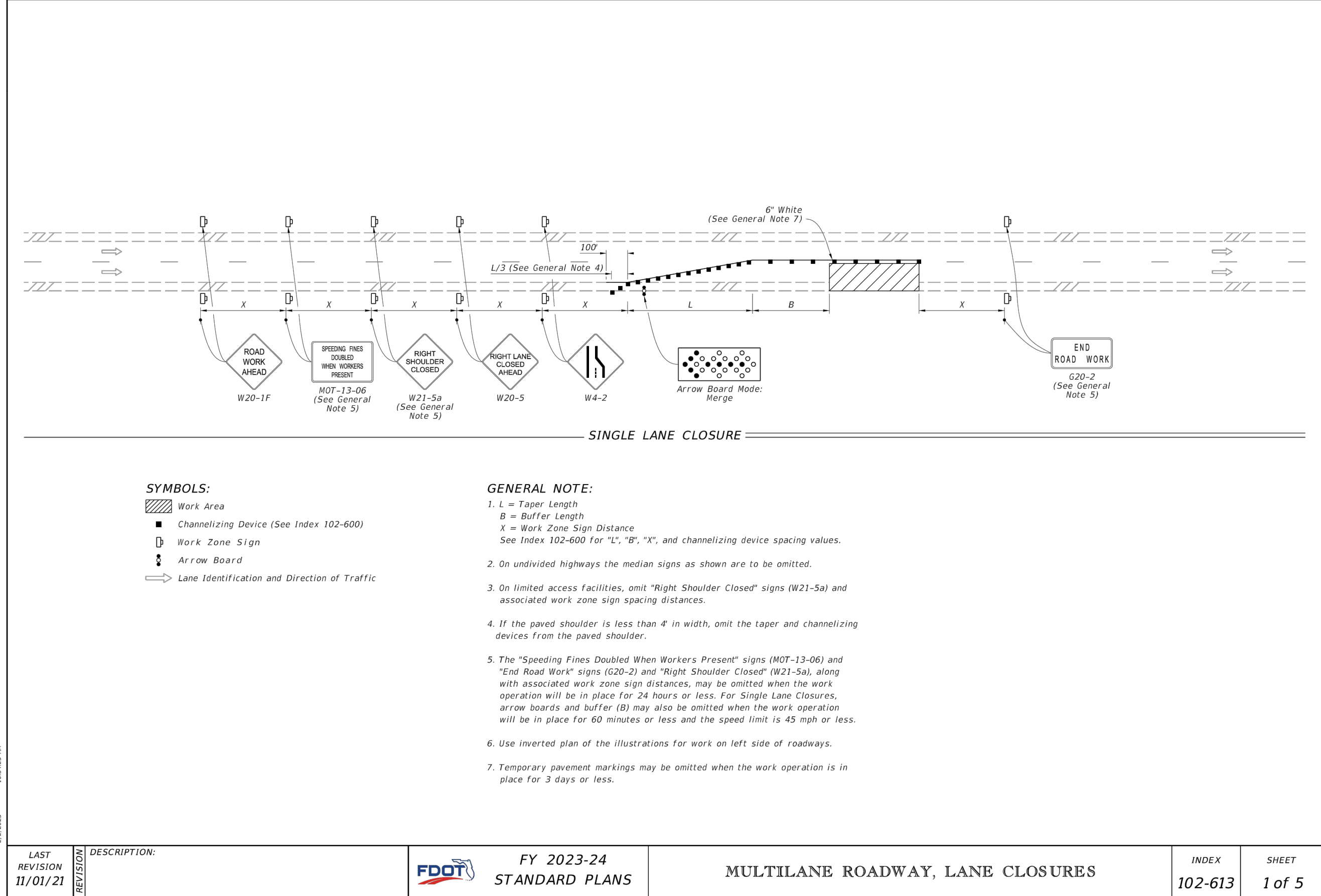
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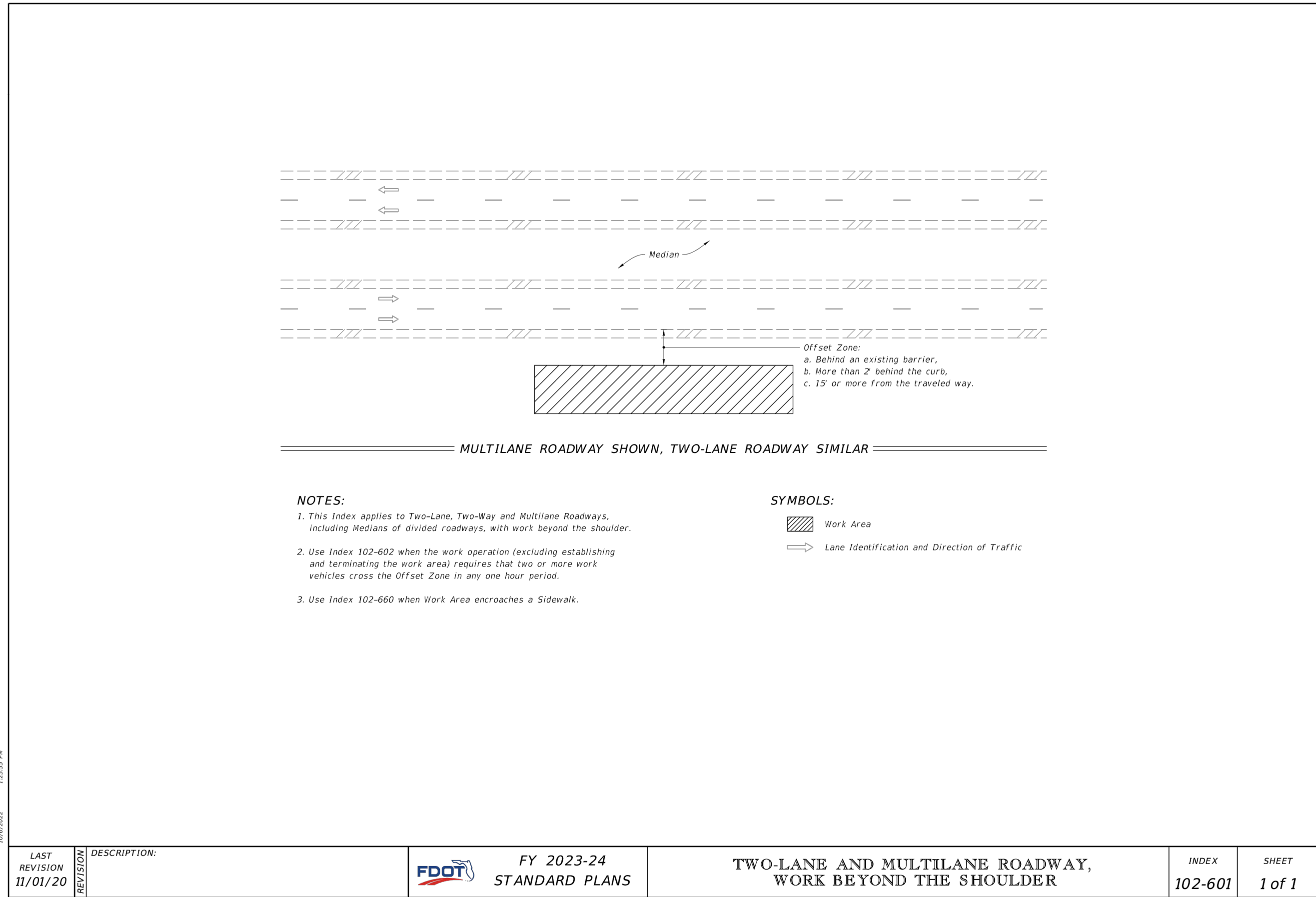
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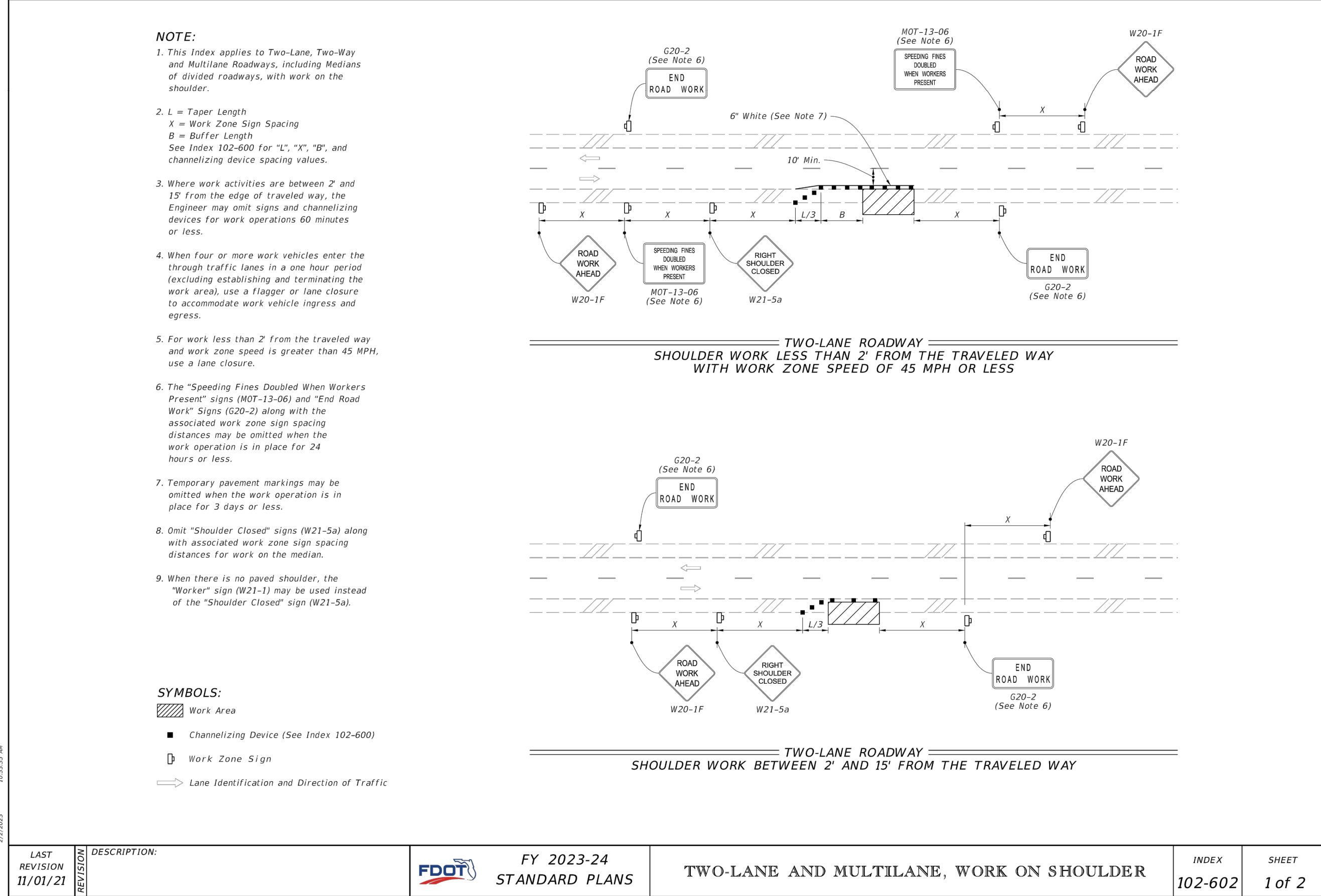
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SHEET NO.

SHEET TITLE

CAMP HELEN STATE PARK

TRAFFIC CONTROL PLAN

PROFESSIONAL REGISTRATION

DESIGNER: SMU

DRAWN BY: SMU

REVIEWED BY: JHP

ISSUE DATE: 11/11/2024

COMP. FILE NO. 21-5438

STATE PROJECT NO. 61307C-N3903

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11/16/2025

PROJECT TITLE

PARK IMPROVEMENT

PROFESSIONAL REGISTRATION

DESIGNER: SMU

DRAWN BY: SMU

REVIEWED BY: JHP

ISSUE DATE: 11/11/2024

COMP. FILE NO. 21-5438

STATE PROJECT NO. 61307C-N3903

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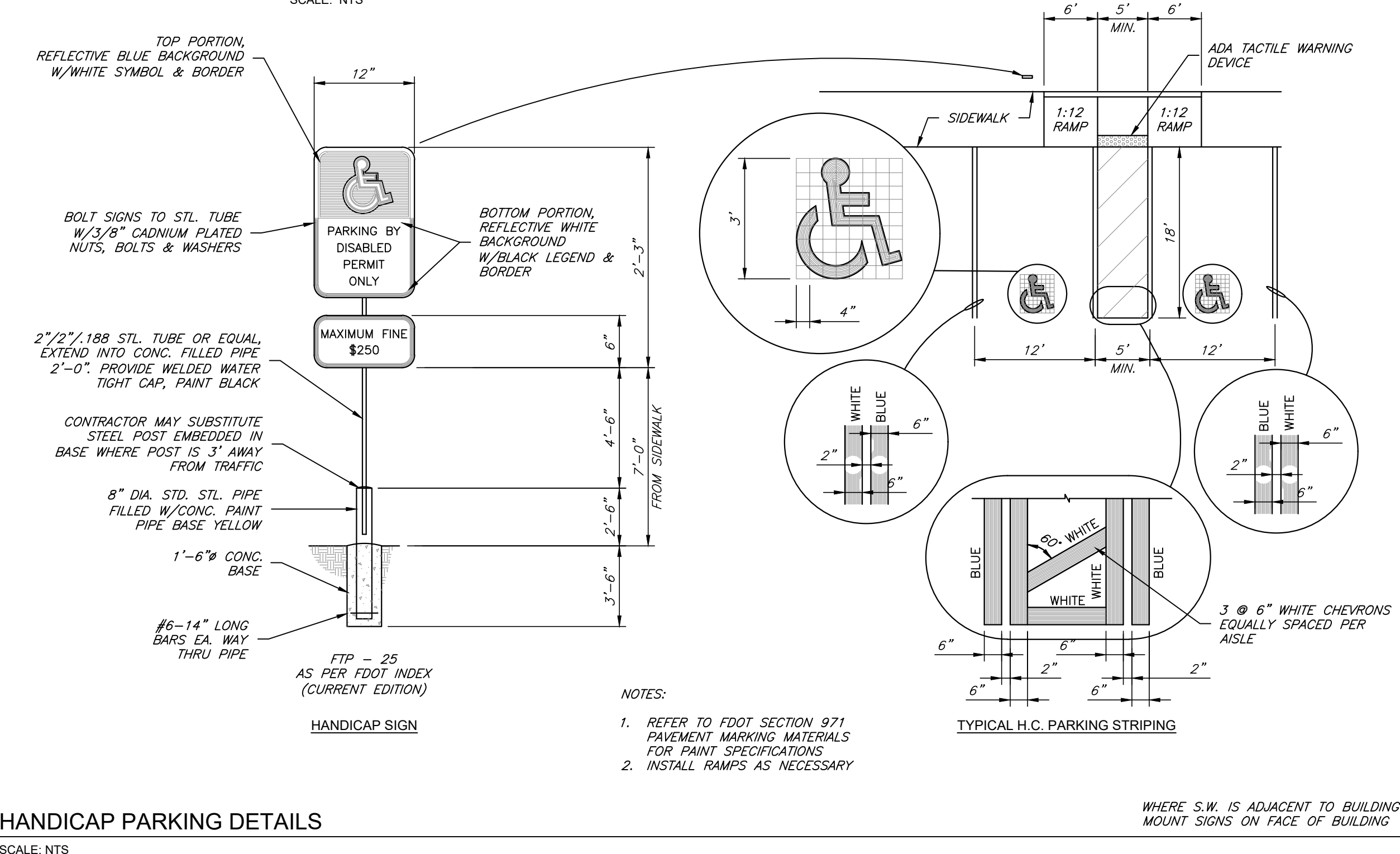
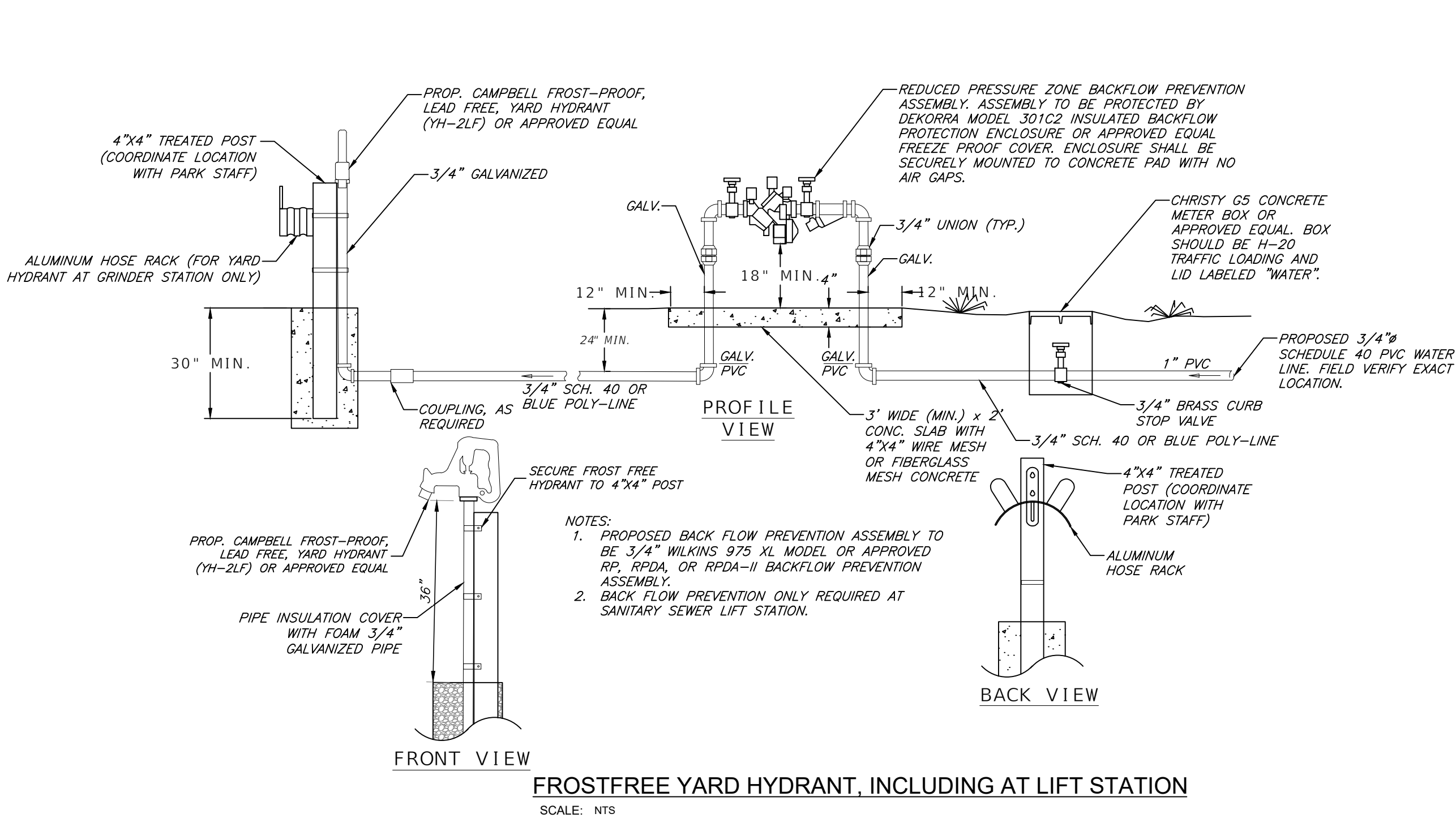
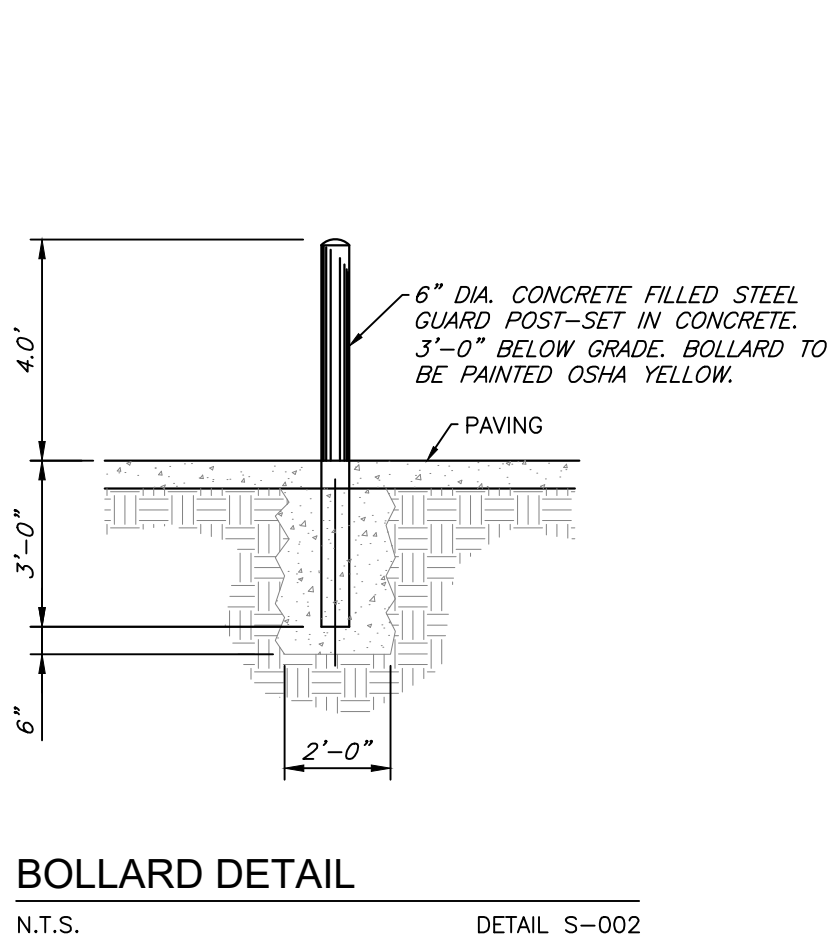
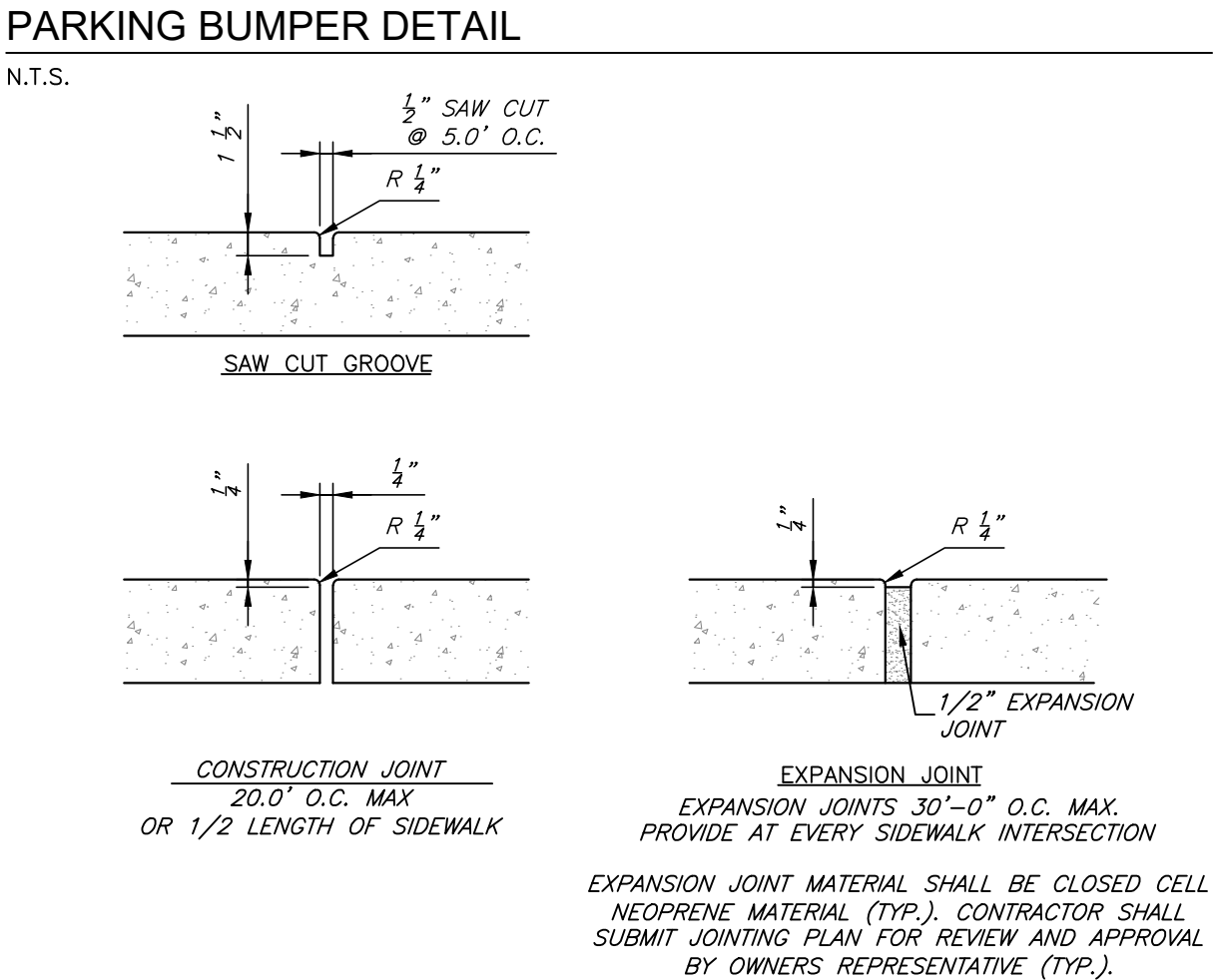
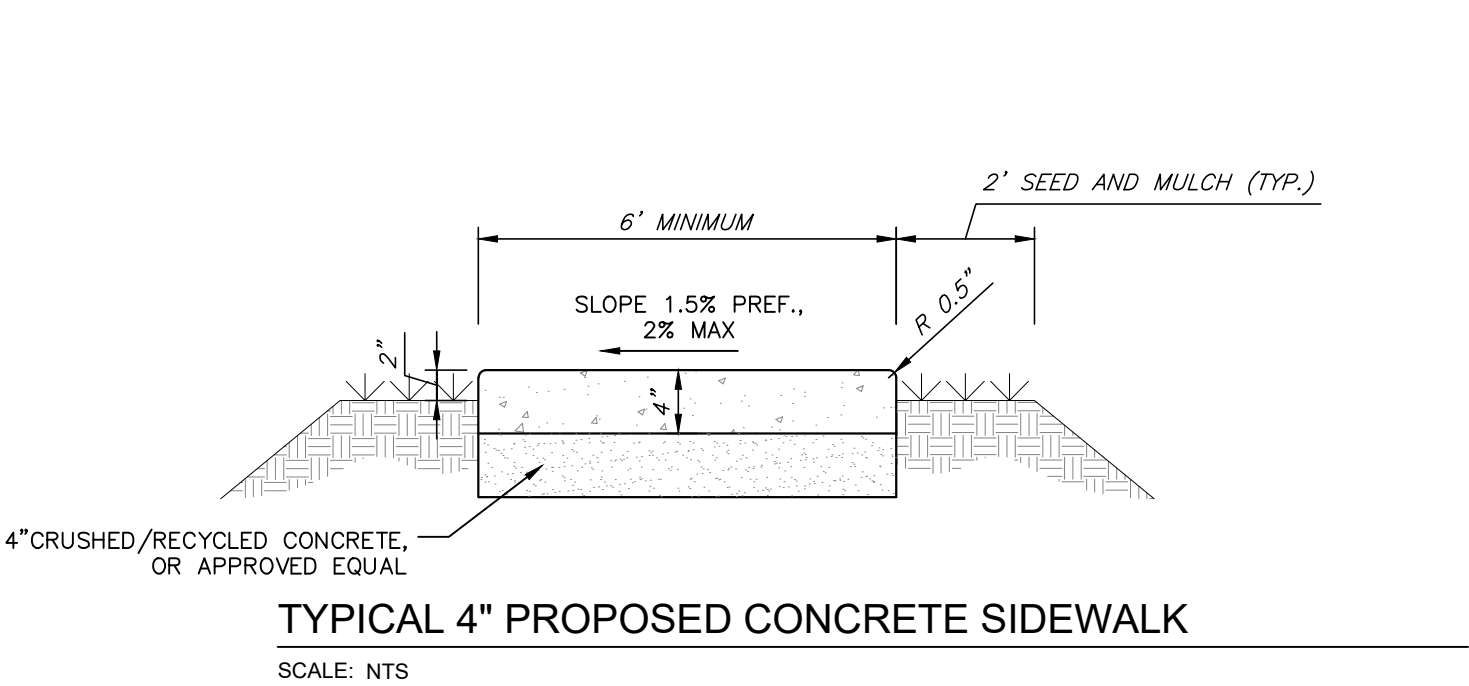
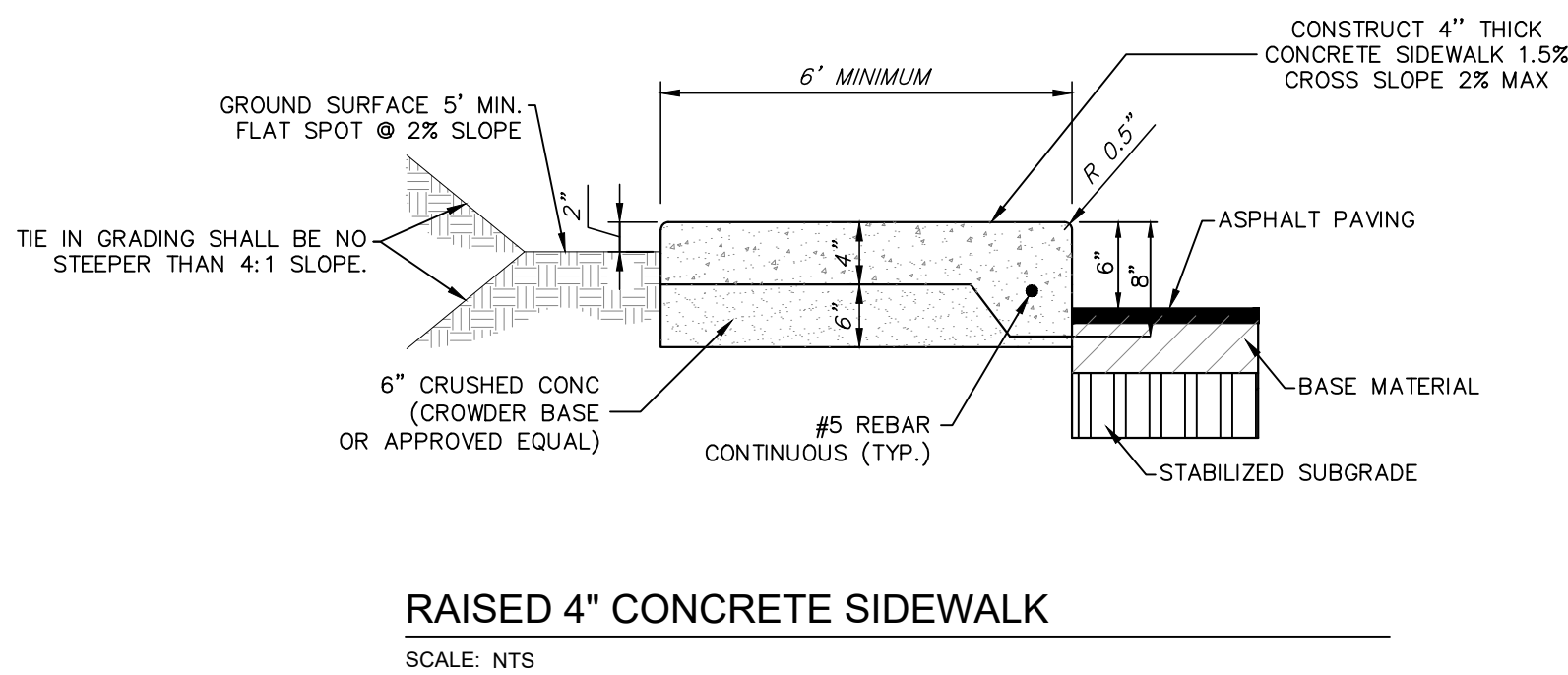
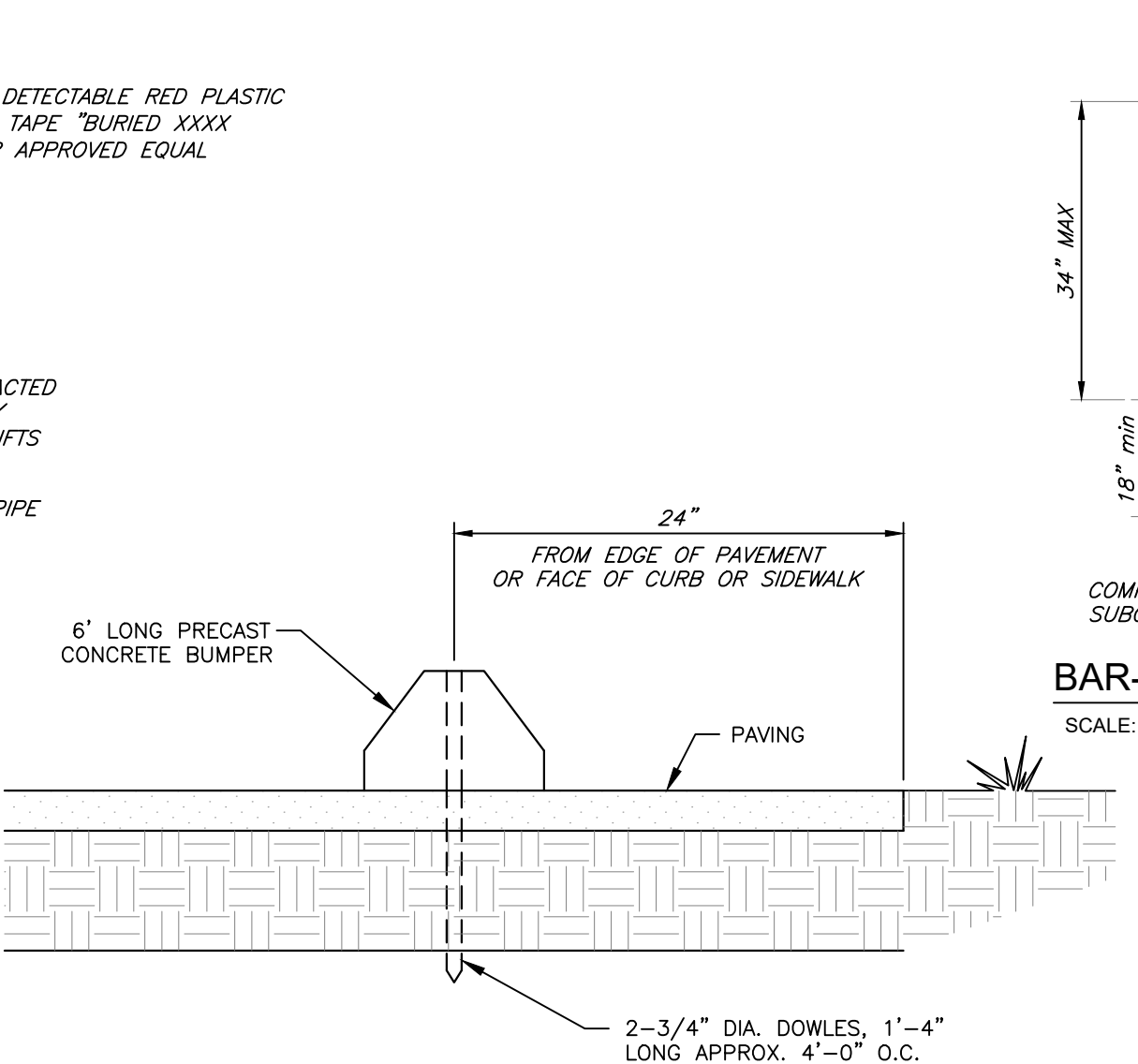
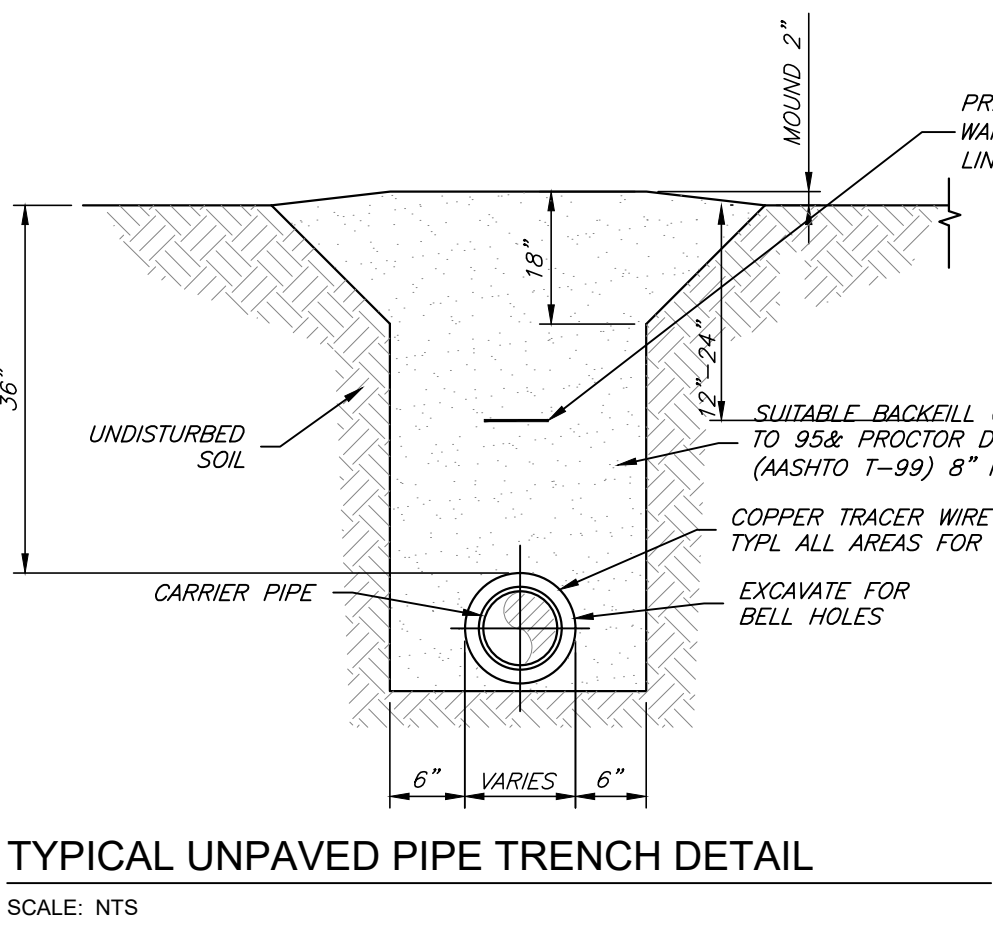
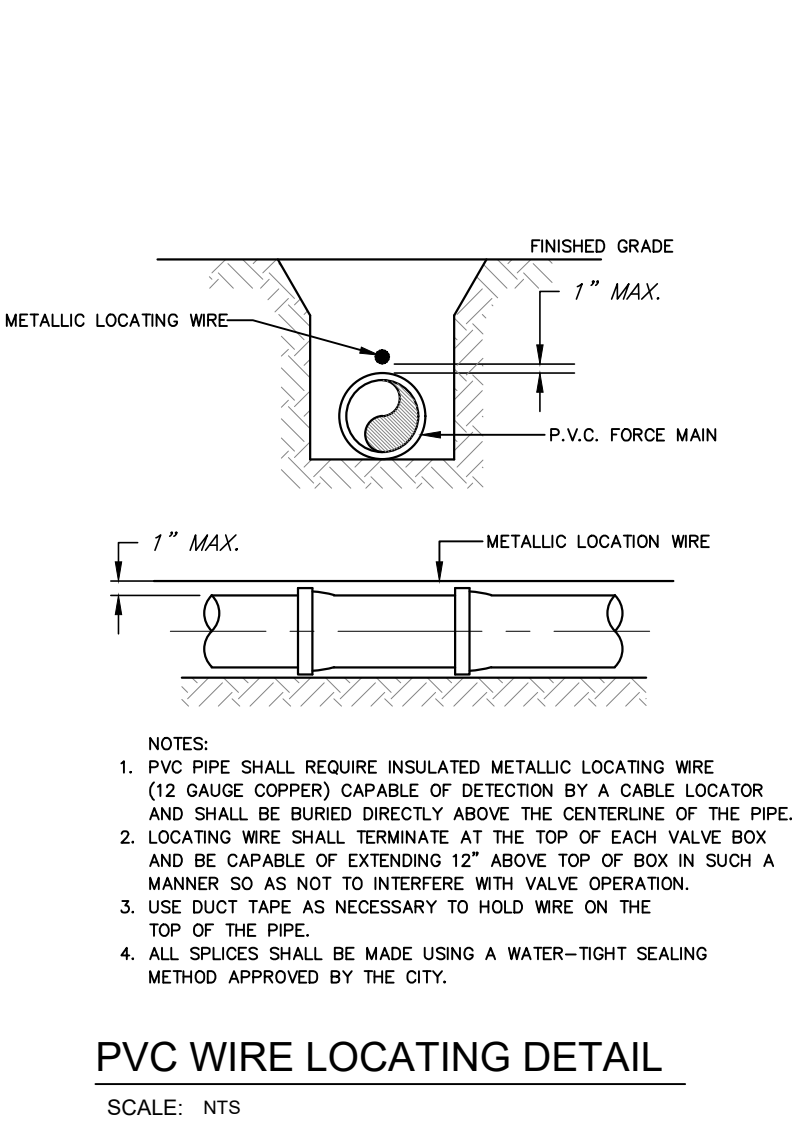
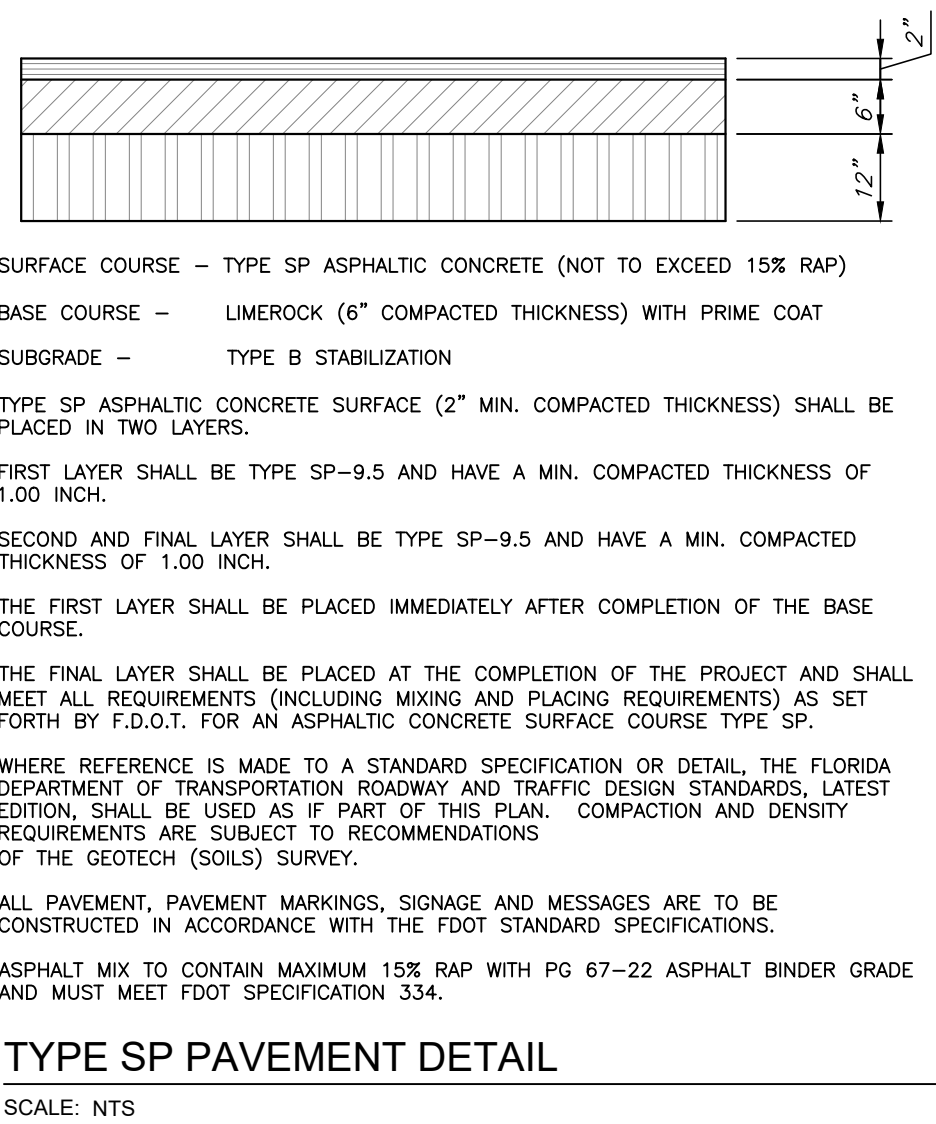
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2024-09-10 00036
11/16/2025



CONSTRUCTION DETAILS

NOT FOR CONSTRUCTION

DATE	REVISION	SYMBOL	DATE	REVISION	SYMBOL	ISSUE DATE: 11/11/2024	100% PLANS	DESIGNER: SMU	SMU	PROFESSIONAL REGISTRATION	SHEET TITLE	PROJECT TITLE
						COMP. FILE No. 21-5486	STATE PROJECT No. 61307C-N3903	DRAWN BY: SMU	REVIEWED BY: JHP		CAMP HELEN STATE PARK	CONSTRUCTION DETAILS
												PARK IMPROVEMENT

Department of Environmental Protection
Division of Recreation and Parks
Bureau of Design and Construction
3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157

George & Associates
Consulting Engineers, Inc.
CONSULTING ENGINEER, PROFESSIONAL LICENSE NO. 27074, EXPIRATION DATE 12/31/2025
1907 Commonwealth Lane, Tallahassee, FL 32303
PHONE: 850/5210344 - FAX: 850/5210345

PROFESSIONAL REGISTRATION
JAMES H. PETERSON, P.E.
No. 88485
STATE OF FLORIDA
CIVIL ENGINEERING
LICENSE NO. 27074
EXPIRATION DATE 12/31/2025

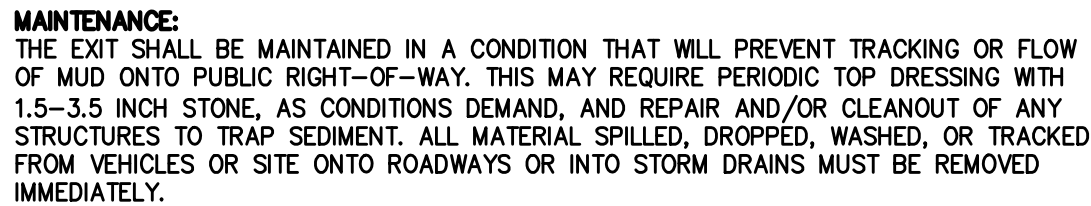
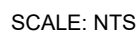
SHEET NO.
C901

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2024/11/09 1:00:03 PM
11/6/2025



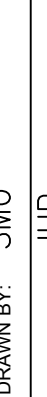
- 1.) NO CUTS SHALL BE MADE BEFORE:
(A) A TEST OF 150 P.S.I. FOR 30 MINUTES IS MADE.
- 2.) ALL TAPS MUST BE OF A SMALLER SIZE THAN THE MAIN BEING TAPPED & PLACED NO CLOSER THAN 30" OR A DISTANCE EQUAL TO (1) MAIN PIPE DIAMETER PLUS (2) TAP PIPE DIAMETERS (WHICHEVER IS LARGER) FROM A JOINT OR FITTING.
- 3.) CONTRACTOR SHALL ADHERE TO INLET BEACH WATER SYSTEM SPECIFICATIONS
- 3.) CONTRACTOR TO SUPPLY A DRY HOLE FOR TAPPING CREW TO WORK AND BACK-HOPE TO LOWER MACHINE INTO HOLE.

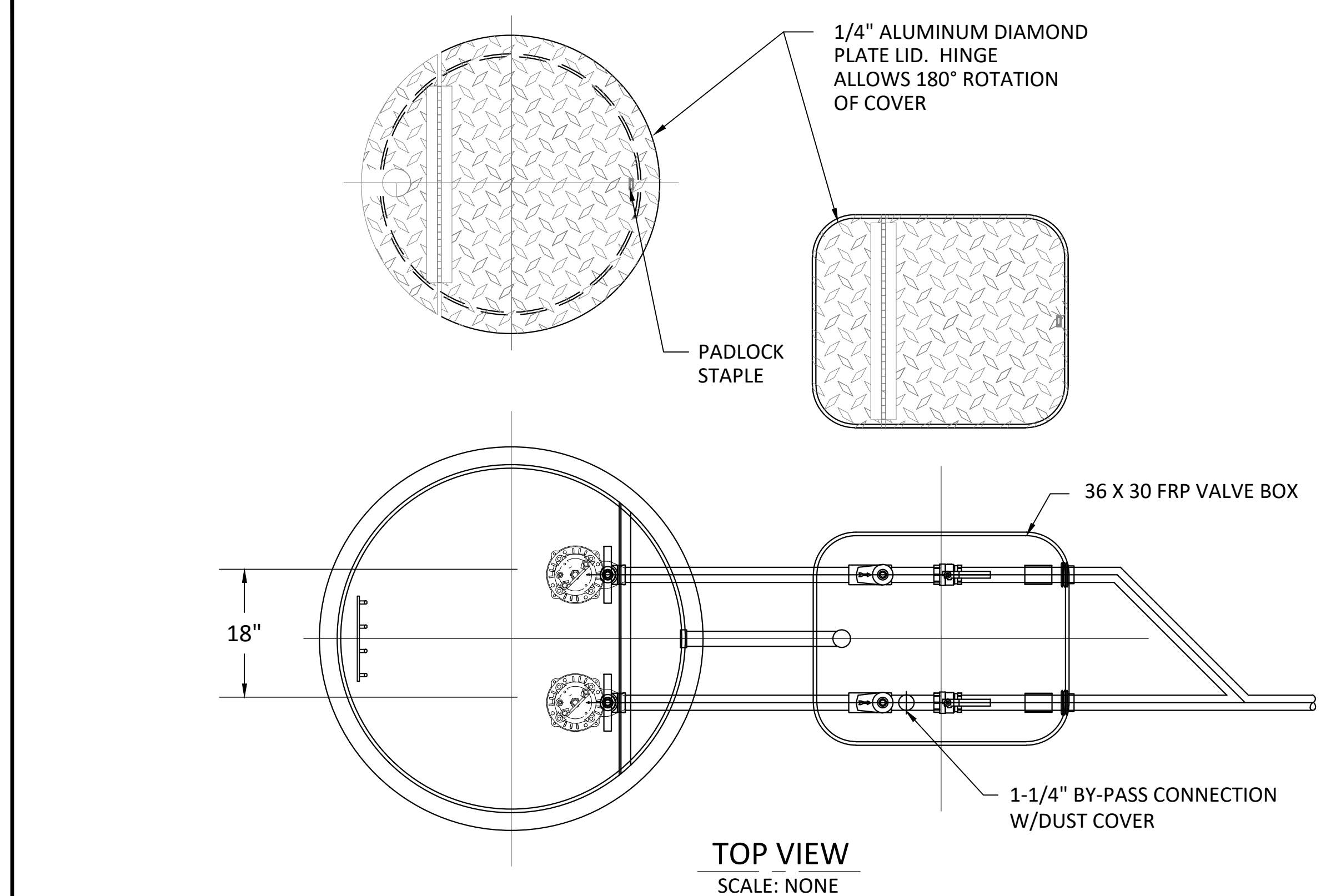
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- NOTES:**
1. AVOID LOCATING ON STEEP SLOPES OR AT CURVES ON PUBLIC ROADS.
 2. REMOVE ALL VEGETATION AND OTHER UNSUITABLE MATERIAL FROM THE FOUNDATION AREA, GRADE, AND CROWN FOR POSITIVE DRAINAGE.
 3. CURVE RADIUS SHALL BE IN ACCORDANCE WITH NATIONAL STONE ASSOCIATION R-2 (1.5"-3.5" STONE).
 4. GRAVEL PAD SHALL HAVE A MINIMUM THICKNESS OF 6".
 5. PAD WIDTH SHALL BE EQUAL FULL WIDTH AT ALL POINTS OF VEHICULAR EGRESS, BUT NO LESS THAN 20'.
 6. A DIVERSION RIDGE SHOULD BE CONSTRUCTED WHEN GRADE TOWARD PAVED AREA IS GREATER THAN 2%.
 7. INSTALL PIPE UNDER THE ENTRANCE IF NEEDED TO MAINTAIN DRAINAGE DITCHES.
 8. WHEN WASHING IS REQUIRED, IT SHOULD BE DONE ON AN AREA STABILIZED WITH CRUSHED STONE THAT DRAINS INTO AN APPROVED SEDIMENT TRAP OR SEDIMENT BASIN (DIVERT ALL SURFACE RUNOFF AND DRAINAGE FROM THE ENTRANCE TO A SEDIMENT CONTROL DEVICE).
 9. WASHRAKES AND/OR TIRE WASHERS MAY BE REQUIRED DEPENDING ON SCALE AND CIRCUMSTANCE. IF NECESSARY, WASHRAK DESIGN MAY CONSIST OF ANY MATERIAL, SLURRY, OR TRUCK TRAFFIC THAT REMOVE MUD AND DIRT.
 10. MAINTAIN AREA IN A WAY THAT PREVENTS TRACKING AND/OR FLOW OF MUD ONTO PUBLIC RIGHTS-OF-WAYS. THIS MAY REQUIRE TOP DRESSING, REPAIR AND/OR CLEANOUT OF ANY MEASURES USED TO TRAP SEDIMENT.
 11. THE GEOTEXTILE UNDERLINER MUST BE PLACED THE FULL LENGTH AND WIDTH OF THE ENTRANCE. GEOTEXTILE SELECTION SHALL BE BASED ON AASHTO M288-06 SPECIFICATION:
 - A. FOR SUBGRADES WITH CBR GREATER THAN OR EQUAL TO 3 OR SHEAR STRENGTH GREATER THAN 90 KPa, GEOTEXTILE MUST MEET REQUIREMENTS OF SECTION AASHTO M288-06 SECTION 7.3, SEPARATION REQUIREMENTS.
 - B. FOR SUBGRADES WITH CBR BETWEEN 1 AND 3 OR SHEAR STRENGTH BETWEEN 30 AND 90 KPa, GEOTEXTILE MUST MEET REQUIREMENTS OF SECTION AASHTO M288-06 SECTION 8, GEOTEXTILE PROPERTY REQUIREMENTS FOR SUBSURFACE DRAINAGE, SEPARATION, STABILIZATION, AND PERMANENT EROSION CONTROL (GEOTEXTILE PROPERTY REQUIREMENTS).

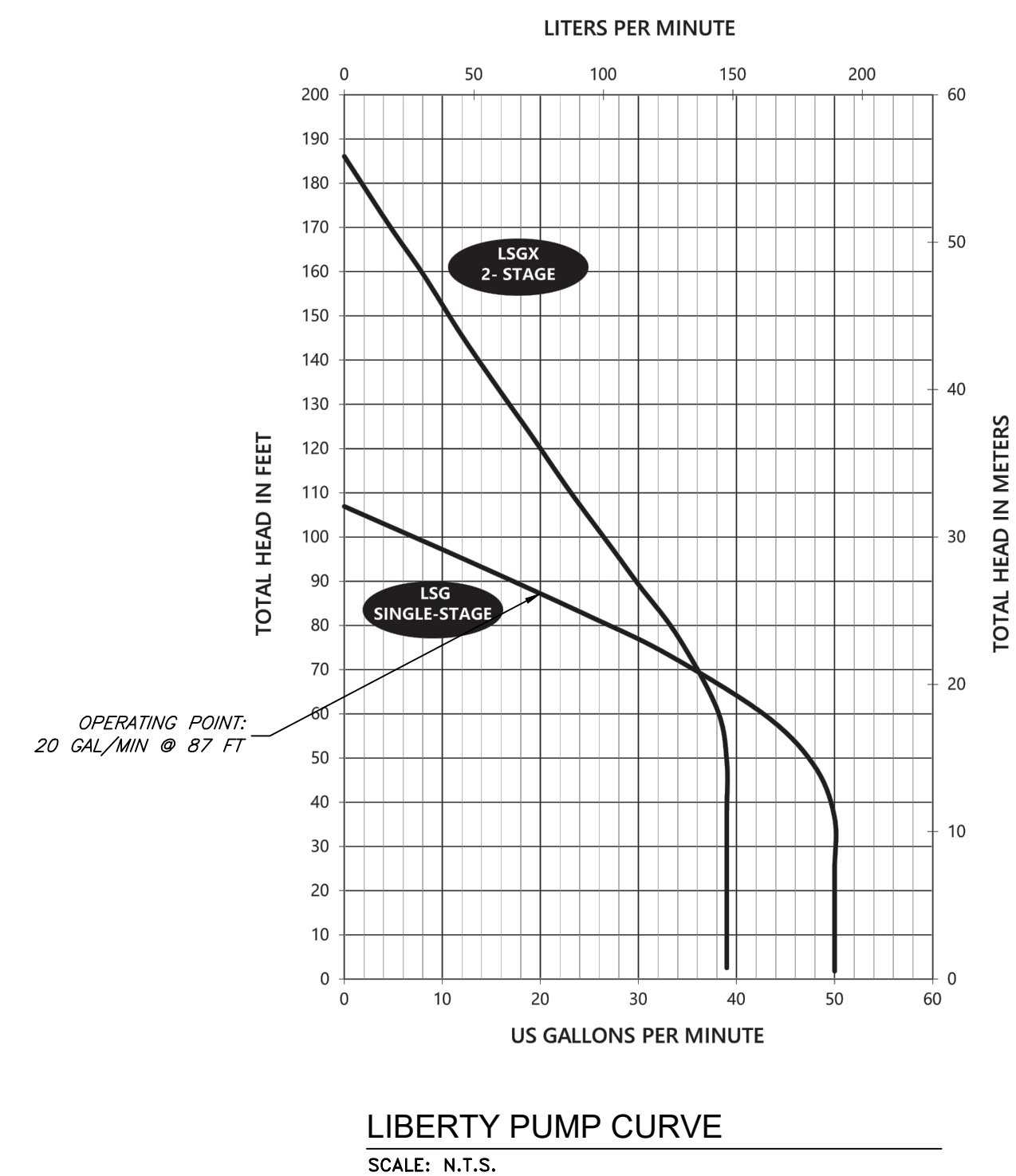
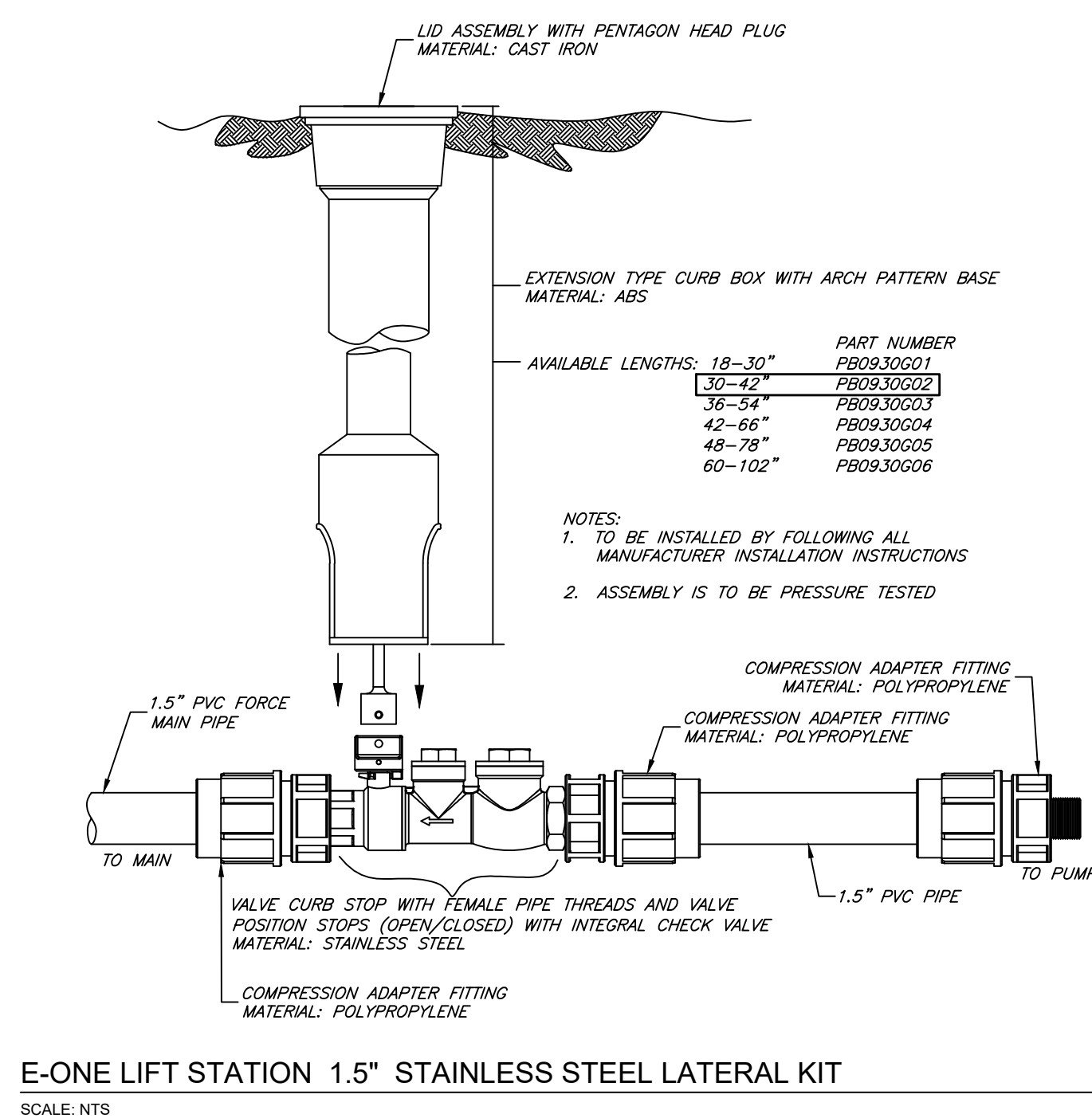
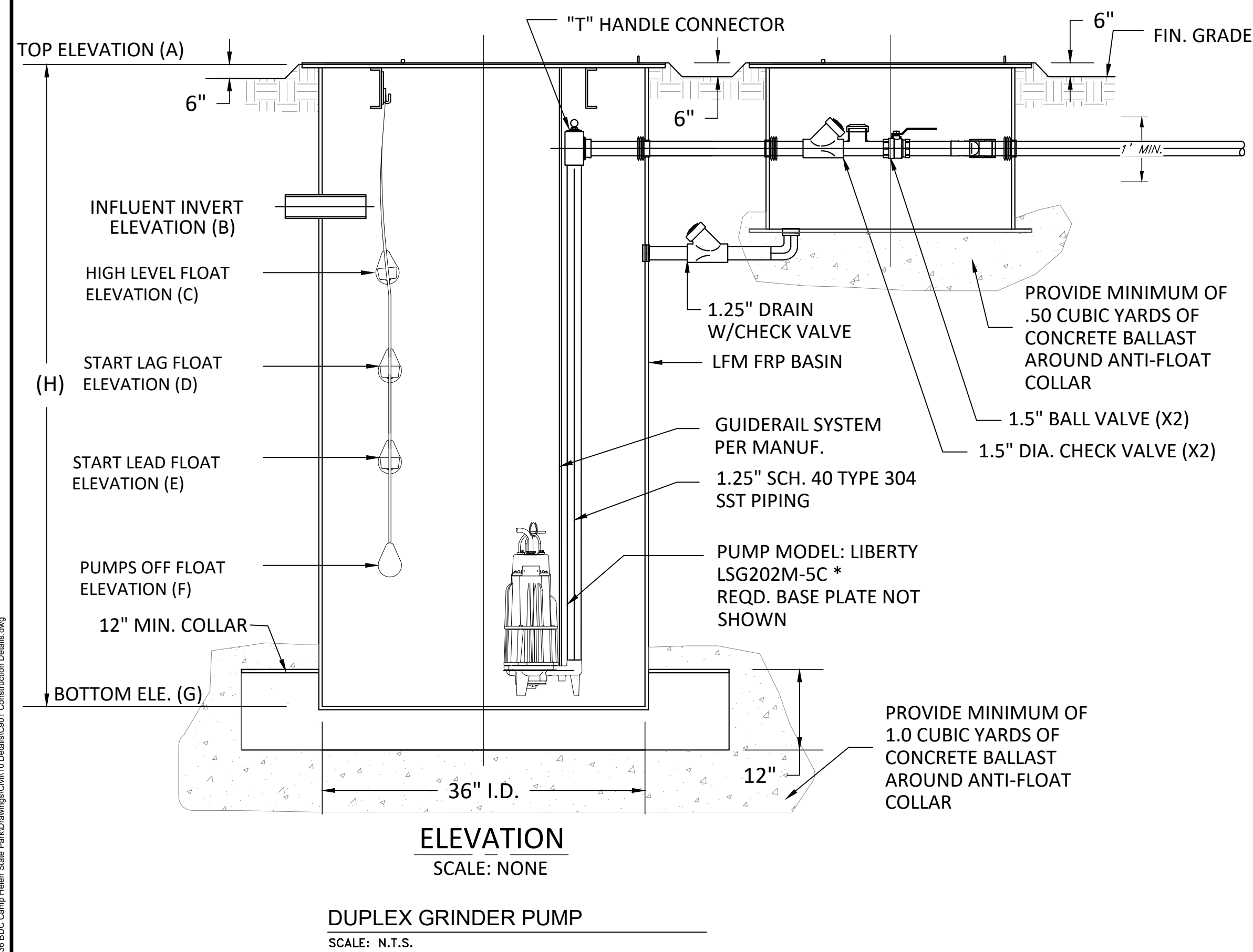
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	SHEET TITLE		CONSTRUCTION DETAILS			
C902	PROJECT TITLE		PARK IMPROVEMENT		JAMES H. PETERSON IV State of Florida P.E. # 80486	



LIFT STATION INFORMATION		
DESCRIPTION	REF.	STATION #1
TOP	'A'	19.25'
INFLUENT INVERT	'B'	17.5'
ALARM	'C'	16.5'
TWO PUMPS ON	'D'	17.33'
ONE PUMP ON	'E'	16.83'
PUMPS OFF	'F'	16.33'
BOTTOM	'G'	14.25'
WET WELL DEPTH	'H'	5'
WET WELL DIAMETER	'I'	36"
# OF PUMPS		2
GPM		20
TDH (FT)		85
VOLTAGE / PHASE		230 V / 1 PH
HP		2
PUMP MODEL	Liberty D3648LSG202-C *	

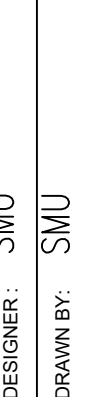
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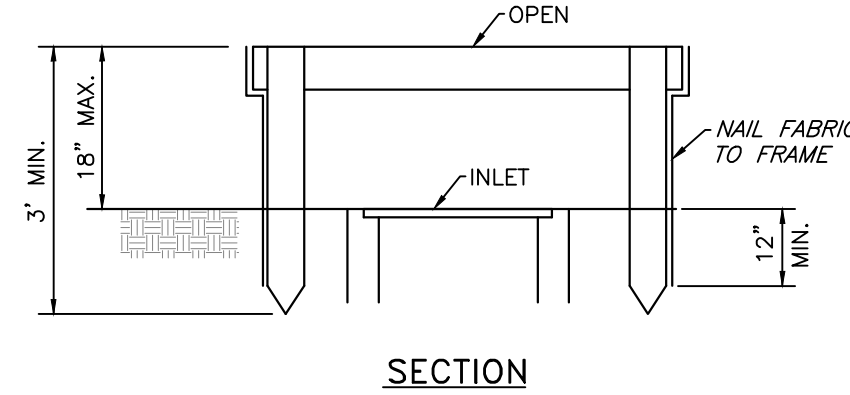
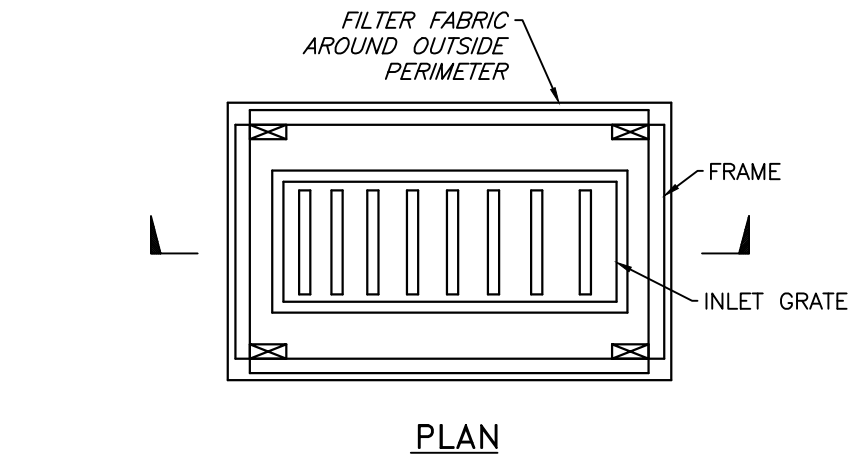
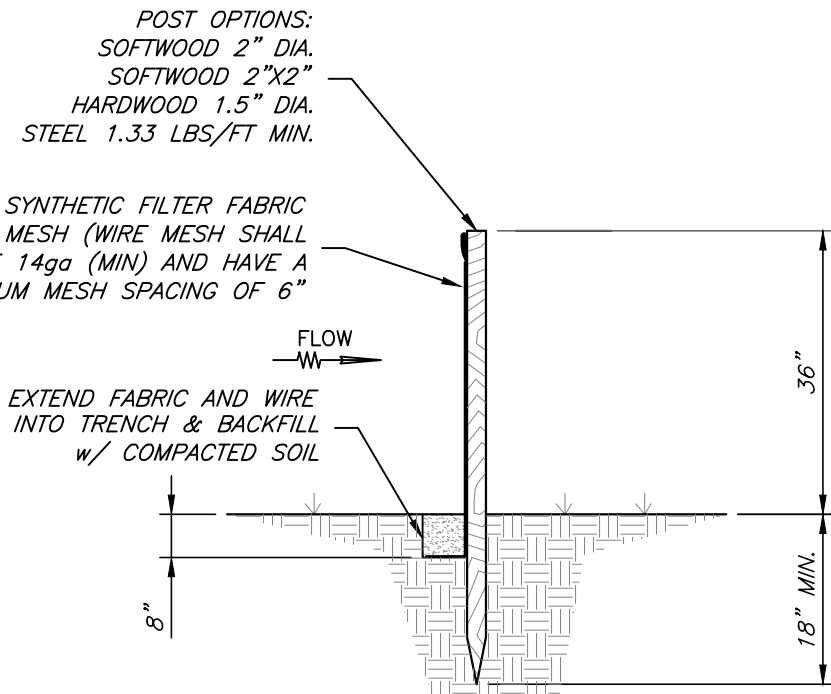
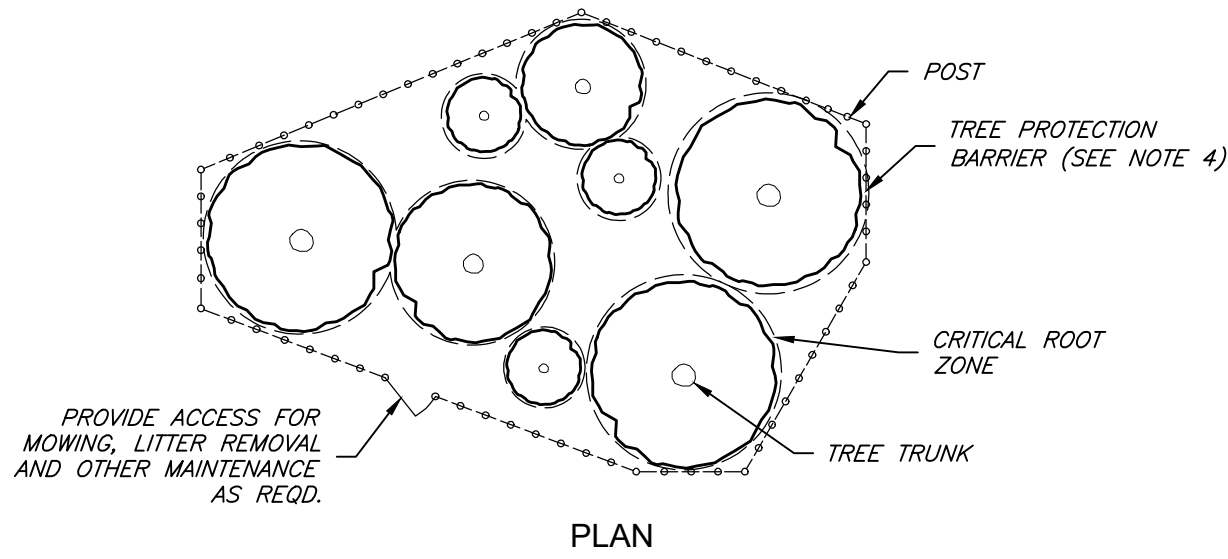
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CONSTRUCTION DETAILS

NOT FOR CONSTRUCTION

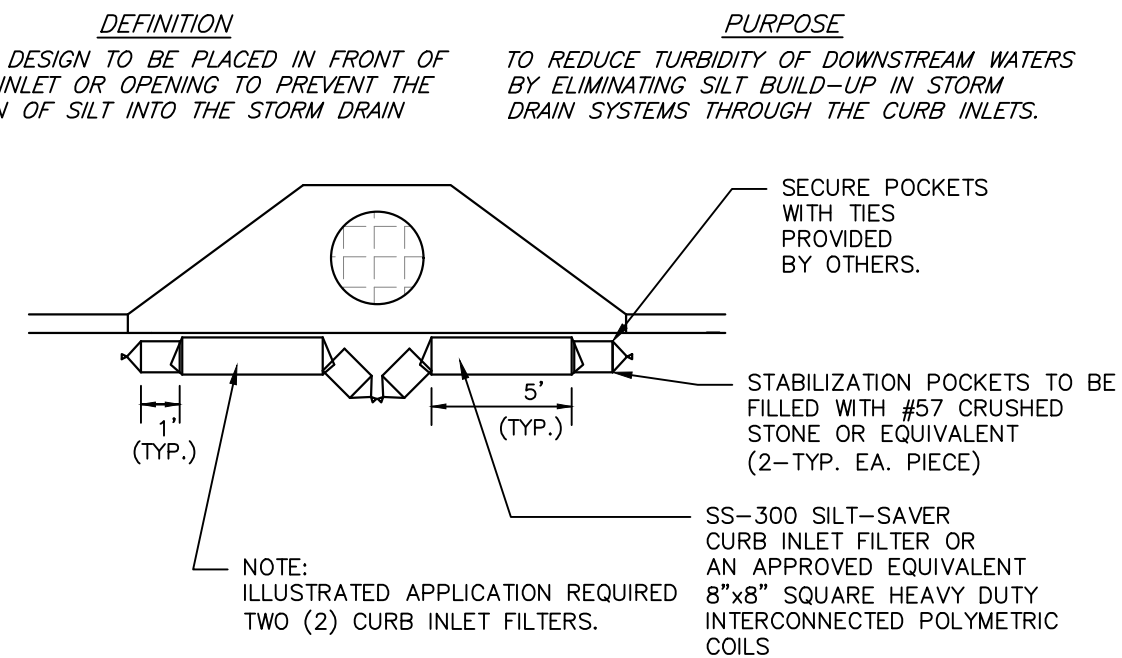
CAMP HELEN STATE PARK				PROFESSIONAL REGISTRATION JAMES H. PETERSON # 80485 State of Florida P.E.#	
CONSTRUCTION DETAILS		DESIGNER: SMU DRAWN BY: SMU REVIEWED BY: JHP		ISSUE DATE: 11/11/2024 100% PLANS COMP. FILE NO: 21-5436 STATE PROJECT NO: 61307/C-N3803	
PROJECT TITLE		Department of Environmental Protection Division of Recreation and Parks Bureau of Design and Construction		SYMBOL DATE REVISION REVISION	
PARK IMPROVEMENT		George & Associates Consulting Engineers, Inc. <small>ONE - FORTYFOURTH AVENUE, SUITE 200, PALM BEACH, FL 33410 1957 COMMONWEALTH LANE, SUITE 200, TALLAHASSEE, FL 32303 PHONE: 850/5210344 • FAX: 850/5210345</small>		3900 Commonwealth Boulevard, Tallahassee, FL 32399 (850) 245-2157	

1. CRITICAL ROOT ZONE: EXTENDS IN ALL DIRECTIONS FROM TREE TRUNK TO A DISTANCE EQUAL TO ONE FOOT PER INCH OF TRUNK DIAMETER AT BREAST HEIGHT.
2. STAGING, STORAGE, DUMPING, WASHING AND OPERATION OF EQUIPMENT IS NOT PERMITTED WITHIN THE LIMITS OF THE TREE PROTECTION BARRIER, INCLUDING DURING BARRIER INSTALLATION.
3. INSTALL ALL TREE PROTECTION PRIOR TO COMMENCEMENT OF CONSTRUCTION AND REMOVE WHEN POTENTIALLY DAMAGING CONSTRUCTION ACTIVITIES ARE FINISHED IN THE VICINITY OF THE PROTECTED TREES.
4. FOR CLOSELY SPACED GROUPS OF TREES, PLACE THE TREE PROTECTION BARRIER AROUND THE ENTIRE GROUP.
5. INSPECT TRUNK PROTECTION AND TREE QUARTERLY TO PREVENT GIRDLING. ADJUST BANDS TO ALLOW TREE GROWTH AS NEEDED.
6. SEE PLANS FOR ANY ADDITIONAL REQUIREMENTS OR MODIFICATIONS WITHIN THE TREE PROTECTION AREA.
7. PLACE WEATHER RESISTANT SIGN EVERY 50' ALONG THE BARRIER, WITH 6" MINIMUM TEXT HEIGHT AND PROVIDE TEXT IN ENGLISH AND SPANISH. SIGN SHOULD READ "KEEP OUT TREE PROTECTION AREA".
8. ALTERNATE TREE PROTECTION SYSTEMS APPROVED BY THE ENGINEER MAY BE USED IN LIEU OF THE TREE PROTECTION BARRIER DETAILED ON THIS PAGE AS LONG AS THE CRITICAL ROOT ZONE IS PROTECTED.
9. THE CRITICAL ROOT ZONE MAY BE REDUCED, IN INSTANCES WHERE THE PLANS CALL FOR UNDERGROUND UTILITY INSTALLATION AND/OR GRADING.
10. WHILE TRENCHING NEAR OR WITHIN THE CRITICAL ROOT ZONE FOLLOW ROOT PRUNING GUIDELINES.



INLET PROTECTION

N.T.S. EC-013



INSTALLATION

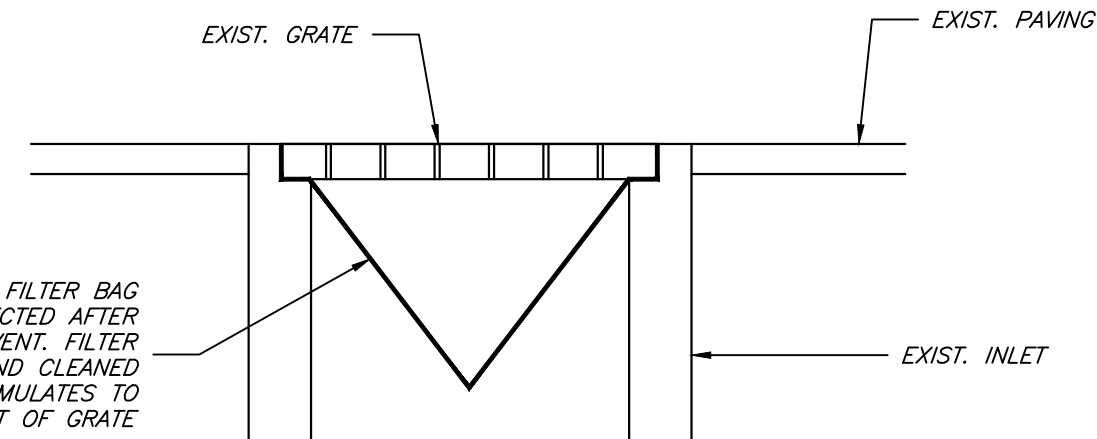
1. IDENTIFY OPENING DIMENSIONS TO DETERMINE HOW MANY FILTERS ARE REQUIRED.
2. COMPLETELY FILL THE ROCK CHAMBERS AT EACH END OF THE FILTER.
3. SECURE THE OPEN ENDS OF THE ROCK CHAMBERS WITH TIE WIRES. FOR LARGER OPENINGS, SIMPLY PLACE FILTERS END TO END.

MAINTENANCE

ALL TEMPORARY EROSION AND SEDIMENT CONTROL PRACTICES SHOULD BE INSPECTED DAILY. REMOVE SEDIMENT AND DISPOSE IN A PROPER MANNER. INSPECT FILTER FOR CUTS, ABRASIONS AND PROPER INSTALLATION, REPLACE OR REPOSITION AS NECESSARY. DISCONTINUE USE IF CURB INLET FILTRATION CREATES TRAFFIC HAZARD.

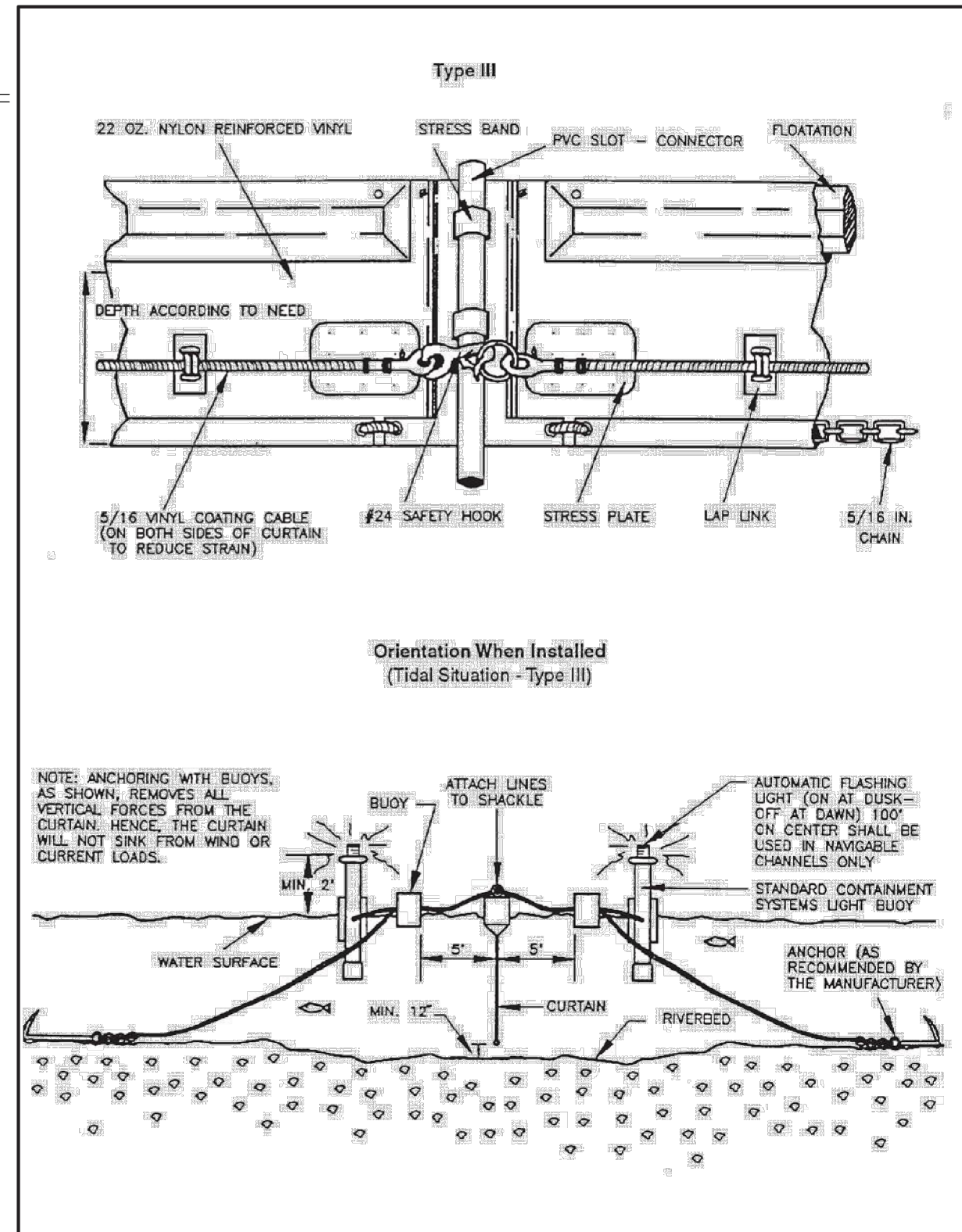
CURB INLET PROTECTION

N.T.S.



INLET PROTECTION

N.T.S.




NOTE: EROSION AND SEDIMENTATION CONTROL MEASURES, INCLUDING FLOATING TURBIDITY BARRIER, SPECIFICATIONS, REQUIREMENTS, AND INSTALLATION SHALL BE PER THE FDEP FLORIDA STORMWATER EROSION AND SEDIMENTATION CONTROL INSPECTORS MANUAL, LATEST EDITION.

TYPE III FLOATING TURBIDITY BARRIER

N.T.S.

EROSION CONTROL DETAILS

DR0010 November 5, 2024 P:\Projects\21-54-38 BDC Camp Helen State Park\Drawings\Civil\10 Details\C901 Construction Details.dwg

SHEET NO.	CAMP HELEN STATE PARK		PROFESSIONAL REGISTRATION	<p>George & Associates Consulting Engineers, Inc.</p> <p><small>CORP. - PROFESSIONAL ENGINEERS - SURVEYORS - LAND USE</small></p> <p>1967 Commonwealth Lane, Suite 200, Tallahassee, FL 32303 PHONE 850/5210344 - FAX 850/5210345</p>	<p>DESIGNER: SMU</p> <p>DRAWN BY: SMU</p> <p>REVIEWED BY: JHP</p>	<p>ISSUE DATE: 11/11/2024</p> <p>COMP. FILE NO.: 21-5436</p> <p>STATE PROJECT NO.: 61307C-N3803</p>	<p>SYMBOL</p> <p>SYMBOL</p>	<p>REVISION</p> <p>REVISION</p>	<p>DATE</p> <p>DATE</p>
	<p>SHEET TITLE</p> <p>EROSION CONTROL DETAILS</p>		<p>PROJECT TITLE</p> <p>PARK IMPROVEMENT</p>		<p>DATE</p> <p>DATE</p>				

NOT FOR CONSTRUCTION

C904

**** OFFICIAL RECORDS ****
BOOK: 1640 PAGE: 1928

FILE# 96-027339
BAY COUNTY, FLORIDA

DEED DOC STAMPS 0.70
06/18/96 *JA* Deputy Clk

-----RESERVED FOR USE BY CLERK OF COURT-----
Property Appraiser's Parcel Identification Number: 35205.000.000

CORRECTIVE WARRANTY DEED

THIS INDENTURE, made this 17th day of JUNE , A.D. 1996, between DANA BEACH RESORTS, INC., a Florida corporation, whose address is 420 East Pine Avenue, Crestview, Florida 32536 ("Grantor"), and the BOARD OF TRUSTEES OF THE INTERNAL IMPROVEMENT TRUST FUND OF THE STATE OF FLORIDA, whose post office address is c/o Florida Department of Environmental Protection, Division of State Lands, 3900 Commonwealth Boulevard, Mail Station, 115, Tallahassee, FL 32399-3000 ("Grantee"),

WITNESSETH: That the said Grantor, for and in consideration of the sum of Ten Dollars and other good and valuable considerations, to said Grantor in hand paid by said Grantee, the receipt whereof is hereby acknowledged, has granted, bargained and sold to the said Grantee, and Grantee's successors and assigns forever, the following described land situate, lying and being in Bay County, Florida, to wit:

Government Lots 2, 7, 8, 10 and 11, lying in and being a part of Section 31, Township 2 South, Range 17 West, Bay County, Florida, LESS AND EXCEPT right of way for U.S. Highway 98 as described in Official Records Book 696, page 869, Official Records Book 1349, page 1603, Deed Book 101, Page 119, and Deed Book 74, Page 25, all being recorded in the Public Records of Bay County, Florida.

THIS CORRECTIVE WARRANTY DEED IS GIVEN TO CORRECT A SCRIVENER'S ERROR IN THE LEGAL DESCRIPTION OF THAT CERTAIN WARRANTY DEED RECORDED AT BOOK 1639, PAGE 311, OFFICIAL RECORDS OF BAY COUNTY, FLORIDA, IN WHICH A REFERENCE WAS MADE TO "DEED BOOK 75" AND WHEREAS THE CORRECT REFERENCE IS "DEED BOOK 74".

This conveyance is subject to easements, restrictions, limitations and conditions of record if any now exist,

but any such interests that may have been terminated are not hereby reimposed.

AND the said Grantor does hereby fully warrant the title to said land, and will defend the same against the lawful claims of all persons whomsoever.

IN WITNESS WHEREOF, the Grantor has hereunto set Grantor's hand and seal, the day and year first above written.

Signed, sealed and delivered
in the presence of:

DANA BEACH RESORTS, INC. a
Florida corporation

Loe Bide
(SIGNATURE OF FIRST WITNESS)

By: *George Dana Doodle Harris*
George Dana Doodle Harris
Its President

Lane Bide
(PRINTED, TYPED OR STAMPED
NAME OF FIRST WITNESS)

J. Robert Hughes
(SIGNATURE OF SECOND WITNESS)

J. Robert Hughes
(PRINTED, TYPED OR STAMPED
NAME OF SECOND WITNESS)

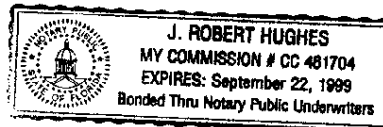
STATE OF FLORIDA
COUNTY OF RAY

The foregoing instrument was acknowledged before me this 17th
day of JUNE, 1996, by GEORGE DANA DOODLE HARRIS, as President of
DANA BEACH RESORTS, INC., a Florida corporation, on behalf of the
corporation, who: (notary **must** check applicable box)
☒ is personally known to me.
☐ produced a current Florida driver's license as identification.
☐ produced _____ as identification.

(SEAL)

J. Robert Hughes
(Print Name)
Notary Public
Serial # _____
My Commission Expires: _____

This Instrument Prepared By and
Please Return To:
J. Robert Hughes
Barron, Redding, Hughes, Fite,
Bassett & Fensom, P.A.
Post Office Box 2467
Panama City, Florida 32402



Part 4: Signatures and Authorization to Access Property

Instructions: For multiple applicants please provide a separate Part 4 for each applicant. For corporations, the application must be signed by a person authorized to bind the corporation. A person who has sufficient real property interest (see Section 4.2.3(d) of Applicant's Handbook Volume I) is required in (B) to authorize access to the property, except when the applicant has the power of eminent domain.

A. By signing this application form, I am applying for the permit and any proprietary authorizations identified above, according to the supporting data and other incidental information filed with this application. I am familiar with the information contained in this application and represent that such information is true, complete and accurate. I understand this is an application and not a permit, and that work prior to approval is a violation. I understand that this application and any permit issued or proprietary authorization issued pursuant thereto does not relieve me of any obligation for obtaining any other required federal, state, water management district, or local permit prior to commencement of construction. I agree to operate and maintain the permitted system unless the permitting agency authorizes transfer of the permit to a different responsible operation and maintenance entity. I understand that knowingly making any false statement or representation in this application is a violation of Section 373.430, F.S. and 18 U.S.C. Section 1001.

David Matson

Typed/Printed Name of Applicant or
Applicant's Authorized Agent

Signature of Applicant or Applicant's
Authorized Agent

Date

Assistant Bureau Chief, FDEP Bureau of Design and Construction
(Corporate Title if applicable)

B. Certification of Sufficient Real Property Interest And Authorization For Staff To Access The Property:

I certify that:

☒ **I possess sufficient real property interest in or control, as defined in Section 4.2.3 (d) of Applicant's Handbook Volume I**, over the land upon which the activities described in this application are proposed and I have legal authority to grant permission to access those lands. I hereby grant permission, evidenced by my signature below, for staff of the Agency to access, inspect, and sample the lands and waters of the property as necessary for the review of the proposed works and other activities specified in this application, upon advance notice. I authorize these agents or personnel to enter the property as many times as may be necessary to make such review, inspection, and/ or sampling. Further, if a permit is granted, upon advance notice, I agree to provide entry to the project site for such agents or personnel with proper identification to determine compliance with permit conditions and permitted plans and specifications.

OR

☐ I represent an entity having **the power of eminent domain and condemnation authority**, and I/we shall make appropriate arrangements to enable staff of the Agency to legally access, inspect, and sample the property as described above.

David Matson

Typed/Printed Name

Signature

Date

Assistant Bureau Chief, FDEP Bureau of Design and Construction
(Corporate Title if applicable)

C. Designation of Authorized Agent (If Applicable):

I hereby designate and authorize Signe Ulsamer (George & Associates Consulting Engineers) to act on my behalf, or on behalf of my corporation, as the agent in the processing of this application for the permit and/or proprietary authorization indicated above and to furnish, on request, supplemental information in support of the application. In addition, I authorize the above-listed agent to bind me, or my corporation, to perform any requirements which may be necessary to procure the permit or authorization indicated above. I understand that knowingly making any false statement or representation in this application is a violation of Section 373.430, F.S., and 18 U.S.C. Section 1001.

David Matson
Typed/Printed Name of Applicant

Signature of Applicant

Date

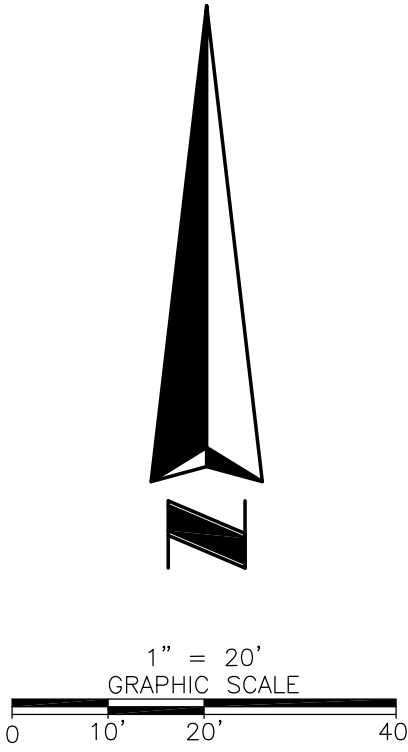
Assistant Bureau Chief, FDEP Bureau of Design and Construction
(Corporate Title if applicable)

CAMP HELEN

MATCHLINE SEE SHEET 1

MATCHLINE SEE SHEET 3

MATCHLINE SEE SHEET 3



PANAMA CITY BEACH
PARKWAY~SR30(US98)
RIGHT OF WAY VARIES
UNPAVED ROADWAY 50+00 TO 51+50

ZONE AE
(EL 8)

ZONE X

ZONE AE
(EL 8)

LEGEND & ABBREVIATIONS:

- | | |
|--------------------------------|---|
| ▽ = BACKFLOW PREVENTER | -FOC- = BURIED FIBER OPTIC LINE |
| h = BENCH | -BTE- = BURIED TELEPHONE LINE |
| ⊙ = BUSH | -GM- = GAS MAIN |
| ⊞ = TELEPHONE PEDESTAL | -OHL- = OVERHEAD UTILITY LINE |
| ⊕ = DRAINAGE MANHOLE | -WL- = WATER LINE |
| ⊞ = ELECTRIC SERVICE METER | -RCW- = RECLAIM WATER LINE |
| ⊞ = FIRE HYDRANT | ~ = HEDGE LINE |
| ∨ = GUY ANCHOR | ~ = TREE LINE |
| ⊙ = WATER SPIGOT | — = GUARDRAIL |
| • = IRON ROD | CPP = CORRUGATED PLASTIC PIPE |
| ◇ = UTILITY POLE | PVC = POLYVINYL CHLORIDE PIPE |
| • = POST/BOLLARD | RCPE = REINFORCED CONCRETE PIPE ELLIPTICAL |
| ⊞ = PUMP | TRAV.PT. = TRAVERSE POINT |
| ⊞ = NON-TRAFFIC SIGN | SSMC = SOUTHEASTERN SURVEYING & MAPPING CORPORATION |
| ⊞ = SPRINKLER | SIZE SHOWN IS TRUNK DIAMETER IN INCHES MEASURED AT CHEST HEIGHT |
| ⊞ = TEST HOLE | ⊞ = PALM |
| ⊞ = TRAFFIC CONTROLLER CABINET | ⊞ = TREE |
| ⊞ = TRAFFIC SIGN | MA = MAGNOLIA |
| ⊞ = UTILITY MARKER | O = OAK |
| ⊞ = WATER METER | PI = PINE |
| ⊞ = WIRING PULL BOX | UK = UNKNOWN |
| ⊞ = WATER VALVE | |
| ⊞ = YARD DRAIN | |
| ⊞ = VALVE COVER | |

SHEET NUMBER 2 OF 3
NOT VALID THROUGH 3
1 THROUGH 3

SSMC
SUE • SURVEY • GIS

SOUTHEASTERN SURVEYING
AND MAPPING CORPORATION

Chipley, Florida 32428
(850) 638-0790
e-mail: info@southeasternsurveying.com
Certification Number: 132106

TOPOGRAPHIC SURVEY

Project: 28937 PANAMA CITY BEACH PARKWAY
PANAMA CITY BEACH, FLORIDA

Scale: 1" = 20'
Drawn By: A. ECKLES
Field Date: 08/15/2023

SEE SHEET 1 FOR NOTES,
LEGEND AND DESCRIPTION.

DRAWING NUMBER

53475002

SHEET

NUMBER

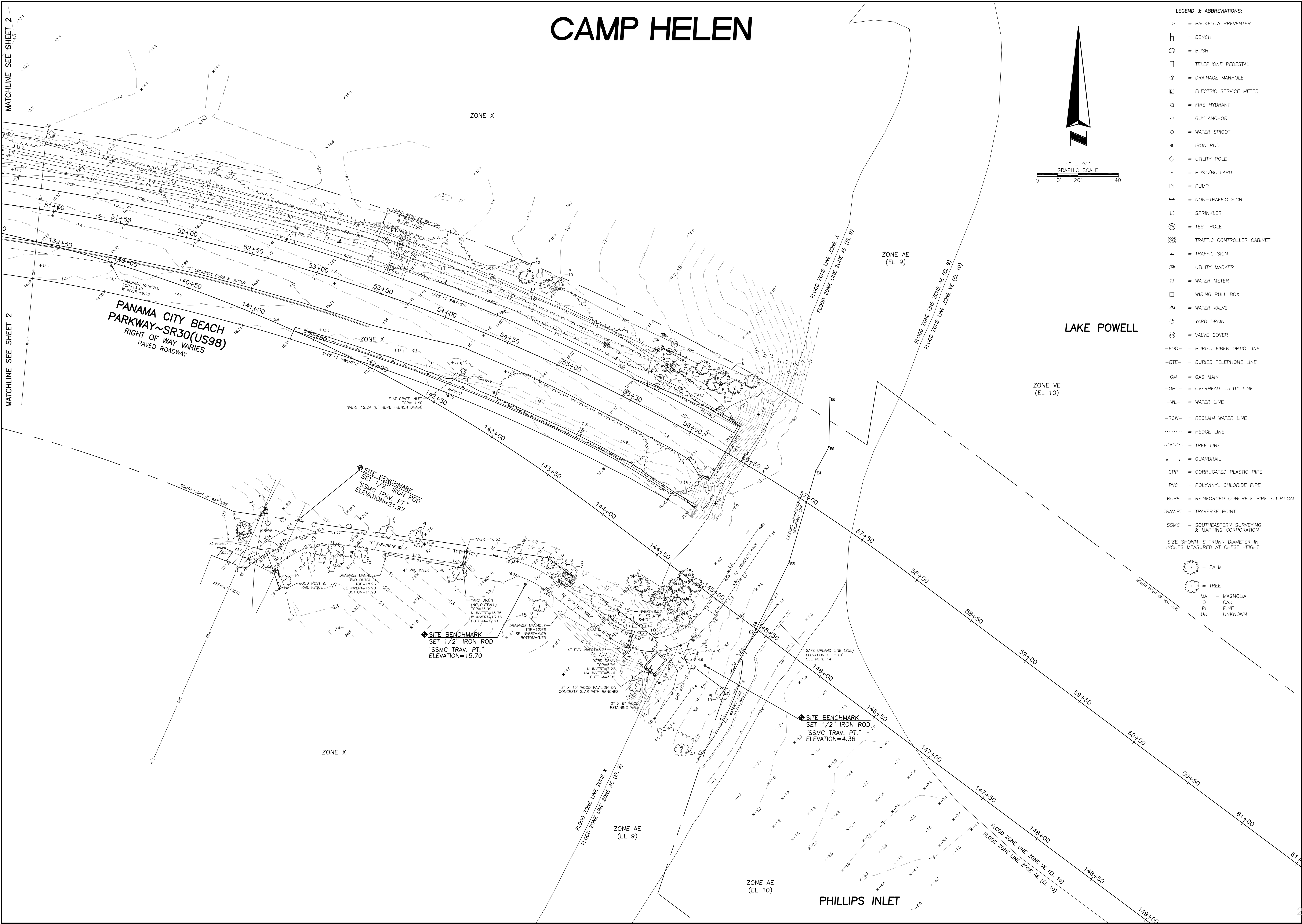
2 OF 3

2024-08-30 00:036

Lisa Ward

1/16/2025

CAMP HELEN



- LEGEND & ABBREVIATIONS:
- ▽ = BACKFLOW PREVENTER
 - h = BENCH
 - ⊙ = BUSH
 - ⊕ = TELEPHONE PEDESTAL
 - ⊕ = DRAINAGE MANHOLE
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SHEET NUMBER 3 OF 3
NOT VALID THROUGH SHEETS 1 THROUGH 3

SSMC
SUE • SURVEY • GIS

SOUTHEASTERN SURVEYING
AND MAPPING CORPORATION
Chipley, Florida 32428
(850) 638-0790
e-mail: info@southeasternsurveying.com
Certification Number 132106

BY	REVISION	REVISION DATE
AE	ADDED ADDITIONAL TOPO	10/28/2023

TOPOGRAPHIC SURVEY

Project 28937 PANAMA CITY BEACH PARKWAY
PANAMA CITY BEACH, FLORIDA

Field Date: 08/15/2023
Drawn By: A. ECKLES
Scale: 1" = 20'

SEE SHEET 1 FOR NOTES,
LEGEND AND DESCRIPTION.

DRAWING NUMBER
53475002
SHEET
NUMBER
3
OF
3



**SOUTHERN
EARTH SCIENCES**
Geotechnical | Environmental | Materials Testing

PANAMA CITY OFFICE

7500 McElvey Road, Ste. A
Panama City Beach, FL 32408

Tel: (850) 769-4773
Fax: (850) 872-9967
www.soeearth.com

George & Associates Consulting Engineers, Inc.
1967 Commonwealth Lane, Ste 200
Tallahassee, FL 32303
Attn: Mr. Brian Miller, PE

September 12, 2023
File No.: P23-0329

Subject: Preliminary Geotechnical Services for the Camp Helen State Park Improvements Project in Bay County, Florida

Dear Mr. Miller:

Southern Earth Sciences, Inc., has completed the geotechnical services for the Improvements Project at Camp Helen State Park in Bay County, Florida. Our services were performed in general accordance with proposal number XP23-4.11.23-1, dated April 11, 2023. This report presents the results of our preliminary field and laboratory testing and includes preliminary recommendations with regard to the design and construction of the foundations for the new bathroom, beach access, and kayak/canoe launch as well as the access road, parking, and turn lanes.

Our testing for this project will be completed in two phases. The first of which we have performed in accessible areas, since no clearing can be performed at this time. Once the project is closer to construction, clearing will be performed. At this time, we will remobilize to perform the additional testing. This report should not be used for final foundation design and should be considered preliminary foundation recommendations.

FIELD INVESTIGATIVE PROCEDURES:

Prior to performing our field testing, we traveled to the project site and met with the Park Staff to layout and observe the proposed access and boring locations. We then contacted Sunshine State One Call of Florida to locate underground utilities within the area. On July 20 and 21, 2023, personnel with our firm traveled to the project site and completed the field testing for the above referenced project. For our geotechnical investigation, a total of two (2) cone penetrometer soundings were performed. One was performed at the canoe/kayak launch on the south side of the park and the second was performed along the beach access area at the north side of the park. The cone penetrometer is track mounted and rather than sampling and testing at five foot intervals, as normally done with a standard penetration borings, the cone penetrometer is an electronic device that provides continuous evaluation of the soils bearing capacity through point and frictional resistances. The cone penetrometer is hydraulically pushed into the soil with point and frictional resistances obtained continuously on a computer

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

printout. This testing equipment provides an accurate definition of the soil strength characteristics and the changes in stratification. The cone soundings were performed in general accordance with ASTM D5778.

To verify soil conditions encountered within the depth of our cone soundings, direct push borings were performed to depths ranging from approximately 5 to 10 feet below the existing ground surface. The direct push borings were performed with our Geoprobe 6622 and the DT22 soil sampling system. This is a closed-piston sampler, with an inner piston rod and outer drive casing, and is driven to the top of the sampling interval. The inner piston rod is removed and the sampler is driven to collect a soil sample. The soil samples are collected in a clear 5-foot PVC liner and are delivered back to our laboratory for soil classifications and laboratory testing.

Additionally, seven hand auger borings were performed along the proposed turn lane and access roadway, and seven hand auger borings were performed at accessible areas of the proposed beach access/restroom area. Most hand auger borings were performed to a depth of five feet, however, hand auger borings at the bathroom areas were performed to a depth of ten feet below existing grade. Test locations HA-7, 8, 9, and 11 were not accessible. Hand dial penetrometer readings were obtained at one-foot intervals throughout the depth of our hand auger borings. The hand dial penetrometer consists of a 5/8-inch diameter cone point attached to a 1/2-inch diameter rod. A proving ring with an Ames dial indicator is attached to the top of the rod. As the penetrometer is pushed into the soil, the proving ring deflects indicating resistance to penetration of the cone point and relative compactness of the soil; therefore, the higher the penetrometer reading, the denser the soil.

Test locations were established in the field by using a hand held GPS and measuring from existing landmarks, therefore, our test locations should be considered approximate. See the attached Figure for our approximate test locations.

LABORATORY TESTING PROCEDURES:

Laboratory investigative work consisted of physical examination of samples obtained during the soil test boring operation. Soil samples were visually classified in the laboratory in accordance with the Unified Soil Classification System. Evaluation of these samples, in conjunction with penetration resistances, have been used to estimate soil characteristics.

Natural Moisture: Five (5) samples were selected for determination of their natural moisture content. In the laboratory, each sample was weighed, dried, and its moisture content was calculated in accordance with ASTM D-2216

Percent Passing 200 Mesh Sieve: Five (5) samples were selected to determine their percent of materials, by dry weight, finer than the U.S. Number 200 Mesh Sieve. This test was performed in accordance with ASTM D-1140.

The laboratory test results are shown on the boring log at the depth of the tested sample. Abbreviations for laboratory data are shown below.

NM = Natural Moisture Content (%)

-200 = Percent finer than the U.S. No. 200 mesh sieve

CONE SOUNDINGS:

CPT Log graphically indicates the cone tip resistance, friction ratio, equivalent N-value and interpreted soil type at each sounding location. Soil classifications and data were interpreted from methods recommended by Robertson and Campanella and/or the Swedish Geotechnical Institute Information Publication No. 15E. Correlations between Cone Resistance values and Standard Penetration Testing “N” values were performed according to the methods developed by Robertson, Campanella and Wightman. The soil types and stratigraphy shown on the CPT Log sheets are based upon material parameters measured and evaluated as the cone is advanced. The CPT Log sheets were developed for general information only.

SITE AND SOIL CONDITIONS:

The Camp Helen Improvements include a new canoe/kayak launch on the south side of the Park, a new beach access and restroom on the north side, as well as new access roadway, parking, turn lanes, and stormwater management on the north side of the Park. The majority of the north side is currently wooded with trees and dense underbrush. We did not have access to the majority of the test locations on the north side with our equipment, and some hand auger borings were not accessible. Clearing cannot be performed at this time, therefore, additional testing, phase 2, will be performed prior to construction, once the site is accessible. Based upon the provided plan, elevations vary across the site, however, typically slope towards the Lake. The beach access and parking are located at the highest point on the property, typically ranging from +17 to +22 Feet. The elevations of our test locations have been interpolated from the provided topographic information, therefore, elevations of our boring locations should be considered approximate.

Based upon the results of our testing, the soils encountered throughout our soundings/borings are predominantly sands. The sands vary in color and texture ranging from

slightly silty to slightly clayey and clean sands. Based upon the results of our cone soundings, the sands within the top one to two feet are typically loose and then become medium dense to an average depth of 22 feet below existing ground surface. For the remaining depths of our soundings, the sands are dense with thin loose zones. The soils encountered throughout our hand auger borings are predominantly loose to medium dense clean sands. However, at the hand auger borings for the proposed turn lanes, we encountered thin, slightly clayey sand layers, some with varying amounts of shell. We typically encountered 6 to 12-inches of organic laden soils (topsoil) within the results of our borings.

On the dates of our field testing (indicated above), the groundwater levels were measured at the depths indicated on the attached logs which ranged from approximately 2.5 to 4.5 feet below existing ground surface, however, at some of our test locations at higher elevations we did not encounter groundwater within the depths of our borings. Fluctuations in the water table depths will occur due to seasonal precipitation/evapotranspiration differences, neighboring drainage/wetland influences and tidal influences, therefore, prior to foundation construction we recommend that groundwater levels be verified.

PRELIMINARY STRUCTURAL INFORMATION:

The proposed bathroom and beach access located on the north side of the Park will be supported on conventional shallow foundations. At this time, no civil or structural information is available. We understand there will be some grading performed to level the footprint, and finished floor elevation will likely be within one to two feet of existing elevation. This will be a single-story CMU structure of approximately 1000 square feet. We have assumed wall loads of 2.5 kips per lineal foot and the bottoms of footings will be approximately two feet below finished floor elevation. As noted above, once clearing has been performed and the building footprint is accessible to our testing equipment, we will re-mobilize to perform additional cone soundings.

The proposed kayak/canoe launch located on the south side of the Park will be a wooden structure extending into Lake Powell. At this time, design pile capacity is unknown. We understand timber piles will be utilized.

The new access roadway will extend north from US Hwy 98 into the Park. We understand the roadway will be a typical two-lane paved roadway with a fairly low volume of traffic. Parking will be located north of the access roadway, near the proposed restroom. There will be two turn lanes, one for eastbound and one for westbound traffic for the north access road. Additionally, there will be a dry retention stormwater management pond located on the north side of the Park. At this time, the size and depth of the pond is unknown.

If any of this information above is incorrect, we should be contacted to provide additional preliminary recommendations. As noted above, this information should be used for preliminary design. Additional field testing, laboratory testing, and engineering evaluation will be necessary to provide foundation and pavement recommendations.

PRELIMINARY SHALLOW FOUNDATION RECOMMENDATIONS – Bathrooms & Beach Access

Our preliminary evaluation of foundation conditions has been based on structural information presented in this report and subsurface data obtained during our investigation. In evaluating soundings and borings, we have used correlations that were previously made between penetration resistances and foundation stabilities observed in soil conditions similar to those encountered at your site.

The soils encountered within our borings are mostly consistent across the footprint of the building, however, some locations were not accessible. Additional field testing will be required. Typically, we encountered loose sands within the top two to three feet of our test locations. We recommend these soils are compacted prior to foundation construction. Since there are no adjacent structures, vibratory compaction may be performed. Dependent upon rainfall conditions at the time of construction, the clean dry sands will likely require the addition of water to achieve proper compaction.

Based upon the results of our field and laboratory testing, it is our opinion that with the compaction of the existing soils, the proposed structure may be supported on a conventionally designed shallow foundation system. We recommend footings be proportionally designed for an allowable soil contact pressure of 1500 psf, or less. Based upon the assumed structural loading indicated above, we have calculated settlements of approximately one inch, or less. We recommend column footings have a minimum width of 24 inches and continuous footings have a minimum width of 18 inches. We recommend the footings have a minimum embedment depth of 18 inches from the bottom of the footings to the outside finished grade. We also recommend the footings have top and bottom reinforcement. Prior to foundation construction we recommend the following site and soil preparations.

1. Clear and grub the surface soils within the building perimeter and extend at least five (5) feet beyond the building perimeter to remove all topsoil, organics laden sands, and other deleterious materials. Based upon the results of our borings, these soils typically were encountered within the top six to twelve inches of our borings.
2. Once the topsoil has been grubbed, prior to the addition of fill soils, compact the existing soils until a density of 95% of the Modified Proctor (ASTM D-1557) maximum dry density

is achieved to a depth of two (2) feet below compacted grade. Moisture conditioning of the soils including dewatering may be required to achieve optimum moisture conditions for compaction.

3. Fill soils shall be sands to slightly silty sands containing no more than twelve (12) percent, by dry weight, finer than U.S. No. 200 mesh sieve. Fill shall be placed in thin level lifts not to exceed twelve (12) inches, loose, and compacted to a density of 95% of the Modified Proctor maximum dry density throughout its full depth.
4. Once footings are excavated, compact the soils at the bottom of footings to achieve a minimum density of 95% of the Modified Proctor maximum dry density to a depth of twelve (12) inches.
5. Laboratory moisture-density relationships (Proctors) and in-place density tests should be performed to verify compliance with the foregoing compaction recommendations. We recommend one density test per column footing, one density test per 50 lineal feet of wall footing, and one density test per 2000 square feet of existing soils and for each foot of fill soils.

As indicated above, the above preliminary shallow foundation recommendations should not be used for final foundation design. Additional cone soundings, field testing, and engineering evaluation will be necessary to provide final foundation recommendations.

DEEP (PILE) RECOMMENDATIONS – Kayak Launch

Our evaluation of foundation conditions has been based on structural information presented in this report and subsurface data obtained during our investigation. In evaluating soundings, we have used correlations that were previously made between penetration resistances and foundation stabilities observed in soil conditions similar to those encountered at your site.

We have calculated compressive and tensile capacities for 8-inch and 10-inch tip timber piles. The embedment depths are below the existing ground surface, therefore, any cantilever above existing grade must be added to determine the total pile length. Allowable compressive capacities include a factor of safety of two (2) in compression, and three (3) in tension. Skin friction has also been reduced by ten (10) percent for pre-jetting or pre-drilling. The allowable capacities are based upon a soil/pile interaction and do not consider the structural aspects of the pile. If requested, lateral analysis can be performed. The tabulated pile capacities should be provided to the Structural Engineer to select the pile length that is consistent with the design

loads and based upon economic considerations for each pile length. Allowable stresses in the piles shall conform to the Florida Building Code.

Table I below provides the estimated allowable compressive and tensile capacities for 8-inch and 10-inch tip timber piles. At this time, water depth (depth to mudline) is unknown. We have assumed the mudline is approximately 5 feet below the surface of the water. The elevation of test location C-1 is unknown, however, based upon the provided topographic information, appears to be approximately +3 Ft. For the purpose of this preliminary design, we have not included the top eight (8) feet of the existing soil skin friction in our pile capacity calculations.

TABLE I: Kayak Launch Dock (Test Locations C-1)

Embedment Depth / <u>Approximate</u> Elevation:	8-inch Tip Timber Piles		10-inch Tip Timber Piles	
	Compressive (tons)	Tensile (tons)	Compressive (tons)	Tensile (tons)
15 ft. / (-12 Ft.)	3.0	1.0	4.5	1.0
20 ft. / (-17 Ft.)	4.5	1.5	6.5	1.5
25 ft. / (-22 Ft.)	5.5	2.0	7.5	2.5

The soil conditions in the Lake may be different than what was encountered in the upland soundings. The pile capacities and evaluation have been based upon the conditions found on land. We encountered similar soil conditions at the recently constructed dock to the south at Camp Helen.

Prior to the installation of production piling, it would be beneficial to perform a pile load test to verify the design capacity. A pile load test can also be performed in accordance with ASTM D-4945 using a Pile Dynamic Analyzer. Depending upon the results of the pile load test and/or CAPWAP analysis, adjustments in the pile lengths or capacities may be required. It is also recommended the installation of all production piling be monitored by Southern Earth Sciences, Inc., employed by the Owner, to verify production piles are installed in accordance with the pile load test program.

The evaluation of scour from hurricane force winds is beyond the scope of our services. It may be advisable to have a Coastal Engineer evaluate scour for this site. A lateral analysis can be performed on the piles once the design load, length of the piles and deflection criteria has been determined. The lateral load indicated for the piles is relatively low and should be acceptable with the foregoing pile lengths. However, confirmation would require a lateral analysis.

PAVEMENT RECOMMENDATIONS:

Based upon the existing conditions, we anticipate minor cutting and filling will be required to achieve final pavement grades. Pavement recommendations are based upon a 15-year life. It should be noted that pavement maintenance and rehabilitation, including an overlay, might be required within the life of the pavement. We have assumed automobiles and light trucks as the primary traffic for this pavement. If this assumption is incorrect, we should be notified to provide revisions to our pavement recommendations.

Fill soils, shall be sands to slightly silty sands (non-plastic) containing no more than 12%, by dry weight, finer than the U.S. No. 200 mesh sieve and shall be free of organics, organic laden sands, rubble, clay balls, and other deleterious materials. Fill soils shall be placed in thin level lifts and compacted to a density of 98% of the Modified Proctor (AASHTO T-180) maximum dry density throughout its full depth.

Subgrade Preparation: Clear and grub the surface soils within the pavement perimeter, extending at least three (3) feet beyond the curblines, to remove all topsoil, organic laden sands, and other deleterious materials. Based upon these materials were encountered within 6 to 12 inches. However, these soils may extend to greater depths than our borings indicate.

Prior to the addition of fill soils or once the soils have been excavated to the bottom of the base, compact the existing soils until a density of 98% of the Modified Proctor (AASHTO T-180) maximum dry density to a depth of twelve (12) inches. Fill soils described above should be placed to achieve final pavement grades. If there are no adjacent structures within 50 feet, a vibratory roller may be used. We also recommend that the top twelve (12) inches of subgrade soils be stabilized to achieve a Limerock Bearing Ratio of 40. Where shallow groundwater conditions are present, we do not recommend clay for stabilization.

Any existing utilities that are located within the pavement areas should be filled and compacted with suitable fill soils similar to those described above. The fill soils should be placed in lifts and compacted each lift to verify proper preparation of the soils.

Base: We recommend either a limerock or graded aggregate base with a minimum thickness of eight (8) inches in heavy traffic areas and six (6) inches in light traffic/parking areas. Crushed concrete may be used if it meets the FDOT specifications requirements for a graded aggregate base.

Wearing Surface: We recommend a SP-12.5 asphaltic concrete wearing surface having a

minimum thickness of two and a half (2.5) inches in heavy traffic areas and two (2.0) inches in light traffic/parking areas. Pavement should be placed and compacted in accordance with FDOT Standard Specifications.

All materials and methods of placement shall be in accordance with applicable sections of the Florida Department of Transportation's "Standard Specifications for Road and Bridge Construction", (Latest Edition).

FIELD TESTING FOR STORMWATER DESIGN:

While the borings performed for this project are representative of subsurface soil conditions at its respective locations/depths and for their respective vertical reaches, local variations of the subsurface materials and seasonal high groundwater levels are anticipated. Soil descriptions and seasonal high groundwater levels represent subsurface conditions at the designated locations.

It is our understanding there will be new stormwater management constructed to the north of the access roadway on the north side of the Park. At this time, the size and depth of the pond are in development. A double ring infiltrometer test was performed at test location SW-1 at a depth of one foot below existing ground surface.

At test location SW-1 seasonal high groundwater levels were estimated by characteristics such as natural vegetation, soil color, soil mottles, and depth to root zone. At our test locations, the seasonal high groundwater level is approximately 2.9 feet (± 0.5 feet) below the existing ground surface. See the individual boring logs attached. It may be advisable to have a Professional Surveyor obtain the elevations of the test locations. During periods of above average rainfall, groundwater levels may rise above the seasonal high depths indicated above.

Vertical Infiltration Rates:

To estimate the vertical infiltration rates a double-ring infiltrometer test was performed at test location SW-1 at a depth of approximately one foot below existing ground surface. The double ring infiltrometer test was performed in general accordance with ASTM D-3385 "Infiltration Rate of Soils in Field Using Double-Ring Infiltrometers". The soils were presaturated prior to performing the test. The double ring infiltration test does not include the effect of long-term saturation and groundwater mounding.

The results for the double-ring infiltrometer test is graphically illustrated as accumulated

intake (inches) versus time (min) and infiltration rate (in/hr) versus time (min) for the test period on the attached Graph. Based upon the results of our double-ring infiltrometer test, the unsaturated vertical infiltration rate at test location SW-1 is approximately 46 inches per hour. We should note the infiltration rate is not factored and should be used with an appropriate factor of safety.

The vertical infiltration rate stated above should not be considered the drawdown rate of the pond or swales. The drawdown rate is a complex 3-dimensional phenomenon dependent upon numerous factors including pond/system geometry, vertical and horizontal infiltration rates, groundwater mounding, etc. The prediction of the drawdown rate is made more difficult by varying soil/groundwater conditions. The Northwest Florida Water Management District recommends a correlation factor between unsaturated vertical infiltration rates and horizontal hydraulic conductivity of 1.5.

ADDITIONAL COMMENTS:

As previously indicated, this report should be considered preliminary and should not be used for final foundation design. Once a final layout is determined and the site has been made accessible, we should be notified so that our additional test locations may be located and performed properly. Additional field and laboratory testing will be required to provide additional foundation recommendations.

CONSTRUCTION TESTING SERVICES:

The effectiveness of the foundation will depend significantly on the proper preparation of the soils, as indicated previously. Therefore, we recommend the owner employ Southern Earth Sciences, Inc., as the testing laboratory to perform construction testing services. If we are not employed to provide construction testing services, Southern Earth Sciences, Inc., can not accept any responsibility for any conditions, which deviate from those described in this geotechnical report. Southern Earth Sciences, Inc., should be invited to the pre-construction conference to discuss the project with all interested parties so that the project may be completed expeditiously and to the intent of our geotechnical report. We would be pleased to review the plans and specifications as they relate to the soil preparation and provide a fee proposal for construction testing.

GENERAL COMMENTS:

Professional judgments on design criteria are presented in this letter. These are based partly on our evaluations of technical information provided, partly on our understanding of the characteristics of the project being planned, and partly on our general experience with subsurface conditions in the area. We do not guarantee performance of the project in any respect, only that our judgments meet the standard of care of our profession.

This information is exclusively for the use and benefit of the addressee(s) identified on the first page of this report and is not for the use or benefit of, nor may it be relied upon by any other person or entity. The contents of this letter may not be quoted in whole or in part or distributed to any person or entity other than the addressee(s) hereof without, in each case, the advance written consent of the undersigned.

This report has been prepared in order to aid in the evaluation of this property and to assist the architects and engineers in the foundation, pavement, and stormwater management design. It is intended for use with regard to the specific project discussed herein, and any substantial changes in the buildings, loads, locations, or assumed (or reported) grades shall be brought to our attention immediately so that we may determine how such changes may effect our conclusions and recommendations. We would appreciate the opportunity to review the plans and specifications for the foundation and floor construction to verify that our conclusions and recommendations are interpreted correctly. Our report does not address environmental issues which may be associated with the subject property. ***This investigation has been performed for preliminary site evaluation. Additional field testing and engineering evaluation should be performed for final foundation recommendations.***

While the soundings and borings performed for this project are representative of subsurface soil conditions at their respective locations and for their respective vertical reaches, local variations of the subsurface materials are anticipated and may be encountered. The boring logs and related information are based on the driller's logs and visual examination of selected samples in the laboratory. Delineation between soil types shown on the boring logs is approximate, and soil descriptions represent our interpretation of subsurface conditions at the designated boring location on the particular date drilled.


We appreciate the opportunity to assist you. If you have any questions or if we may be of further assistance, please call at your convenience.

Yours Very Truly,

SOUTHERN EARTH SCIENCES, INC.

Logan A. Fowler, P.E.
Eng. Reg. No. 82343
State of Florida

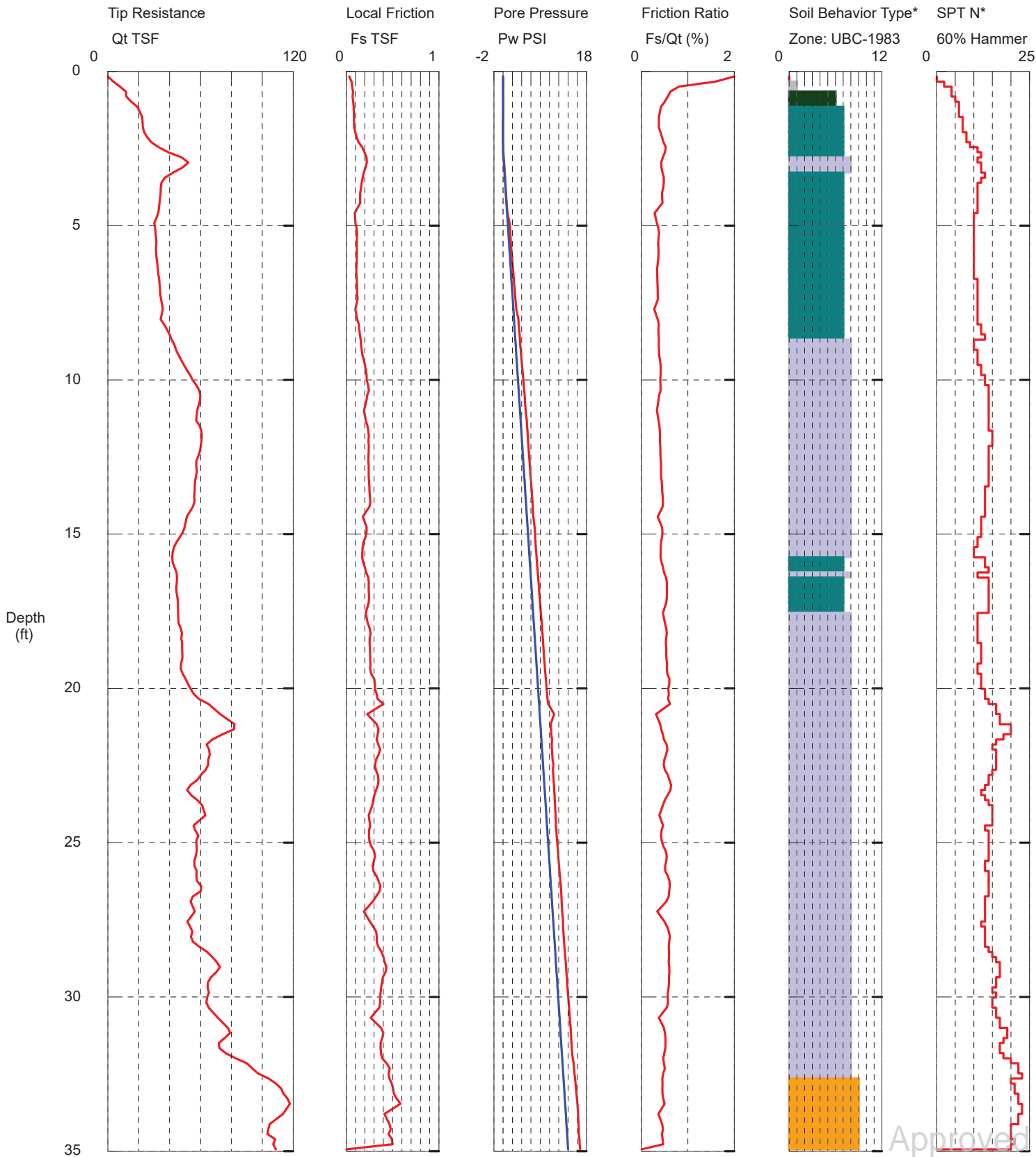


SESI FILE NO: P23-0329	 SOUTHERN EARTH SCIENCES	DRAWN BY:	LF	Approved FIGURE I 2024-D-391-00036 Lisa Ward APPROXIMATE TEST LOCATIONS 1/16/2025
Camp Helen State Park Improvements Project Bay County, FL		CHECKED BY:	LF	
		DATE:	9/8/23	
		SCALE:	1:200	

Southern Earth Sciences Inc.

Operator: Pat Conroy
Sounding: C-1
Cone Used: DDG1485
Groundwater: 2.5 feet

CPT Date/Time: 7/20/2023 10:10:17 AM
Location: Camp Helen State Park
Job Number: P23-0329
Elevation: +4 Feet (Approx.)



Maximum Depth = 35.10 feet

Depth Increment = 0.164 feet

- | | | | |
|--------------------------|-----------------------------|----------------------------|--------------------------------|
| 1 sensitive fine grained | 4 silty clay to clay | 7 silty sand to sandy silt | 10 gravelly sand to sand |
| 2 organic material | 5 clayey silt to silty clay | 8 sand to silty sand | 11 very stiff fine grained (*) |
| 3 clay | 6 sandy silt to clayey silt | 9 sand | 12 sand to clayey sand (*) |

Changenroy

N30 2748Q1W R5 Q88377

*Soil behavior type and SPT based on data from UBC-1983

Approved
2024-D-391-00036
Lisa Ward
7/26/2025

Page 1 of 1

METHOD: Direct Push
DRILLER: PC
ENGR / GEOL: LF
CE ELEVATION: +4 ft

LOG OF BORING P23-0329.GPJ SES PC FL.GDT 9/6/23

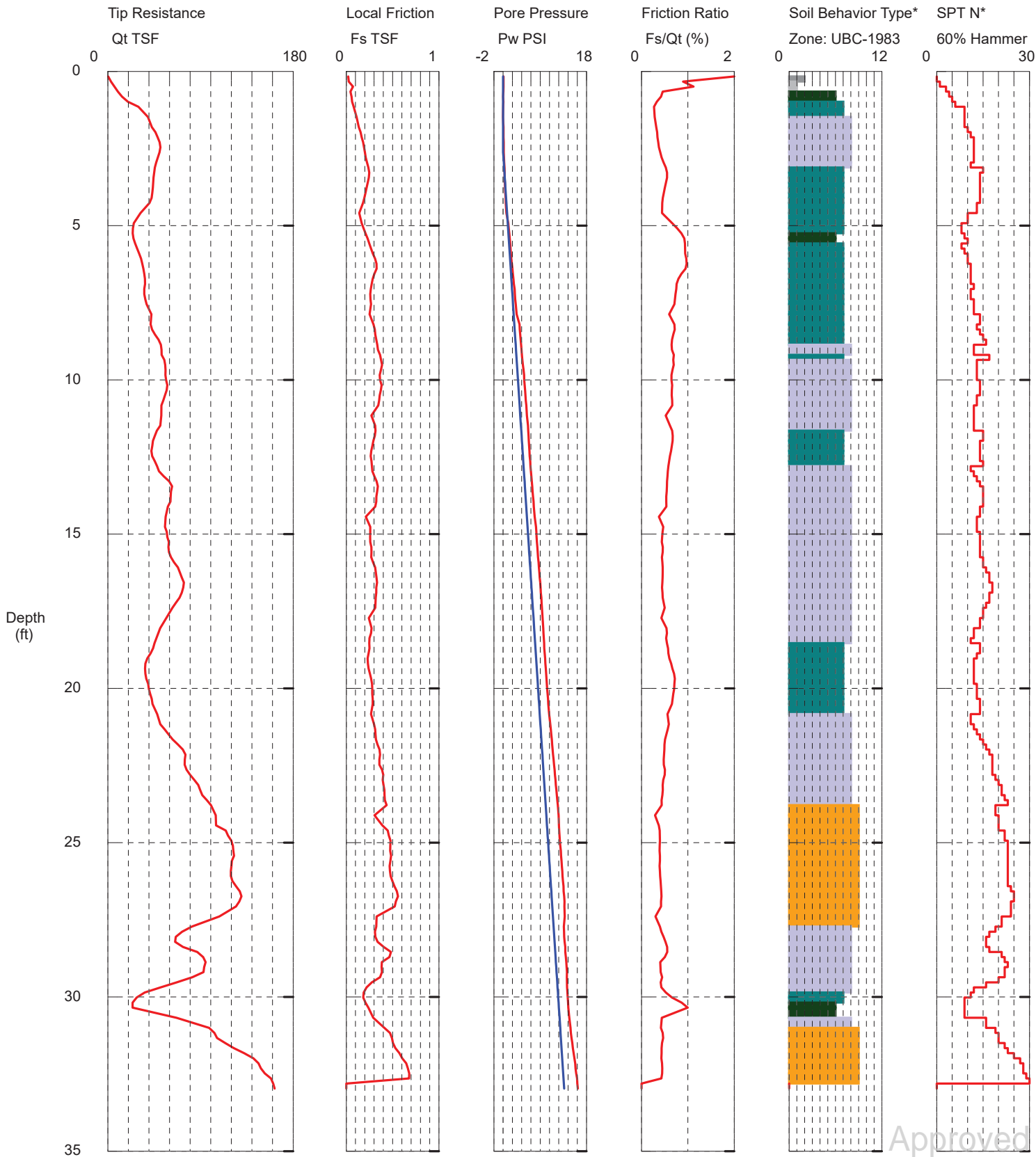
SOUTHERN EARTH SCIENCES, inc.

2024-D-391-00036
Lisa Ward
1/16/2025

Southern Earth Sciences Inc.

Operator: Pat Conroy
Sounding: C-2
Cone Used: DDG1485
Groundwater: 2.8 feet

CPT Date/Time: 7/21/2023 10:01:44 AM
Location: Camp Helen State Park
Job Number: P23-0329
Elevation: +5 Feet (Approx.)



1 sensitive fine grained
2 organic material
3 clay

4 silty clay to clay
5 clayey silt to silty clay
6 sandy silt to clayey silt

7 silty sand to sandy silt
8 sand to silty sand
9 sand

10 gravelly sand to sand
11 very stiff fine grained (*)
12 sand to clayey sand (*)

Changenroy

N30 276705W 85 088801

*Soil behavior type and SPT based on data from UBC-1983

Approved
2024-D-391-00036
Lisa Ward
7/26/2023

Page 1 of 1

METHOD: Direct Push
DRILLER: PC
ENGR / GEOL: LF
CE ELEVATION: +5 ft

LOG OF BORING P23-0329.GPJ SES PC FL.GDT 9/6/23

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1/16/2025

LOG OF BORING HA-1

Page 1 of 1

PROJECT: Camp Helen State Park Improvements
LOCATION: Bay County, Florida
PROJECT NO.: P23-0329
DATE: 07/20/23

METHOD: Hand Auger
DRILLER: HL
ENGR / GEOL: LF
SURFACE ELEVATION: +14 ft

Elevation / Depth	Soil Symbols Sampler Symbols and Field Test Data	USCS	LOCATION	▲ N Value (blows/ft)	NATURAL MOISTURE (%)	ATTERBERG LIMITS (%)			PASSING #200 SIEVE (%)
			Per Plan	20 40 60 80		LL	PL	PI	
				Atterberg Limits Natural Moisture					
				PL MC LL					
14 0			Gray Fine SAND with Organics						
		SP	Light Gray Fine SAND						
13 1									
12 2									
11 3									
		SP	Tan and Orange Fine SAND						
10 4					5				2
9 5									
		SP	Light Tan Fine SAND						
8 6									
7 7									
6 8									
5 9									
4 10									
3 11									

Water Level Est. Seasonal High GWL: ▾ Measured: ▾ Perched: ▾
 Water Observations: Groundwater Not Encountered

Notes:
 -Elevations Should Be Considered Approximate

N - SPT Data (Blows/Ft) P - Pocket Penetrometer (tsf)
 Sample Key: ▨ SPT ▩ Shelby Tube

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 1/16/2025

LOG OF BORING P23-0329.GPJ SES PC FL GDT 9/6/23

LOG OF BORING HA-2

PROJECT: Camp Helen State Park Improvements
LOCATION: Bay County, Florida
PROJECT NO.: P23-0329
DATE: 07/20/23

METHOD: Hand Auger
DRILLER: HL
ENGR / GEOL: LF
SURFACE ELEVATION: +4 ft

Elevation / Depth	Soil Symbols Sampler Symbols and Field Test Data	USCS	LOCATION		▲ N Value (blows/ft)	NATURAL MOISTURE (%)	ATTERBERG LIMITS (%)				PASSING #200 SIEVE (%)
			Per Plan	MATERIAL DESCRIPTION	20 40 60 80		LIQUID LIMIT LL	PLASTIC LIMIT PL	PLASTICITY INDEX PI		
					Atterberg Limits Natural Moisture						
					PL MC LL					20 40 60 80	
4.0 0.0			SP	Gray, Light Gray, and Tan Fine SAND with Trace Organics							
3.5 0.5											
3.0 1.0											
2.5 1.5			SP	Light Gray Fine SAND							
2.0 2.0											
1.5 2.5											
1.0 3.0			SP	Gray Fine SAND							
0.5 3.5											
0.0 4.0											
-0.5 4.5											
-1.0 5.0											

Water Level Est. Seasonal High GWL: Measured: Perched:
Water Observations: Groundwater Measured at 3.1 Feet
Below Existing Ground Surface

N - SPT Data (Blows/Ft) P - Pocket Penetrometer (tsf)

Sample Key: SPT Shelby Tube

Notes:
-Elevations Should Be Considered Approximate

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

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Page 1 of 1

METHOD: Hand Auger
DRILLER: HL
ENGR / GEOL: LF
CE ELEVATION: +17 ft

LOG OF BORING P23-0329.GPJ SES PC FL.GDT 9/6/23

Notes:

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1/16/2025

Page 1 of 1

METHOD: Hand Auger
DRILLER: HL
ENGR / GEOL: LF
SURFACE ELEVATION: +4 ft

LOG OF BORING P23-0329.GPJ SES PC FL.GDT 9/6/23

Notes:

- Elevations Should Be Considered Approximate

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Lisa Ward
1/16/2025

Page 1 of 1

METHOD: Hand Auger
DRILLER: HL
ENGR / GEOL: LF
SURFACE ELEVATION: +17 ft

OG OF BORING P23-0329.GPJ SES PC FL.GDT 9/6/23

Notes:

- Elevations Should Be Considered Approximate

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LOG OF BORING HA-6

Page 1 of 1

PROJECT: Camp Helen State Park Improvements
LOCATION: Bay County, Florida
PROJECT NO.: P23-0329
DATE: 07/20/23

METHOD: Hand Auger
DRILLER: HL
ENGR / GEOL: LF
SURFACE ELEVATION: +20 ft

Elevation / Depth	Soil Symbols Sampler Symbols and Field Test Data	USCS	LOCATION		▲ N Value (blows/ft)				NATURAL MOISTURE (%)	ATTERBERG LIMITS (%)			PASSING #200 SIEVE (%)
			Per Plan	MATERIAL DESCRIPTION	20 40 60 80					LL	PL	PI	
					Atterberg Limits Natural Moisture								
					PL	MC	LL						
20 0		SP-SM SP	Gray Slightly Silty Fine SAND with Organics										
19 1		SP	Light Gray Fine SAND										
18 2													
17 3													
16 4		SP	Orange Fine SAND										
15 5													
14 6													
13 7		SP	Tan and Light Tan Fine SAND										
12 8													
11 9													
10 10													
9 11													

Water Level Est. Seasonal High GWL: ☐ Measured: ☒ Perched: ☒
 Water Observations: Groundwater Not Encountered

Notes:
 -Elevations Should Be Considered Approximate

N - SPT Data (Blows/Ft) P - Pocket Penetrometer (tsf)
 Sample Key: ☒ SPT ☒ Shelby Tube

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 2024-D-391-00036
 Lisa Ward
 1/16/2025

LOG OF BORING HA-10

Page 1 of 1

PROJECT: Camp Helen State Park Improvements
LOCATION: Bay County, Florida
PROJECT NO.: P23-0329
DATE: 07/20/23

METHOD: Hand Auger
DRILLER: HL
ENGR / GEOL: LF
SURFACE ELEVATION: +18 ft

Elevation / Depth	Soil Symbols Sampler Symbols and Field Test Data	USCS	LOCATION	▲ N Value (blows/ft)	Atterberg Limits Natural Moisture				NATURAL MOISTURE (%)	ATTERBERG LIMITS (%)			PASSING #200 SIEVE (%)	
			Per Plan	20	40	60	80	LL		PL	PI			
				PL	MC	LL								
				20	40	60	80							
MATERIAL DESCRIPTION														
18 0		SP	Organics Light Gray Fine SAND											
17 1														
16 2														
15 3														
14 4														
13 5			SP	Orange Fine SAND										
12 6														
11 7														
10 8			SP	Light Tan Fine SAND										
9 9														
8 10														

Water Level Est. Seasonal High GWL: ☐ Measured: ☒ Perched: ☒
 Water Observations: Groundwater Not Encountered

Notes:
 -Elevations Should Be Considered Approximate

N - SPT Data (Blows/Ft) P - Pocket Penetrometer (tsf)
 Sample Key: ☒ SPT ☐ Shelby Tube

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 Lisa Ward
 1/16/2025

LOG OF BORING P23-0329.GPJ SES PC FL GDT 9/6/23

LOG OF BORING HA-12

Page 1 of 1

PROJECT: Camp Helen State Park Improvements
LOCATION: Bay County, Florida
PROJECT NO.: P23-0329
DATE: 07/20/23

METHOD: Hand Auger
DRILLER: HL
ENGR / GEOL: LF
SURFACE ELEVATION: +16 ft

Elevation / Depth	Soil Symbols Sampler Symbols and Field Test Data	USCS	LOCATION	▲ N Value (blows/ft)	NATURAL MOISTURE (%)	ATTERBERG LIMITS (%)			PASSING #200 SIEVE (%)					
			Per Plan	20 40 60 80		LL	PL	PI						
				Atterberg Limits Natural Moisture										
				PL MC LL										
16.0 0.0			Gray Fine SAND with Organics											
15.5 0.5		SP	Light Gray and Tan Fine SAND											
15.0 1.0														
14.5 1.5														
14.0 2.0														
13.5 2.5														
13.0 3.0														
12.5 3.5														
12.0 4.0		SP	Light Orange Fine SAND											
11.5 4.5														
11.0 5.0														

Water Level Est. Seasonal High GWL: ☐ Measured: ☒ Perched: ☒
 Water Observations: Groundwater Not Encountered

Notes:
 -Elevations Should Be Considered Approximate

N - SPT Data (Blows/Ft) P - Pocket Penetrometer (tsf)
 Sample Key: ☒ SPT ☐ Shelby Tube

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LOG OF BORING P23-0329.GPJ SES PC FLGDT 9/6/23

LOG OF BORING HA-13

Page 1 of 1

PROJECT: Camp Helen State Park Improvements
LOCATION: Bay County, Florida
PROJECT NO.: P23-0329
DATE: 07/20/23

METHOD: Hand Auger
DRILLER: PC/KK
ENGR / GEOL: LF
SURFACE ELEVATION: +10 ft

Elevation / Depth	Soil Symbols Sampler Symbols and Field Test Data		USCS	LOCATION	▲ N Value (blows/ft)		NATURAL MOISTURE (%)	ATTERBERG LIMITS (%)			PASSING #200 SIEVE (%)			
				Per Plan	20	40		60	80	LIQUID LIMIT		PLASTIC LIMIT	PLASTICITY INDEX	
					Atterberg Limits Natural Moisture									
						PL		MC	LL					
10	0			MATERIAL DESCRIPTION	20	40	60	80	LL	PL	PI			
			SP	Light Gray Fine SAND with Trace Organics										
			SP	Tan and Light Brown Fine SAND										
9	1													
8	2													
7	3													
6	4													
			SP	Tan Fine SAND										
5	5													

Water Level Est. Seasonal High GWL: ▾ Measured: ▾ Perched: ▾
 Water Observations: Groundwater Measured at 4.5 Feet
 Below Existing Ground Surface

Notes:
 -Elevations Should Be Considered Approximate

N - SPT Data (Blows/Ft) P - Pocket Penetrometer (tsf)
 Sample Key: ▨ SPT ▩ Shelby Tube

SOUTHERN EARTH SCIENCES, inc.

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 2024-D-391-00036
 Lisa Ward
 1/16/2025

LOG OF BORING P23-0329.GPJ SES PC FL GDT 9/6/23

Page 1 of 1

METHOD: Hand Auger
DRILLER: PC/KK
ENGR / GEOL: LF
SURFACE ELEVATION: +10 ft

LOG OF BORING P23-0329.GPJ SES PC FL.GDT 9/6/23

Notes:

-Elevations Should Be Considered Approximate

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2024-D-391-00036
Lisa Ward
1/16/2025

LOG OF BORING HA-15

Page 1 of 1

PROJECT: Camp Helen State Park Improvements
LOCATION: Bay County, Florida
PROJECT NO.: P23-0329
DATE: 07/20/23

METHOD: Hand Auger
DRILLER: HL
ENGR / GEOL: LF
SURFACE ELEVATION: +10 ft

Elevation / Depth	Soil Symbols Sampler Symbols and Field Test Data	USCS	LOCATION	▲ N Value (blows/ft)	NATURAL MOISTURE (%)	ATTERBERG LIMITS (%)			PASSING #200 SIEVE (%)
			Per Plan	20 40 60 80		LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
				Atterberg Limits Natural Moisture					
				PL MC LL					
10 0			MATERIAL DESCRIPTION	20 40 60 80		LL	PL	PI	
		SP-SM	Brown Slightly Silty Fine SAND with Trace Rock and Organics						
		SP-SC	Brown and Light Brown Slightly Clayey Fine SAND						
		SP	Gray Fine SAND						
9 1									
		SP-SC	Gray and Tan Slightly Clayey Fine SAND with Shell						
8 2		SP	Gray, Tan, and Orange Fine SAND						
		SP	Gray Fine SAND with Shell						
7 3		SP	Light Gray Fine SAND						
6 4					4				2
5 5									

Water Level Est. Seasonal High GWL: Measured: Perched:

Water Observations: Groundwater Not Encountered

Notes:

-Elevations Should Be Considered Approximate

N - SPT Data (Blows/Ft) P - Pocket Penetrometer (tsf)

Sample Key: SPT Shelby Tube

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LOG OF BORING P23-0329.GPJ SES PC FL GDT 9/6/23

Page 1 of 1

METHOD: Hand Auger
DRILLER: HL
ENGR / GEOL: LF
SURFACE ELEVATION: +10 ft

[illegible]

- Elevations Should Be Considered Approximate

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LOG OF BORING HA-17

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PROJECT: Camp Helen State Park Improvements
LOCATION: Bay County, Florida
PROJECT NO.: P23-0329
DATE: 07/20/23

METHOD: Hand Auger
DRILLER: HL
ENGR / GEOL: LF
SURFACE ELEVATION: +14 ft

Elevation / Depth	Soil Symbols Sampler Symbols and Field Test Data	USCS	LOCATION		▲ N Value (blows/ft)	NATURAL MOISTURE (%)	ATTERBERG LIMITS (%)			PASSING #200 SIEVE (%)	
			Per Plan	MATERIAL DESCRIPTION	20 40 60 80		LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX		
					Atterberg Limits Natural Moisture						
					PL MC LL						
14 0					20 40 60 80		LL	PL	PI		
		SP-SM	Brown Slightly Silty Fine SAND with Trace Organics								
		SP	Light Brown and Tan Fine SAND								
13 1		SP	Light Tan Fine SAND								
12 2											
11 3											
10 4		SP	Gray and Light Gray Fine SAND								
9 5											
8 6											

Water Level Est. Seasonal High GWL: ☒ Measured: ☒ Perched: ☒
 Water Observations: Groundwater Not Encountered

Notes:
 -Elevations Should Be Considered Approximate

N - SPT Data (Blows/Ft) P - Pocket Penetrometer (tsf)
 Sample Key: ☒ SPT ☒ Shelby Tube

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LOG OF BORING P23-0329.GPJ SES PC FL GDT 9/6/23

LOG OF BORING HA-18

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PROJECT: Camp Helen State Park Improvements
LOCATION: Bay County, Florida
PROJECT NO.: P23-0329
DATE: 07/20/23

METHOD: Hand Auger
DRILLER: HL
ENGR / GEOL: LF
SURFACE ELEVATION: +10 ft

Elevation / Depth	Soil Symbols Sampler Symbols and Field Test Data		USCS	LOCATION	▲ N Value (blows/ft)				NATURAL MOISTURE (%)	ATTERBERG LIMITS (%)			PASSING #200 SIEVE (%)
				Per Plan	20	40	60	80		LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
					Atterberg Limits Natural Moisture								
					PL	MC	LL						
10 0			SP-SC	Brown Slightly Clayey Fine SAND with Trace Organics									
9 1													
8 2			SP	Tan and Light Brown Fine SAND									
7 3													
6 4			SP	Tan Fine SAND									
5 5			SP-SC	Dark Gray Slightly Clayey Fine SAND					13				8

Water Level Est. Seasonal High GWL: ☐ Measured: ☒ Perched: ☐
 Water Observations: Groundwater Not Encountered

Notes:

-Elevations Should Be Considered Approximate

N - SPT Data (Blows/Ft) P - Pocket Penetrometer (tsf)

Sample Key: ☒ SPT ☐ Shelby Tube

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LOG OF BORING P23-0329.GPJ SES PC FL GDT 9/6/23

LOG OF BORING SW-1

Page 1 of 1

PROJECT: Camp Helen State Park Improvements
LOCATION: Bay County, Florida
PROJECT NO.: P23-0329
DATE: 07/21/23

METHOD: Hand Auger
DRILLER: PC
ENGR / GEOL: LF
SURFACE ELEVATION: +7 ft

Elevation / Depth	Soil Symbols Sampler Symbols and Field Test Data	USCS	LOCATION	▲ N Value (blows/ft) Atterberg Limits Natural Moisture PL MC LL 20 40 60 80	NATURAL MOISTURE (%)	ATTERBERG LIMITS (%)			PASSING #200 SIEVE (%)
			Per Plan			LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
			MATERIAL DESCRIPTION			LL	PL	PI	
7 0		SP	Tan Fine SAND with Trace Organics						
		SP	Tan and Orange Fine SAND with Trace Organics						
6 1									
5 2									
4 3	▽	SP	Tan Fine SAND						
3 4	▼								
2 5									
1 6									

Water Level Est. Seasonal High GWL: ▽ Measured: ▼ Perched: ▼
 Water Observations: Groundwater Measured at 4.3 Feet
 Below Existing Ground Surface

Notes:

-Estimated Seasonal High Groundwater 2.9 Feet (+/-0.5 Feet) Below Existing Ground Surface
 -Elevations Should Be Considered Approximate

N - SPT Data (Blows/Ft) P - Pocket Penetrometer (tsf)

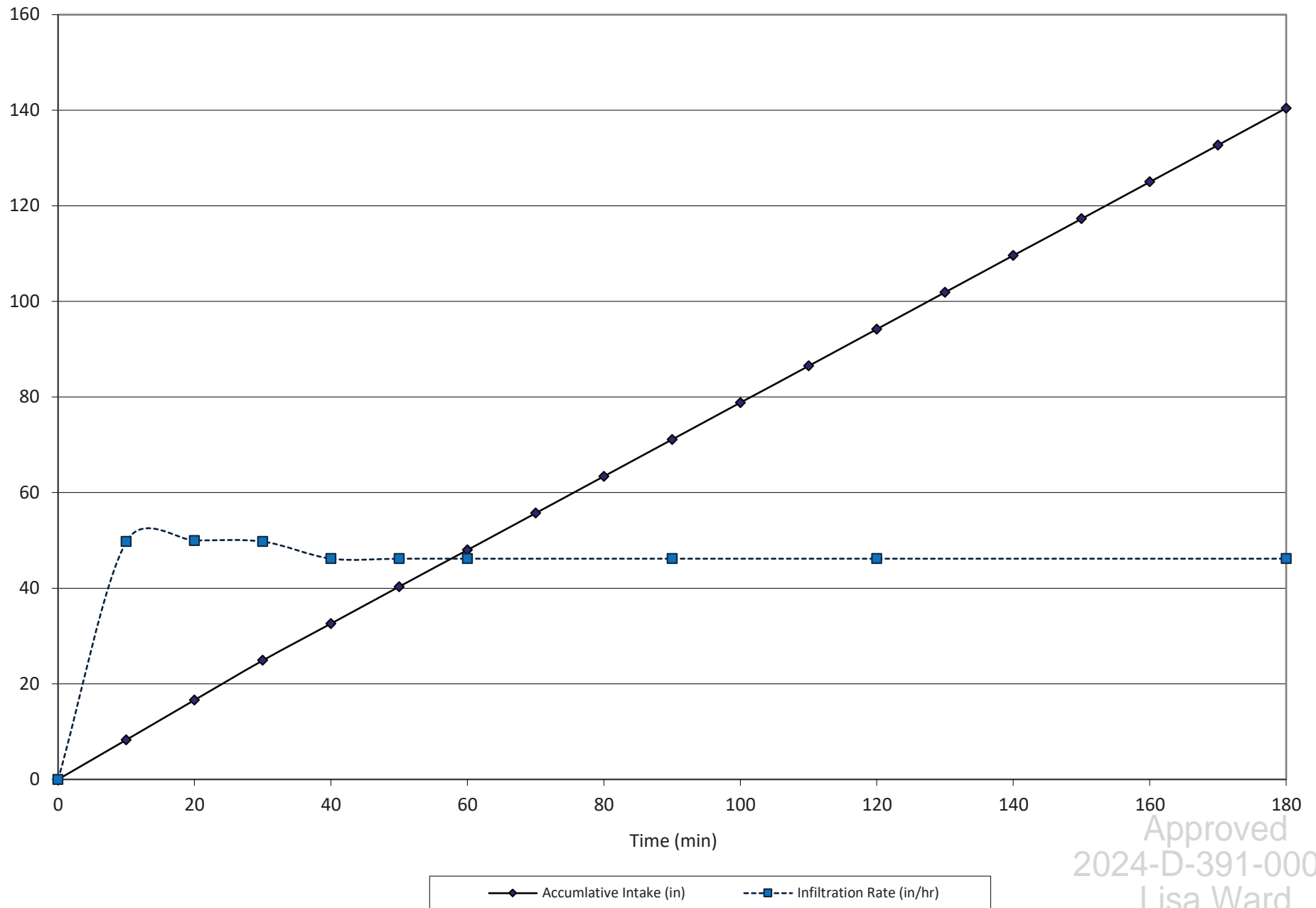
Sample Key: ▣ SPT ▣ Shelby Tube

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Table 1
Double Ring Infiltrometer Test at SW-1



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Important Information About Your Geotechnical Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

The following information is provided to help you manage your risks.

Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical engineering study conducted for a civil engineer may not fulfill the needs of a construction contractor or even another civil engineer. Because each geotechnical engineering study is unique, each geotechnical engineering report is unique, prepared *solely* for the client. No one except you should rely on your geotechnical engineering report without first conferring with the geotechnical engineer who prepared it. *And no one — not even you — should apply the report for any purpose or project except the one originally contemplated.*

Read the Full Report

Serious problems have occurred because those relying on a geotechnical engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

A Geotechnical Engineering Report Is Based on A Unique Set of Project-Specific Factors

Geotechnical engineers consider a number of unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical engineering report that was:

- not prepared for you,
- not prepared for your project,
- not prepared for the specific site explored, or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical engineering report include those that affect:

- the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a light industrial plant to a refrigerated warehouse,

- elevation, configuration, location, orientation, or weight of the proposed structure,
- composition of the design team, or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes—even minor ones—and request an assessment of their impact. *Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.*

Subsurface Conditions Can Change

A geotechnical engineering report is based on conditions that existed at the time the study was performed. *Do not rely on a geotechnical engineering report* whose adequacy may have been affected by: the passage of time; by man-made events, such as construction on or adjacent to the site; or by natural events, such as floods, earthquakes, or groundwater fluctuations. *Always* contact the geotechnical engineer before applying the report to determine if it is still reliable. A minor amount of additional testing or analysis could prevent major problems.

Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ—sometimes significantly—from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide construction observation is the most effective method of managing the risks associated with unanticipated conditions.

A Report's Recommendations Are *Not* Final

Do not overrely on the construction recommendations included in your report. *Those recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations only by observing actual

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subsurface conditions revealed during construction. *The geotechnical engineer who developed your report cannot assume responsibility or liability for the report's recommendations if that engineer does not perform construction observation.*

A Geotechnical Engineering Report Is Subject to Misinterpretation

Other design team members' misinterpretation of geotechnical engineering reports has resulted in costly problems. Lower that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Contractors can also misinterpret a geotechnical engineering report. Reduce that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing construction observation.

Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical engineering report should *never* be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, *but recognize that separating logs from the report can elevate risk.*

Give Contractors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make contractors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give contractors the complete geotechnical engineering report, *but* preface it with a clearly written letter of transmittal. In that letter, advise contractors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. *Be sure contractors have sufficient time to perform additional study.* Only then might you be in a position to give contractors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

Read Responsibility Provisions Closely

Some clients, design professionals, and contractors do not recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that

have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations" many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help others recognize their own responsibilities and risks. *Read these provisions closely.* Ask questions. Your geotechnical engineer should respond fully and frankly.

Geoenvironmental Concerns Are Not Covered

The equipment, techniques, and personnel used to perform a *geoenvironmental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnical engineering report does not usually relate any geoenvironmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures.* If you have not yet obtained your own geoenvironmental information, ask your geotechnical consultant for risk management guidance. *Do not rely on an environmental report prepared for someone else.*

Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the *express purpose* of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, a number of mold prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; ***none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.***

Rely on Your ASFE-Member Geotechnical Engineer for Additional Assistance

Membership in ASFE/The Best People on Earth exposes geotechnical engineers to a wide array of risk management techniques that can be of genuine benefit for everyone involved with a construction project. Confer with you ASFE-member geotechnical engineer for more information.



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CAMP HELEN STATE PARK

Park Improvements

FDOT Design Manual

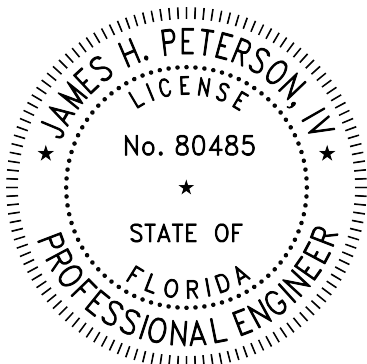
JANUARY 3rd 2025



Prepared By:



James H. Peterson IV, P.E. FL License # 80485
G&A License # 7879



GEORGE & ASSOCIATES CONSULTING ENGINEERS, INC.
1967 COMMON WEALTH LANE, SUITE 200
TALLAHASSEE, FL 32303
CERTIFICATE OF AUTHORIZATION: 7879
JAMES H. PETERSON, I.V., P.E. NO. 80485

THIS ITEM HAS BEEN DIGITALLY SIGNED AND SEALED BY
JAMES H. PETERSON, IV, P.E. ON THE DATE ADJACENT TO
THE SEAL.

PRINTED COPIES OF THIS DOCUMENT ARE NOT
CONSIDERED SIGNED AND SEALED AND THE SIGNATURE
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Approved
2024-D-391-00036
Lisa Ward
1/16/2025

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Attachment 3 – Spread Tabulations

Attachment 4 – Cross Drain and Culvert Calculations

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Attachment 6 – Pre and Post Stage Elevations

Attachment 7 – Model Inputs

CAMP HELEN STATE PARK IMPROVEMENT PROJECT - NARRATIVE

INTRODUCTION

Camp Helen State Park is located at 23937 Panama City Beach Parkway, Panama City Beach, Florida, 32413, situated in Bay County parcel #35205-000-000 within Section 31, Township 2 South, Range 17 West. Camp Helen State Park (CHSP) encompasses approximately 199 acres. The Gulf of Mexico and Walton County are adjacent to the south and west park boundary, respectively. The waterbody of Powell Lake is situated on the east and north park boundaries.

The improvements proposed at CHSP are expected to increase the recreational opportunities. The entire project area encompasses approximately 3.20 acres, this includes three separate site locations. The project area is comprised of an area located on the north side of State Road 30A (SR30A), an area on the south side of SR30A, and discrete areas within the Florida Department of Transportation (FDOT) Rights-of-Way (ROW). The cumulative limits of construction within FDOT ROW are approximately one acre. Please find the project location map on **Sheet C004** of the **Drawings**.

On the north side of SR30A, the construction of a day-use facility is proposed. The **Drawings** illustrate the construction of the new right and left turn lanes on SR30A to enter the proposed driveway. The new driveway will provide access to a proposed day-use picnic area which will include a 20-stall parking area, 14-fixture restroom, 2 picnic pavilions (approx. 20'x20'), with ADA-compliant routes for beach access including hardscaped pathways also equipped with stairs. Stormwater runoff from the north side improvements within CHSP boundaries, including a portion of the new driveway apron, will be captured and treated on-site.

In the ROW of SR30A, the **Drawings** illustrate the new construction of right and left turn lanes on SR30A to enter the proposed driveway. The runoff generated by the proposed turn lanes will be captured by roadside ditches and conveyed within FDOT ROW for terminal discharge downstream and offsite.

On the south side of SR30A, the construction of an ADA compliant floating kayak/canoe launch is proposed. The double boat launch will primarily use the existing path from the parking area. Stormwater runoff generated from this development will not be discharged into the FDOT ROW.

The entirety of this project is within the Powell Lake closed basin watershed. Powell Lake is also classified as an Outstanding Florida Water (OFW). Please find the pre- and post-construction catchment basin maps included with this submission. The stormwater model references the catchment basins identified on these maps.

TURN LANE DESIGN

Below is a summary of the turn lane design and design criteria:

RURAL CONDITIONS

Design Speed: 65 mph
Posted Speed: 45 mph

TURN LANE DESIGN

Queue Length (Left only): 100ft (FDM 212.14.2) (4 car minimum)
Brake to Stop Distance: 290 ft
Clearance Distance: 170 ft
Total Deceleration Distance: 460 ft (Clearance Distance + Brake To stop Distance)
Taper: 50 ft min (this is included in clearance distance)
Total turn lane length: Total deceleration distance + Queue Length = 560 ft

Right turn lane is not required to have a queue; right turn lane total required length is 460 linear feet.

The proposed widening to west bound SR30A consists of a right turn lane at 11' wide with a cross slope of 5% and includes a proposed 5' wide keyhole bike lane as indicated in typical sections in the **Drawings**. The existing roadway is super elevated with a cross slope ranging from 9% to 10.5%. There is a proposed 6' wide proposed shoulder comprised of 2' paved and 4' as grassed shoulder. The grass (sod) shoulder slope must not exceed 3%. Beyond the shoulder, the proposed grades will return to match existing land surface at a 1:4 (V:H) slope (25%).

The proposed east bound left turn lane is 12' wide and has a cross slope of 5%. The existing roadway, adjacent to the proposed turn lane, is super elevated with a cross slope that transitions from 6% to 10.8%. The proposed shoulder is comprised of a 2' paved and 4' sod, in which the slope of the grassed shoulder must not exceed 3%. Beyond the 6' wide shoulder, the proposed grades will return to match existing land surface at a 1:4 (V:H) slope (25%).

PAVEMENT DESIGN

In accordance with FDOT Flexible Pavement Design Manual, January 2023 edition, the pavement design specifications are as follows:

- For the Eastbound and Westbound Lane widening:
 - Optional base group 9
 - Type SP structural course (Traffic C) (PG 76-22) (3'')
 - Friction Course FC-5 (3/4") (PG 76-22)
- For the Shoulder Pavement:
 - Optional base group 1
 - Type SP structural course (Traffic C) (PG 76-22) (1.5'')
 - Friction Course FC-5 (3/4") (PG 76-22)

Please find **Sheet C005** of the **Drawings** for typical sections.

MEDIAN IMPACTS AND DRAINAGE CALCULATIONS

The proposed east bound left turn lane will be impacting the existing median. The proposed turn lane will be superelevated to flow toward the south. Please find **Catchment Basin Maps**, basin **PR-7**. The proposed impacts to the existing median will involve:

- The removal of one and a half landscape islands (**Drawings, Sheet C201**).
- A reduction in median ditch freeboard (**Attachment 1, Ditch Hydraulic Worksheet**).
- Existing french drain inlets, Storm structures **S-1** and **S-2** (**Catchment Basin Maps**) will need to be raised up to meet the proposed grade (**Drawings, Sheet C601**).

To alleviate the amount of stormwater draining to the impacted median ditch, the existing culvert pipe that conveys stormwater from structure **S-4** across the median opening to the mitered end section in the westerly median, will be abandoned and filled with flowable fill. The stormwater that is collected via curb inlets **S-4** and **S-5** (Catchment Basin Map) will be piped to the south side ROW via a cross drain and will enter the south side ROW drainage system. See the median ditch hydraulic calculation sheet that models the reduced basin areas for the altered median ditch (**Attachment 1**). The existing French drain inlets in the median are proposed to be raised up to meet the proposed grade (approx. elevation 7').

The hydraulics of the median ditch were analyzed using the Rational Method, the results of a 10-year (10YR) storm with a time of concentration (TOC) of 10 minutes yielded a freeboard of 0.46 feet within the median ditch. At almost one-half a foot, this does not satisfy the one-foot minimum freeboard requirement per FDOT design standards. The depth of the existing median ditch depth ranges from 1 to 1.5 feet, with side slopes not exceeding 1:4 (25%). Although, considering the types of soils present (i.e. sands) and safety concerns, steeper slopes are not recommended. See **Attachment 1** for median ditch calculations.

The soils in this area have high percolation rates. According to the United States Department of Agriculture (USDA) National Resource Conservation Service (NRCS), the predominant soil types are Lakeland and Kureb Sands. The soils are categorized by USDA as hydrological group 'A,' see **Attachment 2** (USDA NRCS soils map). A field study was conducted to determine percolation rates of site soils by using a Double Ring Infiltrometer (DRI). The results of the DRI indicated an unsaturated vertical infiltration rate of 46 inches per hour with a 1.5 correlation factor with respect to horizontal hydraulic conductivity. Please find the Geotechnical Report, dated September 12, 2023, included with this submission. Due to these high infiltration rates, it is likely that the median ditch will perform better than the calculations indicate as they do not consider infiltration.

Every effort was made to meet FDOT median ditch criteria, but vehicular safety was chosen as the priority. The left turn lane has a 6' wide shoulder and 4(h):1(v) maximum slopes to meet the existing grade. Shoulder width and maximum slopes are vehicular safety standards and therefore the decision was made to maintain these design standards, with the unfortunate consequence of not being able to meet all of the FDOT criteria for minimum freeboard and a 5' wide ditch bottom.

SOUTH SIDE ROW STORMWATER SYSTEM

The south side of SR30A is currently being modified by FDOT project #437759-1-52-01. The design drainage manual (post-conditions) and plans for FDOT project #437759-1-52-01 define the existing conditions for south side ROW drainage system. Currently, stormwater runoff from the eastbound lanes sheet flow into drainage ditches at the south side ROW, except for the newly added right turn lane which was constructed with a curb and gutter (FDOT Project #437759-1-52-01). The stormwater flows west in the drainage ditches until it reaches an approximately 15-acre wetland that extends into Camp Helen State Park property. A 3' by 3.5' box culvert crosses SR30A allowing the stormwater to drain north and enters another wetland (part

of Camp Helen State Park) which flows into a drainage ditch, within Camp Helen State Park, that ultimately flows into Powell Lake.

ALTERNATIVES CONSIDERED

Two alternatives considered for the proposed improvements were: either directing the stormwater runoff to the north side ROW or installing additional exfiltration trenches in the median. Both alternatives were avoided due to the following reasons:

1. All the utilities are running along the north side of 30A. In this area there are approximately 6 underground utilities in the north side ROW. Threading a gravity pipe through these utilities or relocating the utilities would present additional construction challenges.
2. The roadway is super elevated, and the north side ROW ditch elevation is approximately 11' and the invert in the existing stormwater structures **S-4** (Catchment Basin Map) is 8.5'. This area generally slopes down from north to south, therefore routing stormwater to the north would present additional grading challenges.
3. Exfiltration trenches were discouraged by the FDOT, due to maintenance issues, during a pre-application meeting on 8/13/2024 (See uploaded meeting minutes).

COMPUTER MODELING AND DESIGN CALCULATIONS

The engineering software used to model the south side ROW drainage system was *Bentley's Flow Master* and *Streamline Technologies StormWise* (formerly known as *ICPR*). The *StormWise* software was used to perform analyses of forty-two (42) different storm criteria to assist with determining the critical event, pre vs post stormwater discharge rate conditions and stage elevations in the wetland on the south side of SR 30A. *Bentley's Flow Master* software was used to verify the capacity of the *proposed cross drain, existing driveway culvert* and *existing box cross drain (CD-1)*. Alternate computations were performed on the existing box cross drain (**CD-1**) using the rational method and hydraulic equations. These calculations were made to better replicate the type of analysis that was used in the FPID #437759-1-52-01 Drainage Report, which serves as our pre-conditions. (**Attachment 4**).

The rational method was used to evaluate ditch capacity. The rational method was used to yield a flow rate (Q), as shown on the FDOT Hydraulic Worksheets (**Attachment 1**). The *Bentley's Flow Master* yielded depth and velocity values (worksheet not provided) that were used as input values to complete the FDOT Hydraulic Worksheets.

A time of concentration of 10 minutes applied to each catchment basin, except for the undeveloped basin. A time of concentration of 26 minutes was used for the undeveloped basin (Please see **Attachment 4**, Analysis of CD-1, including pages from Project #437759-1-52-01 Drainage Report). The undeveloped basin delineation and time of concentration calculations from FDOT Project #437759-1-52-01 (currently under construction) were verified and used in the Camp Helen stormwater modeling and calculations.

The rainfall data used in the design was obtained from the National Oceanic Atmospheric Administration (NOAA) Precipitation Frequency Server. Please also find **Attachment 7** for a CN calculations table, *StormWise* model node map and input report, and NOAA rainfall data. Drainage calculations for the proposed plans were conducted to verify:

- The *proposed cross drain* will handle the 50-year (50YR) critical storm event.
- The *existing box culvert* (cross drain) will handle the 50YR critical storm event with the addition of new turn lane (impervious) and updated drainage basin delineation.

- The *driveway culvert* under the existing Camp Helen State Park driveway will handle the 25-year (25YR) critical storm criteria.
- The drainage ditches will handle the 10YR design criteria with the added stormwater.
- Existing curb inlets **S-4** and **S-5** will satisfy the allowable spread with the addition of new turn lane (impervious) and updated drainage basin delineation.
- Pre-construction versus post-construction discharge rates and volume into Powell Lake.
- The post-construction (proposed) conditions do not increase the maximum stage in the wetlands on the south side of SR30A.

EXISTING CURB INLET: SPREAD CALCULATIONS

The two (2) inlets **S-4** and **S-5**, and flume **S-3** can accommodate the additional water as the largest calculated spread was 4.11 feet. This spread is less than 6 feet thus satisfies the requirement. See **Attachment 3** for the spread tabulations.

SOUTH SIDE ROW DRAINAGE SYSTEM: DITCH CALCULATIONS

Redirecting the stormwater that flows into the existing curb inlets will add flow to the existing south side ROW drainage ditches. The drainage ditches were evaluated based on the 10 YR storm design criteria. The ditches will continue to work as designed with additional stormwater per the proposed improvements as depicted in the **Drawings**. Please see **Attachment 1** for the pre and post ditch calculation worksheet. The pre-condition ditch hydraulics is taken from the drainage manual for FDOT Project #437759-1-52-01 as this project is currently under construction.

CROSS DRAINS AND CULVERTS

Please find **Attachment 4** for modeling results for the proposed and existing cross drains and culvert, summarized as follows:

- **Box Culvert CD-1 (Existing)**
Two types of analysis were conducted on CD-1. The rational method was used as well as model outputs from *StormWise* to verify that the existing box culvert cross drain has the capacity to handle the 50YR critical storm event. This culvert is sized appropriately to handle the 50YR storm event with a tailwater (36" depth) that reaches the top of the culvert.
- **Driveway Culvert (Existing)**
Model outputs from *StormWise* were used to verify that the existing culvert has the capacity to handle the 25YR critical storm event. This culvert is sized appropriately to handle the 25YR critical storm event with a tailwater (18" depth) that reaches over top of the culvert.
- **Cross Drain (Proposed)**
The stormwater that is captured by the two (2) existing curb inlets then will be redirected to the south side ROW drainage system via a new 14" x 23" elliptical reinforced concrete pipe (RCP). The proposed elliptical pipe is an equivalent to an 18" circular pipe and will accommodate the flow generated from a 50YR critical storm. The critical duration for the 50YR storm event was 1 hour. The calculated maximum velocity of the proposed cross drain as 3.74 ft/sec which is below the threshold velocity of 4 ft/sec, which would require outlet armoring. Therefore, no armoring is proposed. A coverage of 12 inches or more is achieved for the length of the pipe, except for where it crosses under the sidewalk (currently under construction, FDOT project #437759-1-52-01). The cover over the proposed elliptical RCP is approximately 6 inches while crossing under the new sidewalk at south side ROW.

SOUTH SIDE ROW STORMWATER SYSTEM: PRE VS. POST ANALYSIS

Redirecting the stormwater that flows into the existing curb inlets from the median ditch to the south side

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CIVIL ENGINEERING - LAND USE PLANNING - ENVIRONMENTAL - SYSTEMS PLANNING - TRANSPORTATION

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1/16/2025

drainage system will expand the catchment area that is currently captured by the south side ROW drainage system. Based on the results of the software analysis, the pre- versus post- development rate control is not achieved. The largest difference in rate control between the pre- versus post- development conditions is 0.63 cubic feet per second (ft³/s). The 0.63 ft³/s increase occurs during the 100YR 1HR storm event. Given the inability to satisfy the rate control requirement, a variance (or waiver) is requested. It is reasonable to justify an exception to the requirement of rate control since the construction of turn lanes for the north side driveway access must be installed as a safety measure. Since the construction of turn lanes is necessary to accommodate the safety of motorists on SR30A, it is recommended that a variance be provided for the stormwater rate control requirement.

The south side ditch system can accommodate the additional discharge due to the proposed improvements. The pathway the stormwater navigates is through a series of ditches then wetlands until terminal discharge into Powell Lake. Although Powell Lake is a closed basin, the FDEP has a permit to open the lake once it reaches elevation 2.4' which effectively creates a pop-off elevation for the closed basin. Stage elevations in the wetland on the south side of the box culvert were reviewed. Elevation contours from the Bay County GIS data were used to approximate the wetland size. The maximum stage experienced per the *StormWise* model is shown in **Attachment 6**. The largest difference between the pre- and post-development stage elevation in the wetland was 0.03' (0.36 inches) for [both] the 100YR 24HR and 100YR 8HR storm events. That said, the flooding risk to downstream properties should be considered negligible. See **Attachments 5** for *StormWise* pre vs. post discharge rate report.

FLORIDA DEPARTMENT OF TRANSPORTATION
HYDRAULIC WORKSHEET FOR ROADSIDE DITCHES
POST DRAINAGE BASINS - MEDIAN DITCH

ATTACHMENT 1

Road:SR 30A
Project Name:CAMP HELEN STATE PARK - PARK IMPROVEMENT

Prepared by: SMU
Checked by: JP

Date: 11/8/2024
Date: 11/8/2024

STATION TO STATION	SIDE	% Slope	Drain Area (Ac)	"C"	t _c (min)	i ₁₀ (in/hr)	Q (cfs)	Q from up-stream (cfs)	Total Q (cfs)	Ditch Section			"n"	"d" (ft)	"d _{allowable} " (ft)	Calculated Freeboard	Velocity (fps)	Ditch Lining	Remarks
										S.S. (H:1V)	Bottom Width (ft)	N.S. (H:1V)							
SR 30 - Median Ditch																			
STA.143+00 to STA. 145+60	CT	0.7000	0.3351	0.63	10.00	7.7	1.618	0.000	1.618	4	1	6	0.03	0.3750	1.000	0.625	1.52	Sod	<u>BASIN PR-1</u>
STA 145+60 to STA 148+61	CT	0.7000	0.3678	0.63	10.00	7.7	1.788	1.983	3.771	4	1	6	0.03	0.5400	1.000	0.460	1.88	Sod	<u>BASIN PR-2</u>
STA. 148+61 to STA. 150+07	CT	-	0.3103	0.83	10.00	7.7	1.983	0.000	1.983	N/A	N/A	N/A	0.012	-	N/A	-	-	Conc. Flume	<u>BASIN PR-3</u>

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2024-D-391-00036

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1/16/2025

FLORIDA DEPARTMENT OF TRANSPORTATION
HYDRAULIC WORKSHEET FOR ROADSIDE DITCHES
PRE VS POST DRAINAGE BASINS -SOUTH SIDE ROW DRAINAGE DITCHES
Road: SR 30
Project Name: CAMP HELEN STATE PARK - PARK IMPROVEMENT

Prepared by: SMU Date: 12/23/2024
Checked by: JP Date: 12/23/2024

PRE CONSTRUCTION (FROM FDOT DRAINAGE MANUAL FOR PROJECT # 437759-1-52-01 CURRENTLY UNDER CONSTRUCTION)

STATION TO STATION	SIDE	% Slope	Length (ft)		"C"	t _c (min)	i ₁₀ (in/hr)	Q (cfs)	Q from up- stream (cfs)	Total Q (cfs)	Ditch Section			"n"	"d" (ft)	"d _{allowable} " (ft)	Calculated Freeboard	Velocity (fps)	Ditch Lining	Side Drain Pipe (dia.)	Remarks (From FDOT Project 437759-1-52-01)
				Contributing Area (ac)							S.S. (H:1V)	Bottom Width (ft)	N.S. (H:1V)								
SR 30A - South Side ROW Ditch																					
143+43.93 to 145+86.41	RT	0.1500	242.0000	0.3800	0.79	10.00	7.7	2.312	0.000	2.312	6	5	2	0.06	0.5600	0.600	0.040	0.55	Sod	18	Ditch Over Pipe
143+93.85 to 148+33.14	RT	0.5700	439.0000	0.6300	0.83	10.00	7.7	4.026	5.856	9.882	4	5	3	0.042	0.7300	3.300	2.570	1.77	Sod		Min. Pipe size added to convey base flow: additional flow will stage up and flow over without roadway impact
148+33.14 to 155+0.00	RT	1.3900	667.0000	1.6900	0.45	10.00	7.7	5.856	0.000	5.856	4	5	4	0.06	0.5300	1.5	0.970	1.58	Sod	18	

POST CONSTRUCTION

STATION TO STATION	SIDE	% Slope	Length (ft)		"C"	t _c (min)	i ₁₀ (in/hr)	Q (cfs)	Q from up- stream (cfs)	Total Q (cfs)	Ditch Section			"n"	"d" (ft)	"d _{allowable} " (ft)	Calculated Freeboard	Velocity (fps)	Ditch Lining	Side Drain Pipe (dia.)	Remarks
				Contributing Area (ac)							S.S. (H:1V)	Bottom Width (ft)	N.S. (H:1V)								
SR 30 - South Side ROW Ditch																					
143+43.93 to 145+86.41	RT	0.1500	242.0000	0.3800	0.79	10.00	7.7	2.318	0.000	2.318	6	5	2	0.06	0.5600	0.600	0.040	0.55	Sod	18	Ditch Over Pipe
143+93.85 to 148+33.14	RT	0.5700	439.0000	0.76	0.85	10.00	7.7	4.974	9.095	14.070	4	5	3	0.042	0.8917	3.300	2.408	1.96	Sod		Contains additional area from the proposed left turn lane (Basin PR-7)
148+33.14 to 155+0.00	RT	1.3900	667.0000	2.2388	0.53	10.00	7.7	9.095	0.000	9.095	4	5	4	0.06	0.6583	1.5	0.842	1.8	Sod	18	Includes additional Stormwater from West Bound Lanes (Basins PR-4 & PR-5)

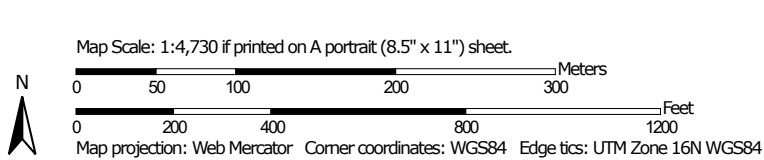
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Lisa Ward
1/16/2025

Attachment 2

Hydrologic Soil Group—Bay County, Florida
(Camp Helen State Park - Park Improvement)



Soil Map may not be valid at this scale.



Natural Resources
Conservation Service

Web Soil Survey
National Cooperative Soil Survey

Approved
2024-D-391-00036
Lisa Ward
7/2/2024
Page 1 of 4

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

Soil Rating Polygons

 A
 A/D
 B
 B/D
 C
 C/D
 D
 Not rated or not available

Soil Rating Lines

 A
 A/D
 B
 B/D
 C
 C/D
 D
 Not rated or not available

Soil Rating Points

 A
 A/D
 B
 B/D

 C
 C/D
 D
 Not rated or not available


Water Features

 Streams and Canals

Transportation

 Rails
 Interstate Highways
 US Routes
 Major Roads
 Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Bay County, Florida
Survey Area Data: Version 23, Aug 24, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Dec 31, 2009—Dec 10, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
11	Lakeland sand, 8 to 12 percent slopes	A	24.3	22.7%
41	Dirego muck	A/D	10.3	9.7%
42	Resota fine sand, 0 to 5 percent slopes	A	13.2	12.4%
45	Kureb sand, 0 to 5 percent slopes	A	13.2	12.4%
99	Water		45.8	42.9%
Totals for Area of Interest			106.8	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

ATTACHMENT 3

FLORIDA DEPARTMENT OF TRANSPORTATION
SPREAD TABULATION FORM

Project: Camp Helen Park Improvements
Description: Proposed Spread Calculations for Two Curb Inlets on SR 30 left turn lane and a Median Flume

County: Bay
Organization: G&A

Rainfall Zone: Zone 1
Post Development

Prepared By: ISMU
Checked By: JHP

Date: 11/18/2024
Date:

	Structure No.	Station	Side	Type of Structure	Drainage Area (acre)	Composite Runoff Coefficient	Rainfall Intensity (in/hr)	Overland Runoff (cfs)	Previous Inlet Bypass (cfs)	Total Runoff (cfs)	Cross Slope (ft/ft)	Longitudinal Slope (ft/ft)	Manning's n	Calculated Spread (ft)	Allowable Spread (ft)	Sumped Spread (ft)	Intercepted Flow (cfs)	Bypass Flow to Next Inlet (cfs)	Bypass to Structure No.
PR-3	S-3	148+54	LT	Flume	0.3103	0.83	4.00	1.030	0.000	1.030	0.0500	0.0100	0.016	4.11	5.00	n/a	1.030	0.000	n/a
PR-4	S-4	150+10	LT	P3	0.2388	0.75	4.00	0.712	0.000	0.712	0.0690	0.0070	0.016	3.13	5.00	n/a	0.712	0.000	n/a
PR-5	S-5	151+35	LT	P3	0.3987	0.77	4.00	1.223	0.000	1.223	0.0680	0.0080	0.016	3.77	5.00	n/a	1.223	0.000	n/a

Remarks:
Spread and bypass computations performed using the 2023 FDOT Drainage Design Guide and FDOT Greenbook.

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1/16/2025

Proposed Cross Drain

1D Links - Max

1

Sim	Link Name	Maximum Flow Rate [cfs]	Maximum US Velocity [fps]
050Y001H	Cross Drain	2.98	3.74
050Y002H	Cross Drain	2.66	3.61
050Y004H	Cross Drain	1.69	3.14
050Y008H	Cross Drain	1.99	3.30
050Y024H	Cross Drain	0.70	2.43
050Y072H	Cross Drain	0.48	2.18
050Y168H	Cross Drain	0.33	1.96
050Y240H	Cross Drain	0.41	2.08

Proposed Cross Drain

Project Description		
Friction Method	Manning Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.024	<div>50 year critical storm discharge rate - from on StormWise model results</div>
Channel Slope	0.022 ft/ft	
Rise	1.2 ft	
Span	1.9 ft	
Discharge	2.98 cfs	
Results		
Normal Depth	5.9 in	
Flow Area	0.7 ft²	
Wetted Perimeter	2.3 ft	
Hydraulic Radius	3.7 in	
Top Width	1.90 ft	
Critical Depth	6.6 in	
Percent Full	42.7 %	
Critical Slope	0.015 ft/ft	
Velocity	4.19 ft/s	
Velocity Head	0.27 ft	
Specific Energy	0.77 ft	
Froude Number	1.208	
Maximum Discharge	8.62 cfs	
Discharge Full	8.05 cfs	
Slope Full	0.161 ft/ft	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	18.0 in	<div>Tailwater Conditions</div>
Length	72.5 ft	
Number Of Steps	20	
GVF Output Data		
Upstream Depth	6.6 in	<div>Upstream depth with tailwater conditions</div>
Profile Description	N/A	
Profile Headloss	0.64 ft	
Average End Depth Over Rise	88.2 %	
Normal Depth Over Rise	42.7 %	
Downstream Velocity	1.71 ft/s	
Upstream Velocity	3.69 ft/s	
Normal Depth	5.9 in	
Critical Depth	6.6 in	
Channel Slope	0.022 ft/ft	
Critical Slope	0.015 ft/ft	

Existing Box Culvert (CD-1)

1D Links - Max

1

Sim	Link Name	Maximum Flow Rate [cfs]	Maximum US Velocity [fps]
050Y001H	Box Culvert	2.67	0.86
050Y001H	Box Culvert PRE	2.06	0.67
050Y002H	Box Culvert	2.88	0.92
050Y002H	Box Culvert PRE	2.24	0.73
050Y004H	Box Culvert	4.04	1.24
050Y004H	Box Culvert PRE	3.50	1.09
050Y008H	Box Culvert	5.27	1.52
050Y008H	Box Culvert PRE	4.80	1.42
050Y024H	Box Culvert	6.93	1.83
050Y024H	Box Culvert PRE	6.60	1.78
050Y072H	Box Culvert	9.07	2.13
050Y072H	Box Culvert PRE	8.78	2.10
050Y168H	Box Culvert	9.59	2.19
050Y168H	Box Culvert PRE	9.34	2.16
050Y240H	Box Culvert	10.42	2.28
050Y240H	Box Culvert PRE	10.11	2.25

Cross Drain - Box Culvert -CD-1

Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	50 year critical storm discharge rate from StormWise model result
Channel Slope	0.001 ft/ft	
Height	3.0 ft	
Bottom Width	3.50 ft	
Discharge	10.47 cfs	
Results		
Normal Depth	15.9 in	
Flow Area	4.6 ft²	
Wetted Perimeter	6.1 ft	
Hydraulic Radius	9.0 in	
Top Width	3.50 ft	
Critical Depth	7.8 in	
Percent Full	44.1 %	
Critical Slope	0.004 ft/ft	
Velocity	2.26 ft/s	
Velocity Head	0.08 ft	
Specific Energy	1.40 ft	
Froude Number	0.346	
Discharge Full	24.85 cfs	
Slope Full	0.001 ft/ft	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	36.0 in	Tailwater Conditions
Length	193.0 ft	
Number Of Steps	20	
GVF Output Data		
Upstream Depth	34.9 in	Upstream depth with tailwater conditions
Profile Description	N/A	
Profile Headloss	0.02 ft	
Average End Depth Over Rise	98.4 %	
Normal Depth Over Rise	44.1 %	
Downstream Velocity	1.00 ft/s	
Upstream Velocity	1.03 ft/s	
Normal Depth	15.9 in	
Critical Depth	7.8 in	
Channel Slope	0.001 ft/ft	
Critical Slope	0.004 ft/ft	

CHSP Existing Driveway Culvert

1D Links - Max

1

Sim	Link Name	Maximum Flow Rate [cfs]	Maximum US Velocity [fps]
025Y001H	Camp Helen Entrance Culvert	3.83	4.08
025Y001H	CH Driveway Culvert PRE	1.40	2.97
025Y002H	Camp Helen Entrance Culvert	3.68	4.02
025Y002H	CH Driveway Culvert PRE	1.37	2.95
025Y004H	Camp Helen Entrance Culvert	2.91	3.72
025Y004H	CH Driveway Culvert PRE	1.57	3.07
025Y008H	Camp Helen Entrance Culvert	3.86	4.09
025Y008H	CH Driveway Culvert PRE	2.13	3.37
025Y024H	Camp Helen Entrance Culvert	1.45	3.00
025Y024H	CH Driveway Culvert PRE	0.86	2.58
025Y072H	Camp Helen Entrance Culvert	1.22	2.85
025Y072H	CH Driveway Culvert PRE	0.82	2.54
025Y168H	Camp Helen Entrance Culvert	0.89	2.61
025Y168H	CH Driveway Culvert PRE	0.62	2.35
025Y240H	Camp Helen Entrance Culvert	1.11	2.77
025Y240H	CH Driveway Culvert PRE	0.76	2.49

Worksheet for Camp Helen Entrance Driveway Culvert

Project Description	
Friction Method	Manning
Solve For	Formula Normal Depth
Input Data	
Roughness Coefficient	0.024
Channel Slope	0.014 ft/ft
Rise	1.2 ft
Span	1.9 ft
Discharge	3.86 cfs
Results	
Normal Depth	7.8 in
Flow Area	1.0 ft ²
Wetted Perimeter	2.6 ft
Hydraulic Radius	4.7 in
Top Width	1.90 ft
Critical Depth	7.5 in
Percent Full	55.3 %
Critical Slope	0.015 ft/ft
Velocity	3.87 ft/s
Velocity Head	0.23 ft
Specific Energy	0.88 ft
Froude Number	0.943
Maximum Discharge	6.89 cfs
Discharge Full	6.43 cfs
Slope Full	0.038 ft/ft
Flow Type	Subcritical
GVF Input Data	
Downstream Depth	18.0 in
Length	74.5 ft
Number Of Steps	20
GVF Output Data	
Upstream Depth	9.2 in
Profile Description	N/A
Profile Headloss	0.29 ft
Average End Depth Over Rise	96.8 %
Normal Depth Over Rise	55.3 %
Downstream Velocity	2.20 ft/s
Upstream Velocity	3.17 ft/s
Normal Depth	7.8 in
Critical Depth	7.5 in
Channel Slope	0.014 ft/ft
Critical Slope	0.015 ft/ft

Discharge from 25
year critical storm
from stormwise
model result

Tailwater condition

Upstream depth with
tailwater condition

Analysis of CD-1 Based on the Rational Method

CD-1											
Runoff Calculation: Rational Method											
Design Event		Return Freq.	Storm Freq Factor, XT	Pre Runoff Coeff.	Post Runoff Coeff.	Time of Concentration	Pre Area	Post Area	Intensity	Pre $Q=C_dIA$	Post $Q=C_dIA$
		(Years)		C	C	(Minutes)	(Acres)	(Acres)	(Inch/Hr)	(cfs)	(cfs)
Min. Flow	25 Year	25	1.1	0.21	0.22	26	41.12	41.89	5.66	53.8	57.4
Design Flow	50 Year	50	1.2	0.21	0.22	26	41.12	41.89	6.25	64.8	69.1
Max. Flow	100 Year	100	1.25	0.21	0.22	26	41.12	41.89	6.8	73.4	78.3

C-Value		CD-1	
		Area (Ac.)	
		Pre	Post
0.15	Sandy Soils	35.47	35.47
0.2	Open	2.78	2.95
0.95	Impervious	2.87	3.46
Cumulative C Value		0.21	0.22

Note: Pre-conditions are from FDOT Project ID #437759-1-52-01, See following pages for cross drain analysis from Drainage Report from aforementioned FDOT project.

Upstream Water Surface Elevation For Q=69.1		
Based on the equation: $h_1 = ((\frac{Q}{C_d A})^2 / 2g) + h_2$		
Inlet Stage Elevation	h_1 (ft)	5.633
Outlet Stage Elevation	h_2 (ft)	4.04
Acceleration due to gravity	g (ft/s ²)	32.174
Culvert Discharge Coefficient	C_d	0.65
Culvert X-Section Area	A (ft ²)	10.5
Discharge	Q (ft ³ /s)	69.1

Will not over top the road
Road surface elevation = 8'

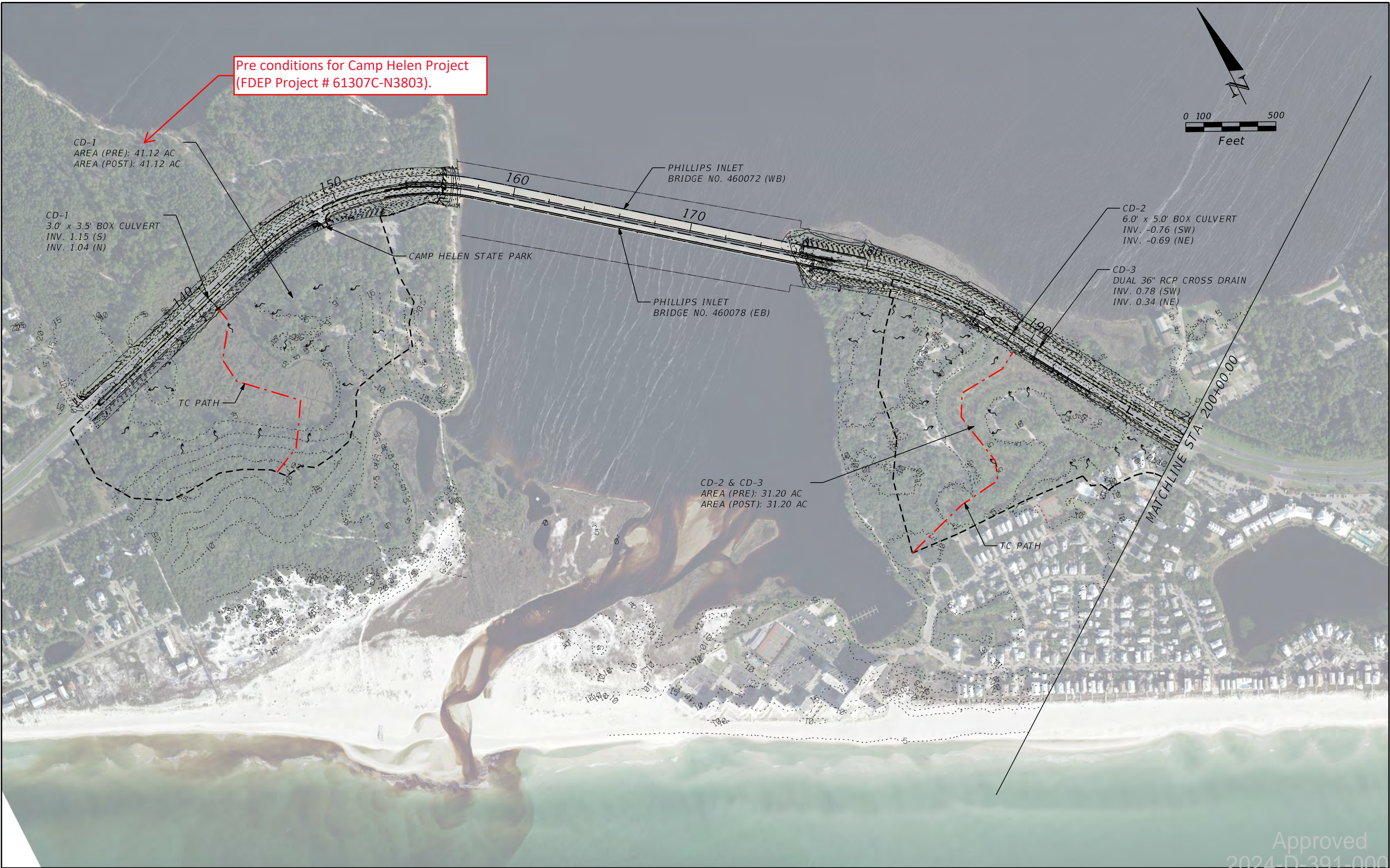
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2024-D-391-00036
Lisa Ward
1/16/2025

Attachment 4

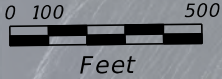
Cross Drain Analysis

Pre-conditions for proposed Camp Helen Project.

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Lisa Ward
1/16/2025



Pre conditions for Camp Helen Project
(FDEP Project # 61307C-N3803).



CD-1
AREA (PRE): 41.12 AC
AREA (POST): 41.12 AC

CD-1
3.0' x 3.5' BOX CULVERT
INV. 1.15 (S)
INV. 1.04 (N)

CAMP HELEN STATE PARK

PHILLIPS INLET
BRIDGE NO. 460072 (WB)

PHILLIPS INLET
BRIDGE NO. 460078 (EB)

CD-2
6.0' x 5.0' BOX CULVERT
INV. -0.76 (SW)
INV. -0.69 (NE)

CD-3
DUAL 36" RCP CROSS DRAIN
INV. 0.78 (SW)
INV. 0.34 (NE)

CD-2 & CD-3
AREA (PRE): 31.20 AC
AREA (POST): 31.20 AC

MATCHLINE STA. 200+00.00

REVISIONS				TRAVIS SHANNON, P.E. P.E. LICENSE NUMBER 73883 HANSON PROFESSIONAL SERVICES INC. 910 N. WAUKESHA STREET BONIFAY, FL 32425 CERTIFICATE OF AUTHORIZATION 00007961	STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION			CROSS DRAIN DRAINAGE MAP	SHEET NO. 36 1/16/2025 C-1
DATE	DESCRIPTION	DATE	DESCRIPTION						
					ROAD NO.	COUNTY	FINANCIAL PROJECT ID		
					SR 30A	BAY	437759-1-52-01		

CD-1										
Runoff Calculation: Rational Method										
Design Event		Return Freq.	Storm Freq. Factor, XT	Pre Runoff Coeff.	Post Runoff Coeff.	Time of Conc.	Area	Intensity	Pre $Q=C_{xf}IA$	Post $Q=C_{xf}IA$
		(Years)		C	C	(Minutes)	(Acres)	(Inch/Hr)	(cfs)	(cfs)
Min. Flow	25 Year	25	1.10	0.20	0.21	26	41.12	5.66	52.3	53.5
Design Flow	50 Year	50	1.20	0.20	0.21	26	41.12	6.25	63.1	64.5
Max. Flow	100 Year	100	1.25	0.20	0.21	26	41.12	6.80	71.4	73.1

CD-2 & CD-3										
Runoff Calculation: Rational Method										
Design Event		Return Freq.	Storm Freq. Factor, XT	Pre Runoff Coeff.	Post Runoff Coeff.	Time of Conc.	Area	Intensity	Pre $Q=C_{xf}IA$	Post $Q=C_{xf}IA$
		(Years)		C	C	(Minutes)	(Acres)	(Inch/Hr)	(cfs)	(cfs)
Min. Flow	25 Year	25	1.10	0.20	0.21	26	31.20	5.66	38.4	40.0
Design Flow	50 Year	50	1.20	0.20	0.21	26	31.20	6.25	46.3	48.3
Max. Flow	100 Year	100	1.25	0.20	0.21	26	31.20	6.80	52.4	54.7

CD-5										
Runoff Calculation: Rational Method										
Design Event		Return Freq.	Storm Freq. Factor, XT	Pre Runoff Coeff.	Post Runoff Coeff.	Time of Conc.	Area	Intensity	Pre $Q=C_{xf}IA$	Post $Q=C_{xf}IA$
		(Years)		C	C	(Minutes)	(Acres)	(Inch/Hr)	(cfs)	(cfs)
Min. Flow	25 Year	25	1.10	0.30	0.33	50	33.13	4.13	44.8	49.0
Design Flow	50 Year	50	1.20	0.30	0.33	50	33.13	4.65	55.1	60.3
Max. Flow	100 Year	100	1.25	0.30	0.33	50	33.13	5.00	61.6	67.5

Pre conditions for Camp Helen project
(FDEP Project # 61307C-N3803)

Cross Drain C-Value Computations																					
C-Value		CD-1		CD-2 & CD-3		CD-5		CD-6		CD-7		CD-8		CD-9		CD-10		CD-11		CD-12	
		Area (Ac.)		Area (Ac.)		Area (Ac.)		Area (Ac.)		Area (Ac.)		Area (Ac.)		Area (Ac.)		Area (Ac.)		Area (Ac.)		Area (Ac.)	
		Pre	Post	Pre	Post	Pre	Post	Pre	Post	Pre	Post	Pre	Post	Pre	Post	Pre	Post	Pre	Post	Pre	Post
0.15	(Sandy Soils)	35.47	35.47	26.14	26.14	8.37	8.37	-	-	-	-	23.05	23.05	-	-	-	-	20.70	20.70	18.43	18.43
0.20	(Open)	3.04	2.78	1.99	1.63	3.46	2.46	4.68	4.20	5.51	4.80	10.33	9.87	8.80	8.66	8.75	8.60	17.51	17.16	1.89	1.71
0.30	(Residential)	-	-	1.66	1.66	17.99	17.99	-	-	-	-	-	-	-	-	-	-	-	-	-	-
0.50	(Residential)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.88	1.88
0.70	(Commercial)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.39	3.39	-	-	-	-
0.95	(Impervious)	2.61	2.87	1.42	1.78	3.31	4.31	2.13	2.61	3.06	3.77	2.82	3.28	2.35	2.49	2.46	2.61	6.75	7.09	2.41	2.59
Cumulative C-Value		0.20	0.21	0.20	0.21	0.32	0.34	0.43	0.49	0.47	0.53	0.23	0.24	0.36	0.37	0.44	0.45	0.29	0.30	0.26	0.26

Cross Drain Time of Concentration Computations										
	CD-1	CD-2 & CD-3	CD-5	CD-6	CD-7	CD-8	CD-9	CD-10	CD-11	CD-12
Sheet Flow										
Length (ft)	100	100	100	100	100	100	50	100	100	100
n	0.2	0.15	0.3	0.2	0.2	0.2	0.2	0.4	0.15	0.15
US elevation	20.5	13.0	31.0	38.0	33.0	37.0	40.0	38.0	40.0	38.0
DS elevation	19.8	10.5	29.8	37.5	32.6	36.5	38.5	37.0	38.5	37.0
Slope (ft/ft)	0.007	0.025	0.012	0.005	0.005	0.005	0.030	0.010	0.015	0.010
Intensity (2yr-24hr)	5.42	5.42	5.42	5.42	5.42	5.42	5.42	5.42	5.42	5.42
Time of Conc. (hr)	0.240	0.115	0.268	0.275	0.287	0.275	0.077	0.363	0.141	0.166
Concentrated Flow										
Length (ft)	1230	1445	260	290	60	170	0	0	700	800
US elevation	19.8	10.5	29.8	37.5	32.6	36.5	0.0	0.0	38.5	37.0
DS elevation	4.0	2.0	24.0	32.0	27.0	35.0	0.0	0.0	33.0	36.0
Slope (ft/ft)	0.013	0.006	0.022	0.019	0.093	0.009	#DIV/0!	#DIV/0!	0.008	0.001
Paved or Unpaved	Unpaved	Unpaved	Unpaved	Unpaved	Unpaved	Unpaved	Unpaved	Unpaved	Unpaved	Unpaved
Velocity (ft/s)	1.83	1.24	2.41	2.22	4.91	1.52	#DIV/0!	#DIV/0!	1.43	0.57
Time of Conc. (hr)	0.187	0.324	0.030	0.036	0.003	0.031	0.000	0.000	0.136	0.390
Ditch Flow										
Length (ft)	0	0	1900	930	1100	2060	1630	1850	1150	650
Velocity (ft/s)	1	1	1	1	1	1	1	0.5	1.5	1.5
Time of Conc. (hr)	0.000	0.000	0.528	0.258	0.306	0.572	0.453	1.028	0.213	0.120
Composite Time of Concentration										
Tc (min)	26	26	50	34	36	53	32	83	29	41

Time of Concentration calculation used for
both pre and post condition modeling.

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

Pre conditions for Camp
Helen project (FDEP
Project # 61307C-N3803)

Table 2 - Summary of Culvert Flows at Crossing: Post CD 1

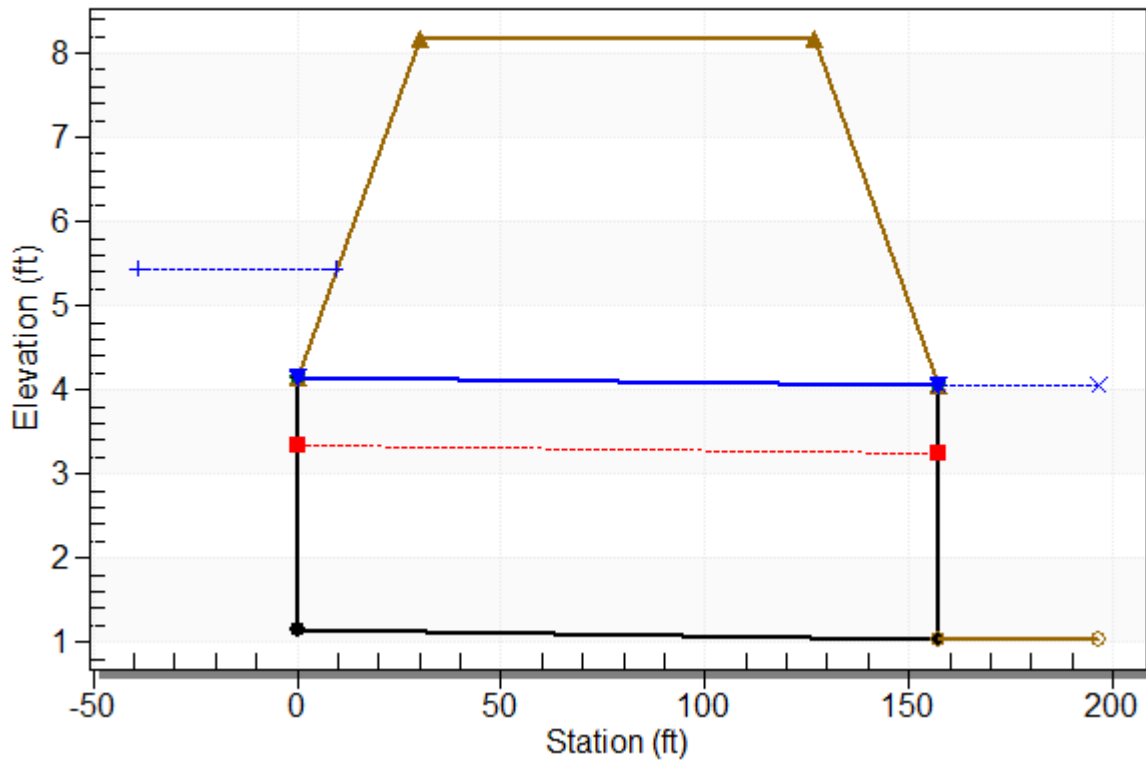
Headwater Elevation (ft)	Total Discharge (cfs)	Culvert 1 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
5.00	53.50	53.50	0.00	1
5.07	55.46	55.46	0.00	1
5.14	57.42	57.42	0.00	1
5.22	59.38	59.38	0.00	1
5.30	61.34	61.34	0.00	1
5.38	63.30	63.30	0.00	1
5.43	64.50	64.50	0.00	1
5.55	67.22	67.22	0.00	1
5.64	69.18	69.18	0.00	1
5.73	71.14	71.14	0.00	1
5.82	73.10	73.10	0.00	1
8.18	111.33	111.33	0.00	Overtopping

Water Surface Profile Plot for Culvert: Culvert 1

Pre conditions for proposed
Camp Helen project

Crossing - Post CD 1, Design Discharge - 64.5 cfs

Culvert - Culvert 1, Culvert Discharge - 64.5 cfs



Site Data - Culvert 1

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 1.15 ft

Outlet Station: 157.00 ft

Outlet Elevation: 1.04 ft

Number of Barrels: 1

Culvert Data Summary - Culvert 1

Barrel Shape: Concrete Box

Barrel Span: 3.50 ft

Barrel Rise: 3.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge (90°) Headwall

Inlet Depression: None

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

ATTACHMENT 5: Pre and Post StormWise Discharge Rate Report

1D Nodes - Max

1

Sim	Node Name	Maximum Total Inflow Rate [cfs]
002Y001H	Outfall	1.36
002Y001H	Outfall PRE w routing	1.02
002Y002H	Outfall	1.46
002Y002H	Outfall PRE w routing	1.08
002Y004H	Outfall	1.69
002Y004H	Outfall PRE w routing	1.24
002Y008H	Outfall	1.66
002Y008H	Outfall PRE w routing	1.23
002Y024H	Outfall	0.88
002Y024H	Outfall PRE w routing	0.60
002Y072H	Outfall	0.12
002Y072H	Outfall PRE w routing	0.07
002Y168H	Outfall	0.00
002Y168H	Outfall PRE w routing	0.00
002Y240H	Outfall	0.00
002Y240H	Outfall PRE w routing	0.00
005Y001H	Outfall	1.70
005Y001H	Outfall PRE w routing	1.28
005Y002H	Outfall	1.81
005Y002H	Outfall PRE w routing	1.35
005Y004H	Outfall	2.01
005Y004H	Outfall PRE w routing	1.50
005Y008H	Outfall	2.03
005Y008H	Outfall PRE w routing	1.55
005Y024H	Outfall	1.63
005Y024H	Outfall PRE w routing	1.47
005Y072H	Outfall	0.22
005Y072H	Outfall PRE w routing	0.12
005Y168H	Outfall	0.02
005Y168H	Outfall PRE w routing	0.01
005Y240H	Outfall	0.00
005Y240H	Outfall PRE w routing	0.00
010Y001H	Outfall	1.98
010Y001H	Outfall PRE w routing	1.51
010Y002H	Outfall	2.11
010Y002H	Outfall PRE w routing	1.60
010Y004H	Outfall	3.05
010Y004H	Outfall PRE w routing	2.46
010Y008H	Outfall	2.42
010Y008H	Outfall PRE w routing	1.85
010Y024H	Outfall	2.85
010Y024H	Outfall PRE w routing	2

Sim	Node Name	Maximum Total Inflow Rate [cfs]
010Y072H	Outfall	0.32
010Y072H	Outfall PRE w routing	0.19
010Y168H	Outfall	0.03
010Y168H	Outfall PRE w routing	0.02
010Y240H	Outfall	0.00
010Y240H	Outfall PRE w routing	0.00
025Y001H	Outfall	2.35
025Y001H	Outfall PRE w routing	1.82
025Y002H	Outfall	2.53
025Y002H	Outfall PRE w routing	1.95
025Y004H	Outfall	3.05
025Y004H	Outfall PRE w routing	2.46
025Y008H	Outfall	3.76
025Y008H	Outfall PRE w routing	3.27
025Y024H	Outfall	5.00
025Y024H	Outfall PRE w routing	4.72
025Y072H	Outfall	0.45
025Y072H	Outfall PRE w routing	0.28
025Y168H	Outfall	0.05
025Y168H	Outfall PRE w routing	0.03
025Y240H	Outfall	0.00
025Y240H	Outfall PRE w routing	0.00
050Y001H	Outfall	2.64
050Y001H	Outfall PRE w routing	2.06
050Y002H	Outfall	2.87
050Y002H	Outfall PRE w routing	2.23
050Y004H	Outfall	4.06
050Y004H	Outfall PRE w routing	3.51
050Y008H	Outfall	5.29
050Y008H	Outfall PRE w routing	4.81
050Y024H	Outfall	6.93
050Y024H	Outfall PRE w routing	6.60
050Y072H	Outfall	0.62
050Y072H	Outfall PRE w routing	0.38
050Y168H	Outfall	0.06
050Y168H	Outfall PRE w routing	0.04
050Y240H	Outfall	0.01
050Y240H	Outfall PRE w routing	0.01
100Y001H	Outfall	2.93
100Y001H	Outfall PRE w routing	2.30
100Y002H	Outfall	3.48
100Y002H	Outfall PRE w routing	2.85

Largest difference is
0.63 cfs

Sim	Node Name	Maximum Total Inflow Rate [cfs]
100Y004H	Outfall	5.31
100Y004H	Outfall PRE w routing	4.77
100Y008H	Outfall	7.08
100Y008H	Outfall PRE w routing	6.58
100Y024H	Outfall	9.23
100Y024H	Outfall PRE w routing	8.84
100Y072H	Outfall	0.79
100Y072H	Outfall PRE w routing	0.55
100Y168H	Outfall	0.08
100Y168H	Outfall PRE w routing	0.05
100Y240H	Outfall	0.02
100Y240H	Outfall PRE w routing	0.01

ATTACHMENT 6 - Pre-Post Stage Elevations for South Wetlands and Volume Report

1D Nodes - Max

1

Sim	Node Name	Maximum Stage [ft]
002Y001H	South Wetland	2.01
002Y001H	Wetland PRE	2.01
002Y002H	South Wetland	2.01
002Y002H	Wetland PRE	2.01
002Y004H	South Wetland	2.02
002Y004H	Wetland PRE	2.01
002Y008H	South Wetland	2.02
002Y008H	Wetland PRE	2.01
002Y024H	South Wetland	2.00
002Y024H	Wetland PRE	2.00
002Y072H	South Wetland	2.00
002Y072H	Wetland PRE	2.00
002Y168H	South Wetland	2.00
002Y168H	Wetland PRE	2.00
002Y240H	South Wetland	2.00
002Y240H	Wetland PRE	2.00
005Y001H	South Wetland	2.02
005Y001H	Wetland PRE	2.01
005Y002H	South Wetland	2.02
005Y002H	Wetland PRE	2.01
005Y004H	South Wetland	2.02
005Y004H	Wetland PRE	2.01
005Y008H	South Wetland	2.02
005Y008H	Wetland PRE	2.01
005Y024H	South Wetland	2.01
005Y024H	Wetland PRE	2.01
005Y072H	South Wetland	2.00
005Y072H	Wetland PRE	2.00
005Y168H	South Wetland	2.00
005Y168H	Wetland PRE	2.00
005Y240H	South Wetland	2.00
005Y240H	Wetland PRE	2.00
010Y001H	South Wetland	2.02
010Y001H	Wetland PRE	2.01
010Y002H	South Wetland	2.02
010Y002H	Wetland PRE	2.01
010Y004H	South Wetland	2.05
010Y004H	Wetland PRE	2.03
010Y008H	South Wetland	2.03
010Y008H	Wetland PRE	2.02
010Y024H	South Wetland	2.04
010Y024H	Wetland PRE	2.04

Sim	Node Name	Maximum Stage [ft]
010Y072H	South Wetland	2.00
010Y072H	Wetland PRE	2.00
010Y168H	South Wetland	2.00
010Y168H	Wetland PRE	2.00
010Y240H	South Wetland	2.00
010Y240H	Wetland PRE	2.00
025Y001H	South Wetland	2.03
025Y001H	Wetland PRE	2.02
025Y002H	South Wetland	2.03
025Y002H	Wetland PRE	2.02
025Y004H	South Wetland	2.05
025Y004H	Wetland PRE	2.03
025Y008H	South Wetland	2.07
025Y008H	Wetland PRE	2.06
025Y024H	South Wetland	2.13
025Y024H	Wetland PRE	2.11
025Y072H	South Wetland	2.00
025Y072H	Wetland PRE	2.00
025Y168H	South Wetland	2.00
025Y168H	Wetland PRE	2.00
025Y240H	South Wetland	2.00
025Y240H	Wetland PRE	2.00
050Y001H	South Wetland	2.04
050Y001H	Wetland PRE	2.02
050Y002H	South Wetland	2.04
050Y002H	Wetland PRE	2.03
050Y004H	South Wetland	2.09
050Y004H	Wetland PRE	2.06
050Y008H	South Wetland	2.14
050Y008H	Wetland PRE	2.12
050Y024H	South Wetland	2.23
050Y024H	Wetland PRE	2.21
050Y072H	South Wetland	2.00
050Y072H	Wetland PRE	2.00
050Y168H	South Wetland	2.00
050Y168H	Wetland PRE	2.00
050Y240H	South Wetland	2.00
050Y240H	Wetland PRE	2.00
100Y001H	South Wetland	2.05
100Y001H	Wetland PRE	2.03
100Y002H	South Wetland	2.06
100Y002H	Wetland PRE	2.04

Sim	Node Name	Maximum Stage [ft]
100Y004H	South Wetland	2.14
100Y004H	Wetland PRE	2.12
100Y008H	South Wetland	2.24
100Y008H	Wetland PRE	2.21
100Y024H	South Wetland	2.38
100Y024H	Wetland PRE	2.35
100Y072H	South Wetland	2.00
100Y072H	Wetland PRE	2.00
100Y168H	South Wetland	2.00
100Y168H	Wetland PRE	2.00
100Y240H	South Wetland	2.00
100Y240H	Wetland PRE	2.00

Most critical storms
with a 0.03' difference

Discharge Volume Report

1D Nodes - Volume

1

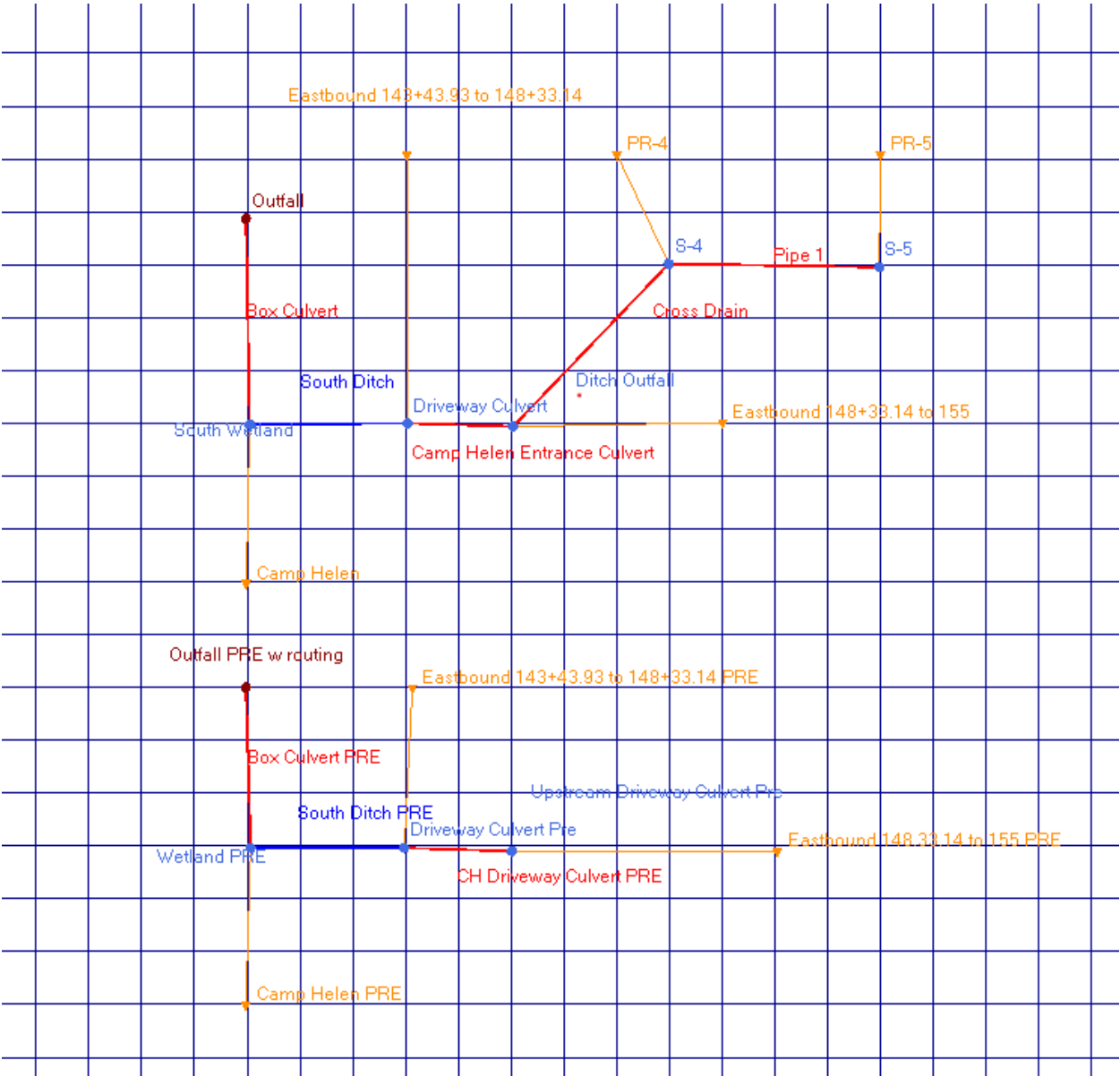
Sim	Node Name	Total Inflow Volume [ft3]
002Y001H	Outfall	6414
002Y001H	Outfall PRE w routing	3985
002Y002H	Outfall	10227
002Y002H	Outfall PRE w routing	6511
002Y004H	Outfall	15590
002Y004H	Outfall PRE w routing	10191
002Y008H	Outfall	20393
002Y008H	Outfall PRE w routing	13552
002Y024H	Outfall	33578
002Y024H	Outfall PRE w routing	23918
002Y072H	Outfall	69014
002Y072H	Outfall PRE w routing	55766
002Y168H	Outfall	118148
002Y168H	Outfall PRE w routing	101549
002Y240H	Outfall	160483
002Y240H	Outfall PRE w routing	141524
005Y001H	Outfall	9269
005Y001H	Outfall PRE w routing	5859
005Y002H	Outfall	14272
005Y002H	Outfall PRE w routing	9270
005Y004H	Outfall	19977
005Y004H	Outfall PRE w routing	13261
005Y008H	Outfall	28894
005Y008H	Outfall PRE w routing	19964
005Y024H	Outfall	70648
005Y024H	Outfall PRE w routing	57273
005Y072H	Outfall	141646
005Y072H	Outfall PRE w routing	123693
005Y168H	Outfall	221564
005Y168H	Outfall PRE w routing	199630
005Y240H	Outfall	283596
005Y240H	Outfall PRE w routing	258963
010Y001H	Outfall	11927
010Y001H	Outfall PRE w routing	7654
010Y002H	Outfall	18078
010Y002H	Outfall PRE w routing	11918
010Y004H	Outfall	41456
010Y004H	Outfall PRE w routing	30806
010Y008H	Outfall	44952
010Y008H	Outfall PRE w routing	33904
010Y024H	Outfall	123481
010Y024H	Outfall PRE w routing	106569

Sim	Node Name	Total Inflow Volume [ft3]
010Y072H	Outfall	233454
010Y072H	Outfall PRE w routing	210981
010Y168H	Outfall	344593
010Y168H	Outfall PRE w routing	317524
010Y240H	Outfall	417588
010Y240H	Outfall PRE w routing	387797
025Y001H	Outfall	15998
025Y001H	Outfall PRE w routing	10457
025Y002H	Outfall	23908
025Y002H	Outfall PRE w routing	16045
025Y004H	Outfall	41456
025Y004H	Outfall PRE w routing	30806
025Y008H	Outfall	84487
025Y008H	Outfall PRE w routing	70087
025Y024H	Outfall	233429
025Y024H	Outfall PRE w routing	210960
025Y072H	Outfall	417569
025Y072H	Outfall PRE w routing	387779
025Y168H	Outfall	569501
025Y168H	Outfall PRE w routing	534512
025Y240H	Outfall	673356
025Y240H	Outfall PRE w routing	635076
050Y001H	Outfall	19434
050Y001H	Outfall PRE w routing	12863
050Y002H	Outfall	31218
050Y002H	Outfall PRE w routing	21917
050Y004H	Outfall	62563
050Y004H	Outfall PRE w routing	49867
050Y008H	Outfall	130609
050Y008H	Outfall PRE w routing	113296
050Y024H	Outfall	344571
050Y024H	Outfall PRE w routing	317505
050Y072H	Outfall	611769
050Y072H	Outfall PRE w routing	575543
050Y168H	Outfall	801002
050Y168H	Outfall PRE w routing	758906
050Y240H	Outfall	915831
050Y240H	Outfall PRE w routing	870433
100Y001H	Outfall	23135
100Y001H	Outfall PRE w routing	15482
100Y002H	Outfall	42930
100Y002H	Outfall PRE w routing	32121

Sim	Node Name	Total Inflow Volume [ft3]
100Y004H	Outfall	92311
100Y004H	Outfall PRE w routing	77379
100Y008H	Outfall	192105
100Y008H	Outfall PRE w routing	171589
100Y024H	Outfall	487171
100Y024H	Outfall PRE w routing	455009
100Y072H	Outfall	838546
100Y072H	Outfall PRE w routing	795402
100Y168H	Outfall	1075540
100Y168H	Outfall PRE w routing	1025720
100Y240H	Outfall	1199816
100Y240H	Outfall PRE w routing	1146683

ATTACHMENT 7 - CN Calculations, Input Report & Rainfall Data

StormWise Model Graphic



Approved
2024-D-391-00036
Lisa Ward
1/16/2025

POST DRAINAGE BASINS

Remarks

STA.143+00 to STA. 145+60	Area (sf)	Area (ac)	CN	CN * A	Weighted 'CN'
Impervious	7,933	0.18	98	777,434.0	53.25
Pervious	6,666	0.15	30	199,980.0	13.70
Total	14,599	0.34		977,414.0	66.95

PR-1

STA 145+60 to STA 148+61	Area (sf)	Area (ac)	CN	CN * A	Weighted 'CN'
Impervious	8,803	0.20	98	862,694.0	53.84
Pervious	7,219	0.17	30	216,570.0	13.52
Total	16,022	0.37		1,079,264.0	67.36

PR-2

STA. 148+61 to STA. 150+07	Area (sf)	Area (ac)	CN	CN * A	Weighted 'CN'
Impervious	11,280	0.26	98	1,105,440.0	81.77
Pervious	2,238	0.05	30	67,143.0	4.97
Total	13,518	0.31		1,172,583.0	86.74

PR-3

STA. 150+07 to STA. 151+31	Area (sf)	Area (ac)	CN	CN * A	Weighted 'CN'
Impervious	7363	0.17	98	721,574.0	69.37
Pervious	3039	0.07	30	91,170.0	8.76
Total	10,402	0.24		812,744.0	78.13

PR-4

STA. 151+31 to STA. 153+28	Area (sf)	Area (ac)	CN	CN * A	Weighted 'CN'
Impervious	12823	0.30	98	1,256,654.0	72.35
Pervious	4546	0.10	30	136,380.0	7.85
Total	17,369	0.40		1,393,034.0	80.20

PR-5

STA. 153+28 to STA. 155+74	Area (sf)	Area (ac)	CN	CN * A	Weighted 'CN'
Impervious	9139	0.30	98	895,622.0	60.25
Pervious	5725	0.13	30	171,750.0	11.55
Total	14,864	0.43		1,067,372.0	71.81

PR-6

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

STA. 142+99 to STA. 148+55	Area (sf)	Area (ac)	CN	CN * A	Weighted 'CN'
Impervious	5712	0.30	98	559,776.0	98.00
Pervious	0	0.00	30	0.0	0.00
Total	5,712	0.30		559,776.0	98.00

PR-7
Left Turn Lane

STA. 148+52 to STA. 149+27	Area (sf)	Area (ac)	CN	CN * A	Weighted 'CN'
Impervious	1026	0.30	98	100,548.0	98.00
Pervious	0	0.00	30	0.0	0.00
Total	1,026	0.30		100,548.0	98.00

PR-8

STA. 143+43.93 to STA. 148+33.14	Area (sf)	Area (ac)	CN	CN * A	Weighted 'CN'
Impervious	41561.08	0.95	98	4,072,985.8	81.95
Pervious	8139.622	0.19	30	244,188.6	4.91
Total	49,701	1.14		4,317,174.5	86.86

ADDITIONAL SUB-BASIN PR-7
PLUS FDOT Basin 143+43.93 to
148+33.14 FROM PROJECT ID
437759-1-52-01

STA. 148+33.14 to 155+0.00	Area (sf)	Area (ac)	CN	CN * A	Weighted 'CN'
Impervious	24829.2	0.57	98	2,433,261.6	33.05
Pervious	48787.2	1.12	30	1,463,616.0	19.88
Total	73,616	1.69		3,896,877.6	52.93

FROM FDOT DRAINAGE
DESIGN MANUAL PROJECT ID
437759-1-52-01

Approved
2024-D-391-00036
Lisa Ward
1/16/2025

Simple Basin: Camp Helen

Scenario: Scenario1
Node: South Wetland
Hydrograph Method: NRCS Unit Hydrograph
Infiltration Method: Curve Number
Time of Concentration: 26.0000 min
Max Allowable Q: 0.00 cfs
Time Shift: 0.0000 hr
Unit Hydrograph: UH323
Peaking Factor: 323.0
Area: 38.6100 ac
Curve Number: 30.0
Ia/S: 0.00
% Impervious: 0.00
% DCIA: 0.00
% Direct: 0.00
Rainfall Name:

Comment: sandy soils" from FDOT project drainage report area

Simple Basin: Camp Helen PRE

Scenario: Scenario1
Node: Wetland PRE
Hydrograph Method: NRCS Unit Hydrograph
Infiltration Method: Curve Number
Time of Concentration: 26.0000 min
Max Allowable Q: 0.00 cfs
Time Shift: 0.0000 hr
Unit Hydrograph: UH323
Peaking Factor: 323.0
Area: 38.6100 ac
Curve Number: 30.0
Ia/S: 0.00
% Impervious: 0.00
% DCIA: 0.00
% Direct: 0.00
Rainfall Name:

Comment:

Simple Basin: Eastbound 143+43.93 to 148+33.14

Scenario: Scenario1
Node: Driveway Culvert
Hydrograph Method: NRCS Unit Hydrograph
Infiltration Method: Curve Number

Time of Concentration: 10.0000 min
Max Allowable Q: 0.00 cfs
Time Shift: 0.0000 hr
Unit Hydrograph: UH323
Peaking Factor: 323.0
Area: 1.1400 ac
Curve Number: 86.9
Ia/S: 0.00
% Impervious: 0.00
% DCIA: 0.00
% Direct: 0.00
Rainfall Name:

Comment:

Simple Basin: Eastbound 143+43.93 to 148+33.14 PRE

Scenario: Scenario1
Node: Driveway Culvert Pre
Hydrograph Method: NRCS Unit Hydrograph
Infiltration Method: Curve Number
Time of Concentration: 10.0000 min
Max Allowable Q: 0.00 cfs
Time Shift: 0.0000 hr
Unit Hydrograph: UH323
Peaking Factor: 323.0
Area: 1.0100 ac
Curve Number: 85.9
Ia/S: 0.00
% Impervious: 0.00
% DCIA: 0.00
% Direct: 0.00
Rainfall Name:

Comment:

Simple Basin: Eastbound 148+33.14 to 155

Scenario: Scenario1
Node: Ditch Outfall
Hydrograph Method: NRCS Unit Hydrograph
Infiltration Method: Curve Number
Time of Concentration: 10.0000 min
Max Allowable Q: 0.00 cfs
Time Shift: 0.0000 hr
Unit Hydrograph: UH323
Peaking Factor: 323.0

Area: 1.6900 ac
Curve Number: 52.8
Ia/S: 0.00
% Impervious: 0.00
% DCIA: 0.00
% Direct: 0.00
Rainfall Name:

Comment:

Simple Basin: Eastbound 148.33.14 to 155 PRE

Scenario: Scenario1
Node: Upstream Driveway Culvert Pre
Hydrograph Method: NRCS Unit Hydrograph
Infiltration Method: Curve Number
Time of Concentration: 10.0000 min
Max Allowable Q: 0.00 cfs
Time Shift: 0.0000 hr
Unit Hydrograph: UH323
Peaking Factor: 323.0
Area: 1.6900 ac
Curve Number: 52.9
Ia/S: 0.00
% Impervious: 0.00
% DCIA: 0.00
% Direct: 0.00
Rainfall Name:

Comment:

Simple Basin: PR-4

Scenario: Scenario1
Node: S-4
Hydrograph Method: NRCS Unit Hydrograph
Infiltration Method: Curve Number
Time of Concentration: 8.0000 min
Max Allowable Q: 0.00 cfs
Time Shift: 0.0000 hr
Unit Hydrograph: UH323
Peaking Factor: 323.0
Area: 0.2400 ac
Curve Number: 78.1
Ia/S: 0.00
% Impervious: 0.00
% DCIA: 0.00

% Direct: 0.00
Rainfall Name:

Comment:

Simple Basin: PR-5

Scenario: Scenario1
Node: S-5
Hydrograph Method: NRCS Unit Hydrograph
Infiltration Method: Curve Number
Time of Concentration: 8.0000 min
Max Allowable Q: 0.00 cfs
Time Shift: 0.0000 hr
Unit Hydrograph: UH323
Peaking Factor: 323.0
Area: 0.4000 ac
Curve Number: 80.2
Ia/S: 0.00
% Impervious: 0.00
% DCIA: 0.00
% Direct: 0.00
Rainfall Name:

Comment:

Node: Ditch Outfall

Scenario: Scenario1
Type: Stage/Area
Base Flow: 0.00 cfs
Initial Stage: 5.95 ft
Warning Stage: 9.00 ft
Alert Stage: 0.00 ft

Comment:

Node: Driveway Culvert

Scenario: Scenario1
Type: Stage/Area
Base Flow: 0.00 cfs
Initial Stage: 4.92 ft
Warning Stage: 8.00 ft

Alert Stage: 0.00 ft

Comment:

Node: Driveway Culvert Pre

Scenario: Scenario1
Type: Stage/Area
Base Flow: 0.00 cfs
Initial Stage: 4.92 ft
Warning Stage: 8.00 ft
Alert Stage: 0.00 ft

Comment:

Node: Outfall

Scenario: Scenario1
Type: Time/Stage
Base Flow: 0.00 cfs
Initial Stage: 2.00 ft
Warning Stage: 0.00 ft
Alert Stage: 0.00 ft
Boundary Stage:

Comment:

Node: Outfall PRE w routing

Scenario: Scenario1
Type: Time/Stage
Base Flow: 0.00 cfs
Initial Stage: 2.00 ft
Warning Stage: 0.00 ft
Alert Stage: 0.00 ft
Boundary Stage:

Comment:

Node: S-4

Scenario: Scenario1
 Type: Stage/Area
 Base Flow: 0.00 cfs
 Initial Stage: 8.50 ft
 Warning Stage: 12.62 ft
 Alert Stage: 0.00 ft

Comment:

Node: S-5

Scenario: Scenario1
 Type: Stage/Area
 Base Flow: 0.00 cfs
 Initial Stage: 9.75 ft
 Warning Stage: 13.90 ft
 Alert Stage: 0.00 ft

Comment:

Node: South Wetland

Scenario: Scenario1
 Type: Stage/Area
 Base Flow: 0.00 cfs
 Initial Stage: 2.00 ft
 Warning Stage: 6.00 ft
 Alert Stage: 0.00 ft

Stage [ft]	Area [ac]	Area [ft2]
2.00	8.0526	350770
3.00	9.0148	392684
4.00	10.6869	465522
5.00	13.4741	586930
6.00	15.5203	676064

Comment:

Node: Upstream Driveway Culvert Pre

Scenario: Scenario1
 Type: Stage/Area

Base Flow: 0.00 cfs
 Initial Stage: 5.95 ft
 Warning Stage: 9.00 ft
 Alert Stage: 0.00 ft

Comment:

Node: Wetland PRE

Scenario: Scenario1
 Type: Stage/Area
 Base Flow: 0.00 cfs
 Initial Stage: 2.00 ft
 Warning Stage: 0.00 ft
 Alert Stage: 0.00 ft

Stage [ft]	Area [ac]	Area [ft2]
2.00	8.0526	350770
3.00	9.0148	392684
4.00	10.6869	465522
5.00	13.4741	586930
6.00	15.5203	676064

Comment:

Pipe Link: Box Culvert

Scenario: Scenario1
 From Node: South Wetland
 To Node: Outfall
 Link Count: 1
 Flow Direction: Both
 Damping: 0.0000 ft
 Length: 193.00 ft
 FHWA Code: 11
 Entr Loss Coef: 0.00
 Exit Loss Coef: 1.00
 Bend Loss Coef: 0.00
 Bend Location: 0.00 dec
 Energy Switch: Energy

Upstream

Invert: 1.15 ft
 Manning's N: 0.0160

Geometry: Rectangular

Max Depth: 3.00 ft
 Max Width: 3.50 ft
 Fillet: 0.00 ft

Bottom Clip

Default: 0.00 ft
 Op Table:
 Ref Node:
 Manning's N: 0.0000

Top Clip

Default: 0.00 ft
 Op Table:
 Ref Node:
 Manning's N: 0.0000

Downstream

Invert: 1.04 ft
 Manning's N: 0.0160

Geometry: Rectangular

Max Depth: 3.00 ft
 Max Width: 3.50 ft
 Fillet: 0.00 ft

Default: 0.00 ft

Op Table:

Ref Node:

Manning's N: 0.0000

Default: 0.00 ft

Op Table:

Ref Node:

Manning's N: 0.0000

Comment:

Pipe Link: Box Culvert PRE		Upstream	Downstream
Scenario:	Scenario1	Invert: 1.15 ft	Invert: 1.04 ft
From Node:	Wetland PRE	Manning's N: 0.0160	Manning's N: 0.0160
To Node:	Outfall PRE w routing	Geometry: Rectangular	Geometry: Rectangular
Link Count:	1	Max Depth: 3.00 ft	Max Depth: 3.00 ft
Flow Direction:	Both	Max Width: 3.50 ft	Max Width: 3.50 ft
Damping:	0.0000 ft	Fillet: 0.00 ft	Fillet: 0.00 ft
Length:	193.00 ft	Bottom Clip	
FHWA Code:	11	Default: 0.00 ft	Default: 0.00 ft
Entr Loss Coef:	0.00	Op Table:	Op Table:
Exit Loss Coef:	1.00	Ref Node:	Ref Node:
Bend Loss Coef:	0.00	Manning's N: 0.0000	Manning's N: 0.0000
Bend Location:	0.00 dec	Top Clip	
Energy Switch:	Energy	Default: 0.00 ft	Default: 0.00 ft
		Op Table:	Op Table:
		Ref Node:	Ref Node:
		Manning's N: 0.0000	Manning's N: 0.0000
Comment:			

Pipe Link: Camp Helen Entrance Culvert		Upstream	Downstream
Scenario:	Scenario1	Invert: 5.95 ft	Invert: 4.92 ft
From Node:	Ditch Outfall	Manning's N: 0.0130	Manning's N: 0.0130
To Node:	Driveway Culvert	Geometry: Horizontal Ellipse	Geometry: Horizontal Ellipse
Link Count:	1	Max Depth: 1.17 ft	Max Depth: 1.17 ft
Flow Direction:	Both	Bottom Clip	
Damping:	0.0000 ft	Default: 0.00 ft	Default: 0.00 ft
Length:	74.50 ft	Op Table:	Op Table:
FHWA Code:	0	Ref Node:	Ref Node:
Entr Loss Coef:	0.03	Manning's N: 0.0000	Manning's N: 0.0000
Exit Loss Coef:	0.70	Top Clip	
Bend Loss Coef:	0.00	Default: 0.00 ft	Default: 0.00 ft
Bend Location:	0.00 dec	Op Table:	Op Table:
Energy Switch:	Energy	Ref Node:	Ref Node:
		Manning's N: 0.0000	Manning's N: 0.0000
Comment:			

Pipe Link: CH Driveway Culvert PRE		Upstream	Downstream
Scenario:	Scenario1	Invert: 5.95 ft	Invert: 4.92 ft
From Node:	Upstream Driveway Culvert Pre	Manning's N: 0.0130	Manning's N: 0.0130
To Node:	Driveway Culvert Pre	Geometry: Horizontal Ellipse	Geometry: Horizontal Ellipse
Link Count:	1	Max Depth: 1.17 ft	Max Depth: 1.17 ft
Flow Direction:	Both	Bottom Clip	
Damping:	0.0000 ft	Default: 0.00 ft	Default: 0.00 ft
		Op Table:	Op Table:
		Ref Node:	Ref Node:

Length:	74.50 ft	Manning's N:	0.0000	Manning's N:	0.0000
FHWA Code:	0	Top Clip			
Entr Loss Coef:	0.03	Default:	0.00 ft	Default:	0.00 ft
Exit Loss Coef:	0.70	Op Table:		Op Table:	
Bend Loss Coef:	0.00	Ref Node:		Ref Node:	
Bend Location:	0.00 dec	Manning's N:	0.0000	Manning's N:	0.0000
Energy Switch:	Energy				
Comment:					

Pipe Link: Cross Drain		Upstream		Downstream	
Scenario:	Scenario1	Invert:	8.50 ft	Invert:	6.92 ft
From Node:	S-4	Manning's N:	0.0130	Manning's N:	0.0130
To Node:	Ditch Outfall	Geometry: Horizontal Ellipse		Geometry: Horizontal Ellipse	
Link Count:	1	Max Depth:	1.17 ft	Max Depth:	1.17 ft
Flow Direction:	Both	Bottom Clip			
Damping:	0.0000 ft	Default:	0.00 ft	Default:	0.00 ft
Length:	72.50 ft	Op Table:		Op Table:	
FHWA Code:	0	Ref Node:		Ref Node:	
Entr Loss Coef:	0.00	Manning's N:	0.0000	Manning's N:	0.0000
Exit Loss Coef:	0.50	Top Clip			
Bend Loss Coef:	0.00	Default:	0.00 ft	Default:	0.00 ft
Bend Location:	0.00 dec	Op Table:		Op Table:	
Energy Switch:	Energy	Ref Node:		Ref Node:	
		Manning's N:	0.0000	Manning's N:	0.0000
Comment:					

Pipe Link: Pipe 1		Upstream		Downstream	
Scenario:	Scenario1	Invert:	9.75 ft	Invert:	8.51 ft
From Node:	S-5	Manning's N:	0.0120	Manning's N:	0.0120
To Node:	S-4	Geometry: Circular		Geometry: Circular	
Link Count:	1	Max Depth:	1.50 ft	Max Depth:	1.50 ft
Flow Direction:	Both	Bottom Clip			
Damping:	0.0000 ft	Default:	0.00 ft	Default:	0.00 ft
Length:	120.00 ft	Op Table:		Op Table:	
FHWA Code:	0	Ref Node:		Ref Node:	
Entr Loss Coef:	0.20	Manning's N:	0.0000	Manning's N:	0.0000
Exit Loss Coef:	0.00	Top Clip			
Bend Loss Coef:	0.00	Default:	0.00 ft	Default:	0.00 ft
Bend Location:	0.00 dec	Op Table:		Op Table:	
Energy Switch:	Energy	Ref Node:		Ref Node:	
		Manning's N:	0.0000	Manning's N:	0.0000
Comment:					

Channel Link: South Ditch		Upstream	Downstream
Scenario:	Scenario1	Invert: 4.92 ft	Invert: 2.32 ft
From Node:	Driveway Culvert	Manning's N: 0.0350	Manning's N: 0.0350
To Node:	South Wetland	Geometry: Trapezoidal	Geometry: Trapezoidal
Link Count:	1	Max Depth: 3.30 ft	Max Depth: 3.30 ft
Flow Direction:	Both	Extrapolation: Normal	Extrapolation: Normal
Damping:	0.0000 ft	Bottom Width: 5.00 ft	Bottom Width: 5.00 ft
Length:	439.00 ft	Left Slope: 4.000 (h:v)	Left Slope: 4.000 (h:v)
Contraction Coef:	0.00	Right Slope: 3.000 (h:v)	Right Slope: 3.000 (h:v)
Expansion Coef:	0.00	Bottom Clip	
Entr Loss Coef:	0.00	Default: 0.00 ft	Default: 0.00 ft
Exit Loss Coef:	1.00	Op Table:	Op Table:
Bend Loss Coef:	0.00	Ref Node:	Ref Node:
Bend Location:	0.00 dec	Manning's N: 0.0000	Manning's N: 0.0000
Energy Switch:	Energy	Top Clip	
		Default: 0.00 ft	Default: 0.00 ft
		Op Table:	Op Table:
		Ref Node:	Ref Node:
		Manning's N: 0.0000	Manning's N: 0.0000
Comment:			

Channel Link: South Ditch PRE		Upstream	Downstream
Scenario:	Scenario1	Invert: 4.92 ft	Invert: 2.32 ft
From Node:	Driveway Culvert	Manning's N: 0.0350	Manning's N: 0.0350
	Pre	Geometry: Trapezoidal	Geometry: Trapezoidal
To Node:	Wetland PRE	Max Depth: 3.30 ft	Max Depth: 3.30 ft
Link Count:	1	Extrapolation: Normal	Extrapolation: Normal
Flow Direction:	Both	Bottom Width: 5.00 ft	Bottom Width: 5.00 ft
Damping:	0.0000 ft	Left Slope: 4.000 (h:v)	Left Slope: 4.000 (h:v)
Length:	439.00 ft	Right Slope: 3.000 (h:v)	Right Slope: 3.000 (h:v)
Contraction Coef:	0.00	Bottom Clip	
Expansion Coef:	0.00	Default: 0.00 ft	Default: 0.00 ft
Entr Loss Coef:	0.00	Op Table:	Op Table:
Exit Loss Coef:	1.00	Ref Node:	Ref Node:
Bend Loss Coef:	0.00	Manning's N: 0.0000	Manning's N: 0.0000
Bend Location:	0.00 dec	Top Clip	
Energy Switch:	Energy	Default: 0.00 ft	Default: 0.00 ft
		Op Table:	Op Table:
		Ref Node:	Ref Node:
		Manning's N: 0.0000	Manning's N: 0.0000
Comment:			

Simulation: 002Y001H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:30:06 PM

Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	6.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
Extern Hydrograph Set:
Curve Number Set: 1

Green-Ampt Set:
Vertical Layers Set:
Impervious Set: 1

Tolerances & Options

Time Marching: SAOR	IA Recovery Time: 24.0000 hr
Max Iterations: 6	
Over-Relax Weight: 0.5 dec	Ia/S: 0.20 dec
Fact:	
dZ Tolerance: 0.0010 ft	
Max dZ: 1.0000 ft	Smp/Man Basin Rain: Global
	Opt:
Link Optimizer Tol: 0.0001 ft	

Rainfall Name: ~FDOT-1
 Rainfall Amount: 2.30 in
 Storm Duration: 1.0000 hr
 Dflt Damping (1D): 0.0050 ft
 Min Node Srf Area 100 ft2
 (1D):
 Energy Switch (1D): Energy

Comment: 100 yr / 001 hr

Simulation: 002Y002H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:30:07 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	8.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:

Unit Hydrograph
Folder:

Curve Number Set: 1

Green-Ampt Set:
Vertical Layers Set:
Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
Max Iterations: 6
Over-Relax Weight 0.5 dec
Fact:
dZ Tolerance: 0.0010 ft
Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-2
Rainfall Amount: 2.92 in
Storm Duration: 2.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 002 hr

Simulation: 002Y004H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:30:09 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	12.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-4

Rainfall Amount: 3.67 in

Storm Duration: 4.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2

(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 004 hr

Simulation: 002Y008H

Scenario: Scenario1

Run Date/Time: 11/18/2024 4:30:11 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	16.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

 Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight: 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft
 Max dZ: 1.0000 ft

IA Recovery Time: 24.0000 hr

 Ia/S: 0.20 dec

 Smp/Man Basin Rain: Global
 Opt:

Link Optimizer Tol: 0.0001 ft

Rainfall Name: ~FDOT-8
 Rainfall Amount: 4.28 in
 Storm Duration: 8.0000 hr
 Dflt Damping (1D): 0.0050 ft
 Min Node Srf Area 100 ft2
 (1D):
 Energy Switch (1D): Energy

Comment: 100 yr / 008 hr

Simulation: 002Y024H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:30:14 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	36.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Lookup Tables

Rainfall Folder:

Unit Hydrograph
Folder:

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight: 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft
 Max dZ: 1.0000 ft
 Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain: Global
 Opt:

Rainfall Name: ~FDOT-24
 Rainfall Amount: 5.42 in
 Storm Duration: 24.0000 hr
 Dflt Damping (1D): 0.0050 ft
 Min Node Srf Area: 100 ft2
 (1D):
 Energy Switch (1D): Energy

Comment: 100 yr / 024 hr

Simulation: 002Y072H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:30:21 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	84.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-72

Rainfall Amount: 6.82 in

Storm Duration: 72.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2

(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 072 hr

Simulation: 002Y168H

Scenario: Scenario1

Run Date/Time: 11/18/2024 4:30:44 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	180.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft
 Max dZ: 1.0000 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
 Opt:

Link Optimizer Tol: 0.0001 ft

Rainfall Name: ~FDOT-168
 Rainfall Amount: 8.10 in
 Storm Duration: 168.0000 hr
 Dflt Damping (1D): 0.0050 ft
 Min Node Srf Area 100 ft2
 (1D):
 Energy Switch (1D): Energy

Comment: 100 yr / 168 hr

Simulation: 002Y240H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:31:40 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	252.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources	Lookup Tables
Rainfall Folder:	Boundary Stage Set:
Unit Hydrograph Folder:	Extern Hydrograph Set:
	Curve Number Set: 1
	Green-Ampt Set:
	Vertical Layers Set:
	Impervious Set: 1

Tolerances & Options	
Time Marching: SAOR	IA Recovery Time: 24.0000 hr
Max Iterations: 6	
Over-Relax Weight: 0.5 dec	Ia/S: 0.20 dec
Fact:	
dZ Tolerance: 0.0010 ft	
Max dZ: 1.0000 ft	Smp/Man Basin Rain: Global
	Opt:
Link Optimizer Tol: 0.0001 ft	
	Rainfall Name: ~FDOT-240
	Rainfall Amount: 8.99 in
	Storm Duration: 240.0000 hr
	Dflt Damping (1D): 0.0050 ft
	Min Node Srf Area: 100 ft2
	(1D):
	Energy Switch (1D): Energy

Comment: 100 yr / 240 hr

Simulation: 005Y001H				
Scenario:	Scenario1			
Run Date/Time:	11/18/2024 4:32:55 PM			
Program Version:	StormWise 4.08.01			

General				
Run Mode:	Normal			
	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	6.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		
Max Calculation Time:		60.0000		

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-1

Rainfall Amount: 2.78 in

Storm Duration: 1.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2
(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 001 hr

Simulation: 005Y002H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:32:56 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	8.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight: 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft
 Max dZ: 1.0000 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec
 Smp/Man Basin Rain: Global

Link Optimizer Tol: 0.0001 ft

Opt:

Rainfall Name: ~FDOT-2
 Rainfall Amount: 3.50 in
 Storm Duration: 2.0000 hr
 Dflt Damping (1D): 0.0050 ft
 Min Node Srf Area 100 ft2
 (1D):
 Energy Switch (1D): Energy

Comment: 100 yr / 002 hr

Simulation: 005Y004H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:32:58 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	12.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources	Lookup Tables
Rainfall Folder:	Boundary Stage Set:
Unit Hydrograph Folder:	Extern Hydrograph Set:
	Curve Number Set: 1
	Green-Ampt Set:
	Vertical Layers Set:
	Impervious Set: 1

Tolerances & Options			
Time Marching:	SAOR	IA Recovery Time:	24.0000 hr
Max Iterations:	6		
Over-Relax Weight	0.5 dec	Ia/S:	0.20 dec
Fact:			
dZ Tolerance:	0.0010 ft		
Max dZ:	1.0000 ft	Smp/Man Basin Rain	Global
		Opt:	
Link Optimizer Tol:	0.0001 ft		
		Rainfall Name:	~FDOT-4
		Rainfall Amount:	4.23 in
		Storm Duration:	4.0000 hr
		Dflt Damping (1D):	0.0050 ft
		Min Node Srf Area	100 ft2
		(1D):	
		Energy Switch (1D):	Energy

Comment: 100 yr / 004 hr

Simulation: 005Y008H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:33:02 PM
Program Version: StormWise 4.08.01

General				
Run Mode:		Normal		
	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	16.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		
Max Calculation Time:	60.0000			

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-8

Rainfall Amount: 5.13 in

Storm Duration: 8.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2

(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 008 hr

Simulation: 005Y024H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:33:09 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	36.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec

Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-24
Rainfall Amount: 6.87 in
Storm Duration: 24.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 024 hr

Simulation: 005Y072H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:33:19 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	84.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources	Lookup Tables
Rainfall Folder:	Boundary Stage Set:
Unit Hydrograph Folder:	Extern Hydrograph Set:
	Curve Number Set: 1
	Green-Ampt Set:
	Vertical Layers Set:
	Impervious Set: 1

Tolerances & Options			
Time Marching:	SAOR	IA Recovery Time:	24.0000 hr
Max Iterations:	6		
Over-Relax Weight	0.5 dec	Ia/S:	0.20 dec
Fact:			
dZ Tolerance:	0.0010 ft		
Max dZ:	1.0000 ft	Smp/Man Basin Rain	Global
Link Optimizer Tol:	0.0001 ft	Opt:	
		Rainfall Name:	~FDOT-72
		Rainfall Amount:	8.61 in
		Storm Duration:	72.0000 hr
		Dflt Damping (1D):	0.0050 ft
		Min Node Srf Area	100 ft2
		(1D):	
		Energy Switch (1D):	Energy

Comment: 100 yr / 072 hr

Simulation: 005Y168H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:33:51 PM
Program Version: StormWise 4.08.01

General				
Run Mode:	Normal			
	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	180.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		
Max Calculation Time:		60.0000		

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
Extern Hydrograph Set:
Curve Number Set: 1Green-Ampt Set:
Vertical Layers Set:
Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
Max Iterations: 6
Over-Relax Weight: 0.5 dec
Fact:
dZ Tolerance: 0.0010 ft
Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain: Global
Opt:Rainfall Name: ~FDOT-168
Rainfall Amount: 10.10 in
Storm Duration: 168.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area: 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 168 hr

Simulation: 005Y240H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:35:07 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	252.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec

Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-240
Rainfall Amount: 11.10 in
Storm Duration: 240.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 240 hr

Simulation: 010Y001H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:36:28 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	6.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources		Lookup Tables	
Rainfall Folder:		Boundary Stage Set:	
Unit Hydrograph Folder:		Extern Hydrograph Set:	
		Curve Number Set:	1
		Green-Ampt Set:	
		Vertical Layers Set:	
		Impervious Set:	1

Tolerances & Options			
Time Marching:	SAOR	IA Recovery Time:	24.0000 hr
Max Iterations:	6	Ia/S:	0.20 dec
Over-Relax Weight	0.5 dec		
Fact:			
dZ Tolerance:	0.0010 ft	Smp/Man Basin Rain	Global
Max dZ:	1.0000 ft	Opt:	
Link Optimizer Tol:	0.0001 ft		
		Rainfall Name:	~FDOT-1
		Rainfall Amount:	3.18 in
		Storm Duration:	1.0000 hr
		Dflt Damping (1D):	0.0050 ft
		Min Node Srf Area	100 ft2
		(1D):	
		Energy Switch (1D):	Energy

Comment: 100 yr / 001 hr

Simulation: 010Y002H				
Scenario:	Scenario1			
Run Date/Time:	11/18/2024 4:36:29 PM			
Program Version:	StormWise 4.08.01			

General				
Run Mode:	Normal			
	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	8.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		
Max Calculation Time:		60.0000		

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-2

Rainfall Amount: 4.00 in

Storm Duration: 2.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2
(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 002 hr

Simulation: 010Y004H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:36:31 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	12.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec

Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-4
Rainfall Amount: 5.82 in
Storm Duration: 4.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 004 hr

Simulation: 010Y008H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:36:35 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	16.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		
Max Calculation Time:		60.0000		

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0001 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-8

Rainfall Amount: 5.97 in

Storm Duration: 8.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2

(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 008 hr

Simulation: 010Y024H

Scenario: Scenario1

Run Date/Time: 11/18/2024 4:36:43 PM

Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	36.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000

Max Calculation Time: 60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
Extern Hydrograph Set:
Curve Number Set: 1

Green-Ampt Set:
Vertical Layers Set:
Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
Max Iterations: 6
Over-Relax Weight: 0.5 dec
Fact:
dZ Tolerance: 0.0010 ft
Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain: Global
Opt:

Rainfall Name: ~FDOT-24
Rainfall Amount: 8.22 in
Storm Duration: 24.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area: 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 024 hr

Simulation: 010Y072H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:36:54 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	84.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec

Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-72
Rainfall Amount: 10.30 in
Storm Duration: 72.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 072 hr

Simulation: 010Y168H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:37:14 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	180.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources	Lookup Tables
Rainfall Folder:	Boundary Stage Set:
Unit Hydrograph Folder:	Extern Hydrograph Set:
	Curve Number Set: 1
	Green-Ampt Set:
	Vertical Layers Set:
	Impervious Set: 1

Tolerances & Options	
Time Marching: SAOR	IA Recovery Time: 24.0000 hr
Max Iterations: 6	
Over-Relax Weight: 0.5 dec	Ia/S: 0.20 dec
Fact:	
dZ Tolerance: 0.0010 ft	
Max dZ: 1.0000 ft	Smp/Man Basin Rain: Global
	Opt:
Link Optimizer Tol: 0.0001 ft	
	Rainfall Name: ~FDOT-168
	Rainfall Amount: 12.00 in
	Storm Duration: 168.0000 hr
	Dflt Damping (1D): 0.0050 ft
	Min Node Srf Area: 100 ft2
	(1D):
	Energy Switch (1D): Energy

Comment: 100 yr / 168 hr

Simulation: 010Y240H				
Scenario:	Scenario1			
Run Date/Time:	11/18/2024 4:37:59 PM			
Program Version:	StormWise 4.08.01			

General				
Run Mode:	Normal			
	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	252.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		

Max Calculation Time: 60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-240

Rainfall Amount: 13.00 in

Storm Duration: 240.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2

(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 240 hr

Simulation: 025Y001H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:39:06 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	6.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec

Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-1
Rainfall Amount: 3.74 in
Storm Duration: 1.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 001 hr

Simulation: 025Y002H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:39:07 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	8.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		
Max Calculation Time:		60.0000		

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources	Lookup Tables
Rainfall Folder:	Boundary Stage Set:
Unit Hydrograph Folder:	Extern Hydrograph Set:
	Curve Number Set: 1
	Green-Ampt Set:
	Vertical Layers Set:
	Impervious Set: 1

Tolerances & Options			
Time Marching:	SAOR	IA Recovery Time:	24.0000 hr
Max Iterations:	6		
Over-Relax Weight	0.5 dec	Ia/S:	0.20 dec
Fact:			
dZ Tolerance:	0.0010 ft	Smp/Man Basin Rain	Global
Max dZ:	1.0000 ft	Opt:	
Link Optimizer Tol:	0.0001 ft		
		Rainfall Name:	~FDOT-2
		Rainfall Amount:	4.71 in
		Storm Duration:	2.0000 hr
		Dflt Damping (1D):	0.0050 ft
		Min Node Srf Area	100 ft2
		(1D):	
		Energy Switch (1D):	Energy

Comment: 100 yr / 002 hr

Simulation: 025Y004H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:39:09 PM
Program Version: StormWise 4.08.01

General				
Run Mode:	Normal			
	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	12.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		
Max Calculation Time:		60.0000		

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-4

Rainfall Amount: 5.82 in

Storm Duration: 4.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2
(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 004 hr

Simulation: 025Y008H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:39:12 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	16.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec

Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-8
Rainfall Amount: 7.27 in
Storm Duration: 8.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 008 hr

Simulation: 025Y024H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:39:16 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	36.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources		Lookup Tables	
Rainfall Folder:		Boundary Stage Set:	
Unit Hydrograph Folder:		Extern Hydrograph Set:	
		Curve Number Set:	1
		Green-Ampt Set:	
		Vertical Layers Set:	
		Impervious Set:	1

Tolerances & Options			
Time Marching:	SAOR	IA Recovery Time:	24.0000 hr
Max Iterations:	6		
Over-Relax Weight:	0.5 dec	Ia/S:	0.20 dec
Fact:			
dZ Tolerance:	0.0010 ft	Smp/Man Basin Rain Opt:	Global
Max dZ:	1.0000 ft		
Link Optimizer Tol:	0.0001 ft		
		Rainfall Name:	~FDOT-24
		Rainfall Amount:	10.30 in
		Storm Duration:	24.0000 hr
		Dflt Damping (1D):	0.0050 ft
		Min Node Srf Area (1D):	100 ft2
		Energy Switch (1D):	Energy

Comment: 100 yr / 024 hr

Simulation: 025Y072H				
Scenario:	Scenario1			
Run Date/Time:	11/18/2024 4:39:27 PM			
Program Version:	StormWise 4.08.01			

General				
Run Mode:	Normal			
	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	84.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		
Max Calculation Time:		60.0000		

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-72

Rainfall Amount: 13.00 in

Storm Duration: 72.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2

(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 072 hr

Simulation: 025Y168H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:41:14 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	180.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec

Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-168
Rainfall Amount: 14.90 in
Storm Duration: 168.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 168 hr

Simulation: 025Y240H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:42:06 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	252.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-240

Rainfall Amount: 16.10 in

Storm Duration: 240.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2

(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 240 hr

Simulation: 050Y001H

Scenario: Scenario1

Run Date/Time: 11/18/2024 4:43:23 PM

Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	6.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000

Max Calculation Time: 60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-1

Rainfall Amount: 4.18 in

Storm Duration: 1.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2

(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 001 hr

Simulation: 050Y002H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:43:25 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	8.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec

Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-2
Rainfall Amount: 5.29 in
Storm Duration: 2.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 002 hr

Simulation: 050Y004H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:43:27 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	12.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources	Lookup Tables
Rainfall Folder:	Boundary Stage Set:
Unit Hydrograph Folder:	Extern Hydrograph Set:
	Curve Number Set: 1
	Green-Ampt Set:
	Vertical Layers Set:
	Impervious Set: 1

Tolerances & Options	
Time Marching: SAOR	IA Recovery Time: 24.0000 hr
Max Iterations: 6	
Over-Relax Weight: 0.5 dec	Ia/S: 0.20 dec
Fact:	
dZ Tolerance: 0.0010 ft	
Max dZ: 1.0000 ft	Smp/Man Basin Rain: Global
	Opt:
Link Optimizer Tol: 0.0001 ft	
	Rainfall Name: ~FDOT-4
	Rainfall Amount: 6.62 in
	Storm Duration: 4.0000 hr
	Dflt Damping (1D): 0.0050 ft
	Min Node Srf Area: 100 ft2
	(1D):
	Energy Switch (1D): Energy

Comment: 100 yr / 004 hr

Simulation: 050Y008H				
Scenario:	Scenario1			
Run Date/Time:	11/18/2024 4:43:32 PM			
Program Version:	StormWise 4.08.01			

General				
Run Mode:	Normal			
	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	16.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		

Max Calculation Time: 60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global

Opt:

Rainfall Name: ~FDOT-8

Rainfall Amount: 8.38 in

Storm Duration: 8.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2

(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 008 hr

Simulation: 050Y024H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:43:38 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	36.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec

Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-24
Rainfall Amount: 12.00 in
Storm Duration: 24.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 024 hr

Simulation: 050Y072H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:43:50 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	84.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources	Lookup Tables
Rainfall Folder:	Boundary Stage Set:
Unit Hydrograph Folder:	Extern Hydrograph Set:
	Curve Number Set: 1
	Green-Ampt Set:
	Vertical Layers Set:
	Impervious Set: 1

Tolerances & Options	
Time Marching: SAOR	IA Recovery Time: 24.0000 hr
Max Iterations: 6	
Over-Relax Weight: 0.5 dec	Ia/S: 0.20 dec
Fact:	
dZ Tolerance: 0.0010 ft	
Max dZ: 1.0000 ft	Smp/Man Basin Rain: Global
	Opt:
Link Optimizer Tol: 0.0001 ft	
	Rainfall Name: ~FDOT-72
	Rainfall Amount: 15.40 in
	Storm Duration: 72.0000 hr
	Dflt Damping (1D): 0.0050 ft
	Min Node Srf Area: 100 ft2
	(1D):
	Energy Switch (1D): Energy

Comment: 100 yr / 072 hr

Simulation: 050Y168H				
Scenario:	Scenario1			
Run Date/Time:	11/18/2024 4:44:19 PM			
Program Version:	StormWise 4.08.01			

General				
Run Mode:	Normal			
	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	180.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		
Max Calculation Time:		60.0000		

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-168

Rainfall Amount: 17.50 in

Storm Duration: 168.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2
(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 168 hr

Simulation: 050Y240H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:45:17 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	252.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec

Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-240
Rainfall Amount: 18.70 in
Storm Duration: 240.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 240 hr

Simulation: 100Y001H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:46:10 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	6.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources	Lookup Tables
Rainfall Folder:	Boundary Stage Set:
Unit Hydrograph Folder:	Extern Hydrograph Set:
	Curve Number Set: 1
	Green-Ampt Set:
	Vertical Layers Set:
	Impervious Set: 1

Tolerances & Options	
Time Marching: SAOR	IA Recovery Time: 24.0000 hr
Max Iterations: 6	
Over-Relax Weight: 0.5 dec	Ia/S: 0.20 dec
Fact:	
dZ Tolerance: 0.0010 ft	
Max dZ: 1.0000 ft	Smp/Man Basin Rain: Global
	Opt:
Link Optimizer Tol: 0.0001 ft	
	Rainfall Name: ~FDOT-1
	Rainfall Amount: 4.63 in
	Storm Duration: 1.0000 hr
	Dflt Damping (1D): 0.0050 ft
	Min Node Srf Area: 100 ft2
	(1D):
	Energy Switch (1D): Energy

Comment: 100 yr / 001 hr

Simulation: 100Y002H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:46:12 PM
Program Version: StormWise 4.08.01

General				
Run Mode:	Normal			
	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	8.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		
Max Calculation Time:		60.0000		

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-2

Rainfall Amount: 5.89 in

Storm Duration: 2.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2
(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 002 hr

Simulation: 100Y004H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:46:15 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	12.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec

Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-4
Rainfall Amount: 7.48 in
Storm Duration: 4.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 004 hr

Simulation: 100Y008H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:46:19 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	16.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-8

Rainfall Amount: 9.59 in

Storm Duration: 8.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2

(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 008 hr

Simulation: 100Y024H

Scenario: Scenario1

Run Date/Time: 11/18/2024 4:46:23 PM

Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	36.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000

Max Calculation Time: 60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-24

Rainfall Amount: 13.90 in

Storm Duration: 24.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2

(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 024 hr

Simulation: 100Y072H

Scenario: Scenario1
 Run Date/Time: 11/18/2024 4:46:38 PM
 Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	84.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:
 Extern Hydrograph Set:
 Curve Number Set: 1

Green-Ampt Set:
 Vertical Layers Set:
 Impervious Set: 1

Tolerances & Options

Time Marching: SAOR
 Max Iterations: 6
 Over-Relax Weight 0.5 dec
 Fact:
 dZ Tolerance: 0.0010 ft

IA Recovery Time: 24.0000 hr
 Ia/S: 0.20 dec

Max dZ: 1.0000 ft
Link Optimizer Tol: 0.0001 ft

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-72
Rainfall Amount: 17.90 in
Storm Duration: 72.0000 hr
Dflt Damping (1D): 0.0050 ft
Min Node Srf Area 100 ft2
(1D):
Energy Switch (1D): Energy

Comment: 100 yr / 072 hr

Simulation: 100Y168H

Scenario: Scenario1
Run Date/Time: 11/18/2024 4:47:03 PM
Program Version: StormWise 4.08.01

General

Run Mode: Normal

	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	180.0000

	Hydrology [sec]	Surface Hydraulics [sec]
Min Calculation Time:	60.0000	0.1000
Max Calculation Time:		60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources	Lookup Tables
Rainfall Folder:	Boundary Stage Set:
Unit Hydrograph Folder:	Extern Hydrograph Set:
	Curve Number Set: 1
	Green-Ampt Set:
	Vertical Layers Set:
	Impervious Set: 1

Tolerances & Options	
Time Marching: SAOR	IA Recovery Time: 24.0000 hr
Max Iterations: 6	
Over-Relax Weight: 0.5 dec	Ia/S: 0.20 dec
Fact:	
dZ Tolerance: 0.0010 ft	
Max dZ: 1.0000 ft	Smp/Man Basin Rain: Global
	Opt:
Link Optimizer Tol: 0.0001 ft	
	Rainfall Name: ~FDOT-168
	Rainfall Amount: 20.30 in
	Storm Duration: 168.0000 hr
	Dflt Damping (1D): 0.0050 ft
	Min Node Srf Area: 100 ft2
	(1D):
	Energy Switch (1D): Energy

Comment: 100 yr / 168 hr

Simulation: 100Y240H				
Scenario:	Scenario1			
Run Date/Time:	11/18/2024 4:48:11 PM			
Program Version:	StormWise 4.08.01			

General				
Run Mode:	Normal			
	Year	Month	Day	Hour [hr]
Start Time:	0	0	0	0.0000
End Time:	0	0	0	252.0000
	Hydrology [sec]	Surface Hydraulics [sec]		
Min Calculation Time:	60.0000	0.1000		

Max Calculation Time: 60.0000

Output Time Increments

Hydrology

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Surface Hydraulics

Year	Month	Day	Hour [hr]	Time Increment [min]
0	0	0	0.0000	5.0000

Restart File

Save Restart: False

Resources & Lookup Tables

Resources

Rainfall Folder:

Unit Hydrograph
Folder:

Lookup Tables

Boundary Stage Set:

Extern Hydrograph Set:

Curve Number Set: 1

Green-Ampt Set:

Vertical Layers Set:

Impervious Set: 1

Tolerances & Options

Time Marching: SAOR

Max Iterations: 6

Over-Relax Weight 0.5 dec

Fact:

dZ Tolerance: 0.0010 ft

Max dZ: 1.0000 ft

Link Optimizer Tol: 0.0001 ft

IA Recovery Time: 24.0000 hr

Ia/S: 0.20 dec

Smp/Man Basin Rain Global
Opt:

Rainfall Name: ~FDOT-240

Rainfall Amount: 21.50 in

Storm Duration: 240.0000 hr

Dflt Damping (1D): 0.0050 ft

Min Node Srf Area 100 ft2

(1D):

Energy Switch (1D): Energy

Comment: 100 yr / 240 hr



NOAA Atlas 14, Volume 9, Version 2
Location name: Panama City Beach, Florida, USA*
Latitude: 30.2769°, Longitude: -85.9929°
Elevation: 8 ft**
 * source: ESRI Maps
 ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffrey Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerals](#)

Used in Ditch Hydraulic
Worksheet

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) ¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	6.42 (5.33-7.76)	7.46 (6.19-9.05)	9.13 (7.55-11.1)	10.5 (8.59-12.8)	12.2 (9.62-15.3)	13.5 (10.4-17.2)	14.8 (10.9-19.3)	16.0 (11.3-21.6)	17.6 (11.9-24.3)	18.7 (12.3-26.5)
10-min	4.70 (3.90-5.69)	5.47 (4.54-6.62)	6.68 (5.53-8.12)	7.66 (6.29-9.35)	8.95 (7.04-11.2)	9.91 (7.61-12.6)	10.8 (8.02-14.2)	11.7 (8.29-15.8)	12.9 (8.71-17.8)	13.7 (9.03-19.4)
15-min	3.82 (3.17-4.62)	4.44 (3.69-5.38)	5.43 (4.49-6.60)	6.23 (5.12-7.60)	7.28 (5.73-9.11)	8.06 (6.19-10.3)	8.80 (6.52-11.5)	9.53 (6.74-12.8)	10.5 (7.08-14.5)	11.1 (7.34-15.8)
30-min	2.87 (2.38-3.47)	3.35 (2.78-4.06)	4.12 (3.41-5.01)	4.74 (3.89-5.79)	5.55 (4.37-6.95)	6.15 (4.73-7.83)	6.73 (4.98-8.80)	7.29 (5.15-9.81)	7.99 (5.42-11.1)	8.50 (5.62-12.0)
60-min	2.01 (1.67-2.43)	2.30 (1.91-2.78)	2.78 (2.30-3.38)	3.18 (2.61-3.89)	3.74 (2.96-4.73)	4.18 (3.23-5.36)	4.63 (3.44-6.09)	5.08 (3.61-6.88)	5.70 (3.87-7.94)	6.16 (4.07-8.74)
2-hr	1.29 (1.08-1.55)	1.46 (1.22-1.76)	1.75 (1.45-2.11)	2.00 (1.65-2.42)	2.36 (1.88-2.97)	2.65 (2.06-3.38)	2.95 (2.21-3.86)	3.26 (2.33-4.40)	3.70 (2.54-5.14)	4.04 (2.69-5.69)
3-hr	0.990 (0.830-1.19)	1.11 (0.927-1.33)	1.32 (1.10-1.58)	1.50 (1.25-1.82)	1.79 (1.44-2.26)	2.02 (1.58-2.59)	2.28 (1.72-2.98)	2.55 (1.83-3.44)	2.93 (2.02-4.07)	3.24 (2.16-4.55)
6-hr	0.598 (0.504-0.711)	0.670 (0.564-0.797)	0.802 (0.673-0.958)	0.927 (0.773-1.11)	1.12 (0.911-1.41)	1.28 (1.02-1.64)	1.47 (1.11-1.92)	1.66 (1.21-2.24)	1.95 (1.35-2.70)	2.18 (1.46-3.04)
12-hr	0.338 (0.286-0.399)	0.388 (0.329-0.459)	0.480 (0.405-0.569)	0.565 (0.474-0.673)	0.696 (0.570-0.874)	0.808 (0.642-1.02)	0.930 (0.711-1.21)	1.06 (0.776-1.42)	1.25 (0.877-1.72)	1.41 (0.953-1.95)
24-hr	0.193 (0.164-0.226)	0.226 (0.192-0.265)	0.286 (0.243-0.337)	0.342 (0.288-0.404)	0.428 (0.352-0.534)	0.501 (0.400-0.631)	0.580 (0.446-0.750)	0.666 (0.489-0.886)	0.790 (0.556-1.08)	0.891 (0.606-1.23)
2-day	0.112 (0.096-0.130)	0.131 (0.112-0.153)	0.166 (0.142-0.194)	0.200 (0.169-0.235)	0.252 (0.209-0.313)	0.296 (0.239-0.372)	0.345 (0.267-0.444)	0.399 (0.295-0.528)	0.477 (0.338-0.648)	0.540 (0.370-0.739)
3-day	0.081 (0.070-0.094)	0.094 (0.081-0.109)	0.119 (0.102-0.139)	0.143 (0.122-0.167)	0.180 (0.150-0.224)	0.213 (0.172-0.267)	0.249 (0.194-0.319)	0.288 (0.214-0.380)	0.346 (0.246-0.469)	0.393 (0.270-0.536)
4-day	0.064 (0.056-0.074)	0.074 (0.064-0.086)	0.094 (0.080-0.109)	0.112 (0.096-0.131)	0.141 (0.118-0.175)	0.167 (0.135-0.209)	0.195 (0.152-0.250)	0.226 (0.169-0.298)	0.272 (0.194-0.368)	0.309 (0.213-0.420)
7-day	0.041 (0.036-0.048)	0.048 (0.041-0.055)	0.059 (0.051-0.069)	0.071 (0.061-0.082)	0.088 (0.074-0.109)	0.104 (0.084-0.129)	0.120 (0.094-0.153)	0.139 (0.104-0.182)	0.166 (0.119-0.223)	0.188 (0.130-0.254)
10-day	0.032 (0.028-0.037)	0.037 (0.032-0.042)	0.046 (0.039-0.053)	0.054 (0.046-0.062)	0.066 (0.056-0.081)	0.077 (0.063-0.095)	0.089 (0.070-0.113)	0.102 (0.077-0.133)	0.121 (0.087-0.162)	0.136 (0.095-0.184)
20-day	0.021 (0.019-0.024)	0.024 (0.021-0.028)	0.029 (0.026-0.034)	0.034 (0.029-0.039)	0.040 (0.034-0.049)	0.046 (0.038-0.056)	0.052 (0.041-0.065)	0.058 (0.044-0.075)	0.067 (0.048-0.089)	0.074 (0.052-0.099)
30-day	0.017 (0.015-0.020)	0.020 (0.017-0.022)	0.023 (0.020-0.027)	0.027 (0.023-0.031)	0.031 (0.026-0.037)	0.035 (0.029-0.042)	0.039 (0.031-0.048)	0.043 (0.032-0.055)	0.048 (0.035-0.064)	0.053 (0.037-0.070)
45-day	0.014 (0.012-0.016)	0.016 (0.014-0.018)	0.019 (0.017-0.022)	0.021 (0.019-0.024)	0.025 (0.021-0.029)	0.027 (0.022-0.033)	0.030 (0.023-0.036)	0.032 (0.024-0.041)	0.036 (0.026-0.046)	0.038 (0.027-0.050)
60-day	0.012 (0.011-0.014)	0.014 (0.012-0.016)	0.016 (0.014-0.019)	0.018 (0.016-0.021)	0.021 (0.018-0.025)	0.023 (0.019-0.027)	0.025 (0.020-0.030)	0.027 (0.020-0.033)	0.029 (0.021-0.037)	0.030 (0.021-0.040)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

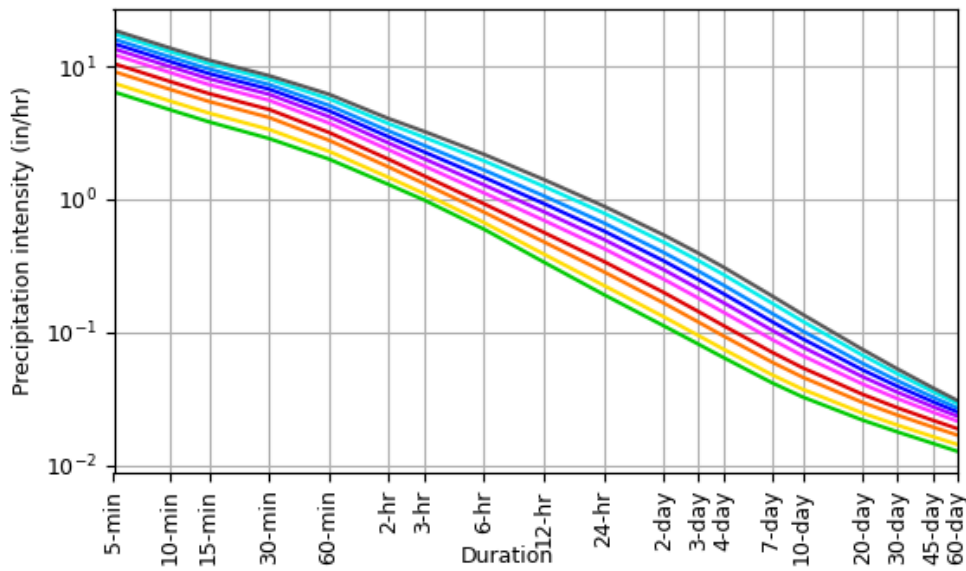
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PF graphical

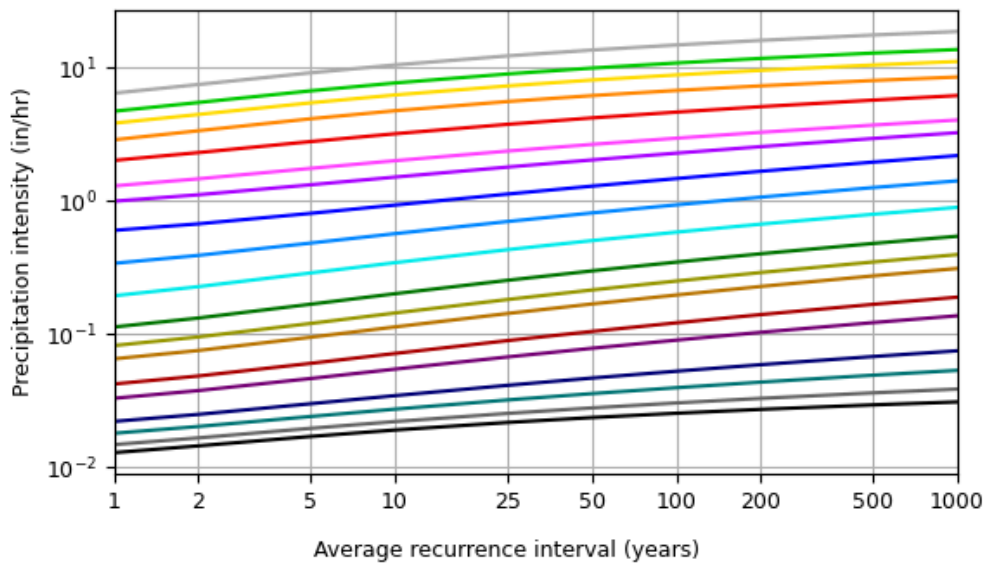
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PDS-based intensity-duration-frequency (IDF) curves

Latitude: 30.2769°, Longitude: -85.9929°



Average recurrence interval (years)
1
2
5
10
25
50
100
200
500
1000



Duration
5-min
10-min
15-min
30-min
60-min
2-hr
3-hr
6-hr
12-hr
24-hr
2-day
3-day
4-day
7-day
10-day
20-day
30-day
45-day
60-day

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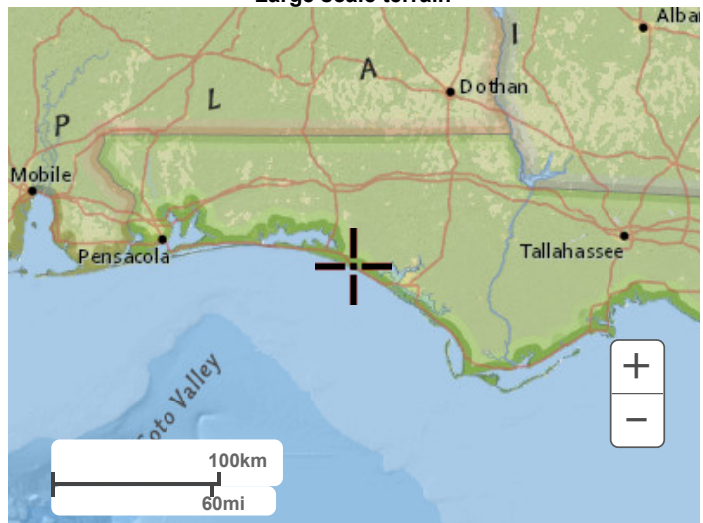
Maps & aerials

Small scale terrain

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Large scale terrain

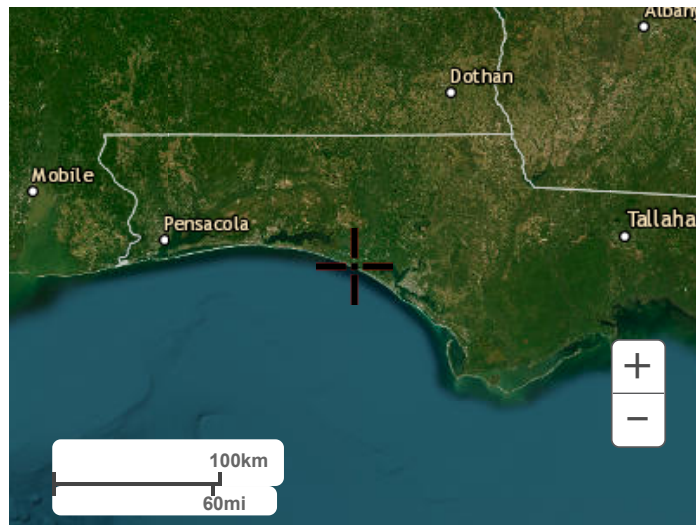


Large scale map



Large scale aerial

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NOAA Atlas 14, Volume 9, Version 2
Location name: Panama City Beach, Florida, USA*
Latitude: 30.2753°, Longitude: -85.9905°
Elevation: 12 ft**

* source: ESRI Maps

** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffrey Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

For StormWise Inputs

[PF tabular](#) | [PF graphical](#) | [Maps & aerals](#)

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.535 (0.444-0.647)	0.622 (0.516-0.754)	0.761 (0.629-0.925)	0.872 (0.716-1.06)	1.02 (0.802-1.28)	1.13 (0.867-1.44)	1.23 (0.912-1.61)	1.33 (0.944-1.80)	1.46 (0.992-2.03)	1.56 (1.03-2.21)
10-min	0.783 (0.650-0.948)	0.911 (0.756-1.10)	1.11 (0.921-1.35)	1.28 (1.05-1.56)	1.49 (1.17-1.87)	1.65 (1.27-2.10)	1.80 (1.34-2.36)	1.95 (1.38-2.63)	2.14 (1.45-2.97)	2.28 (1.50-3.23)
15-min	0.955 (0.793-1.16)	1.11 (0.922-1.35)	1.36 (1.12-1.65)	1.56 (1.28-1.90)	1.82 (1.43-2.28)	2.01 (1.55-2.56)	2.20 (1.63-2.88)	2.38 (1.68-3.21)	2.61 (1.77-3.62)	2.78 (1.84-3.94)
30-min	1.43 (1.19-1.74)	1.68 (1.39-2.03)	2.06 (1.70-2.51)	2.37 (1.95-2.89)	2.78 (2.18-3.48)	3.08 (2.36-3.92)	3.36 (2.49-4.40)	3.64 (2.58-4.90)	4.00 (2.71-5.54)	4.25 (2.82-6.00)
60-min	2.01 (1.67-2.43)	2.30 (1.91-2.78)	2.78 (2.30-3.38)	3.18 (2.61-3.89)	3.74 (2.96-4.73)	4.18 (3.23-5.36)	4.63 (3.44-6.09)	5.08 (3.61-6.88)	5.70 (3.87-7.94)	6.25 (4.07-8.74)
2-hr	2.58 (2.16-3.10)	2.92 (2.44-3.51)	3.50 (2.91-4.22)	4.00 (3.30-4.84)	4.71 (3.77-5.94)	5.29 (4.12-6.76)	5.89 (4.42-7.73)	6.52 (4.67-8.80)	7.39 (5.07-10.3)	8.08 (5.37-11.4)
3-hr	2.98 (2.49-3.56)	3.33 (2.79-3.99)	3.95 (3.30-4.75)	4.52 (3.75-5.46)	5.37 (4.32-6.77)	6.08 (4.76-7.77)	6.83 (5.15-8.96)	7.65 (5.51-10.3)	8.81 (6.07-12.2)	9.74 (6.50-13.7)
6-hr	3.58 (3.02-4.26)	4.01 (3.38-4.78)	4.81 (4.04-5.74)	5.55 (4.63-6.66)	6.71 (5.46-8.46)	7.70 (6.08-9.82)	8.78 (6.67-11.5)	9.96 (7.23-13.4)	11.7 (8.11-16.1)	13.0 (8.71-18.7)
12-hr	4.08 (3.46-4.81)	4.68 (3.96-5.53)	5.78 (4.88-6.86)	6.81 (5.72-8.11)	8.40 (6.87-10.5)	9.74 (7.74-12.4)	11.2 (8.57-14.6)	12.8 (9.36-17.1)	15.1 (10.6-20.8)	17.0 (11.5-23.5)
24-hr	4.63 (3.95-5.43)	5.42 (4.62-6.37)	6.87 (5.84-8.09)	8.22 (6.93-9.72)	10.3 (8.46-12.8)	12.0 (9.61-15.2)	13.9 (10.7-18.0)	16.0 (11.8-21.3)	19.0 (13.4-25.9)	21.4 (14.6-29.4)
2-day	5.40 (4.64-6.29)	6.31 (5.41-7.35)	8.00 (6.84-9.36)	9.61 (8.16-11.3)	12.1 (10.0-15.0)	14.2 (11.5-17.9)	16.6 (12.9-21.4)	19.2 (14.2-25.4)	22.9 (16.2-31.1)	26.0 (17.8-35.5)
3-day	5.87 (5.06-6.81)	6.82 (5.87-7.92)	8.61 (7.38-10.0)	10.3 (8.80-12.1)	13.0 (10.9-16.1)	15.4 (12.4-19.2)	17.9 (14.0-23.0)	20.8 (15.5-27.4)	24.9 (17.8-33.8)	28.3 (19.5-38.6)
4-day	6.22 (5.38-7.20)	7.19 (6.21-8.32)	9.04 (7.77-10.5)	10.8 (9.24-12.6)	13.6 (11.4-16.9)	16.1 (13.0-20.1)	18.8 (14.7-24.0)	21.8 (16.2-28.7)	26.1 (18.7-35.3)	29.7 (20.5-40.4)
7-day	7.05 (6.12-8.10)	8.10 (7.02-9.32)	10.1 (8.70-11.6)	12.0 (10.3-13.9)	14.9 (12.5-18.3)	17.5 (14.3-21.7)	20.3 (15.9-25.8)	23.4 (17.6-30.6)	28.0 (20.1-37.6)	31.7 (22.0-42.8)
10-day	7.86 (6.85-9.00)	8.99 (7.82-10.3)	11.1 (9.60-12.7)	13.0 (11.2-15.0)	16.1 (13.5-19.6)	18.7 (15.3-23.0)	21.5 (16.9-27.2)	24.6 (18.5-32.0)	29.1 (21.0-38.9)	32.8 (22.8-44.2)
20-day	10.5 (9.24-12.0)	11.9 (10.4-13.6)	14.3 (12.5-16.3)	16.5 (14.3-18.9)	19.7 (16.6-23.6)	22.3 (18.3-27.1)	25.1 (19.8-31.3)	28.1 (21.2-36.1)	32.4 (23.4-42.8)	35.8 (25.1-47.9)
30-day	12.9 (11.3-14.6)	14.5 (12.7-16.4)	17.2 (15.1-19.6)	19.6 (17.0-22.4)	22.9 (19.3-27.2)	25.6 (21.0-30.8)	28.4 (22.4-35.0)	31.3 (23.6-39.8)	35.2 (25.5-46.2)	38.3 (26.9-51.0)
45-day	15.9 (14.0-17.9)	17.9 (15.7-20.1)	21.0 (18.5-23.8)	23.7 (20.7-26.9)	27.2 (22.9-31.9)	30.0 (24.6-35.7)	32.7 (25.8-39.9)	35.4 (26.8-44.6)	38.9 (28.2-50.6)	41.5 (29.3-55.1)
60-day	18.4 (16.3-20.7)	20.7 (18.3-23.3)	24.4 (21.5-27.5)	27.3 (23.9-30.9)	31.1 (26.1-36.1)	33.8 (27.8-40.0)	36.4 (28.9-44.3)	39.0 (29.5-48.8)	42.1 (30.6-54.4)	44.3 (31.4-58.6)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

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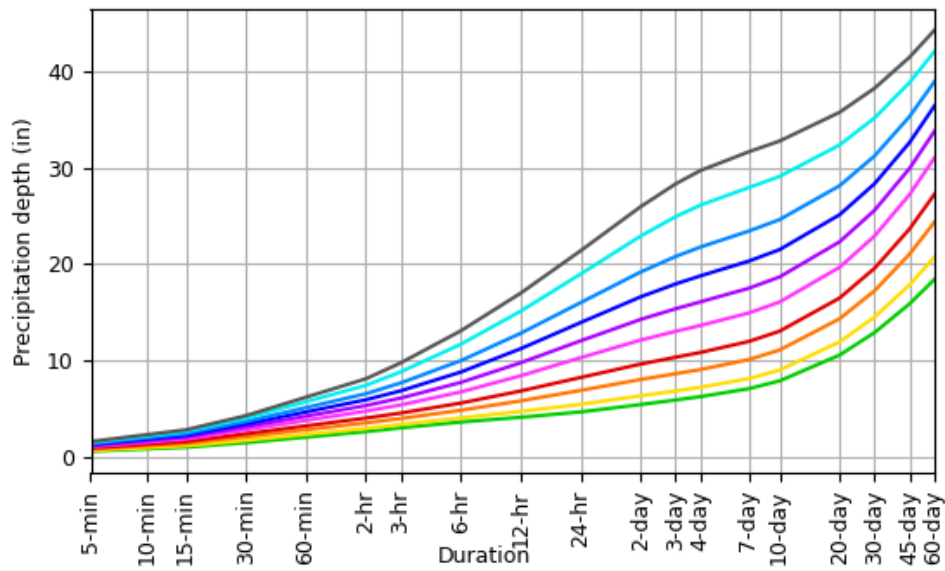
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PF graphical

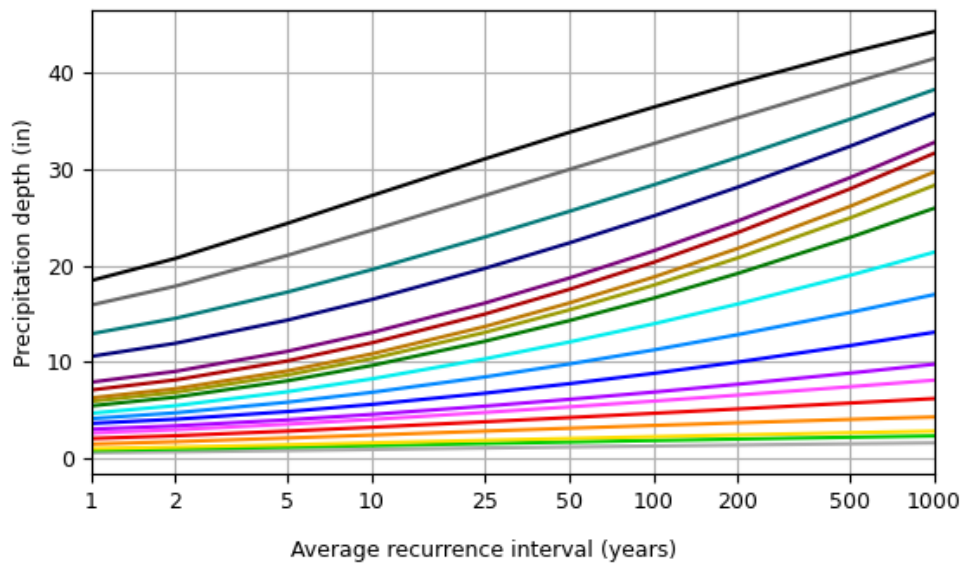
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PDS-based depth-duration-frequency (DDF) curves

Latitude: 30.2753°, Longitude: -85.9905°

Average recurrence
interval
(years)

1
2
5
10
25
50
100
200
500
1000



Duration

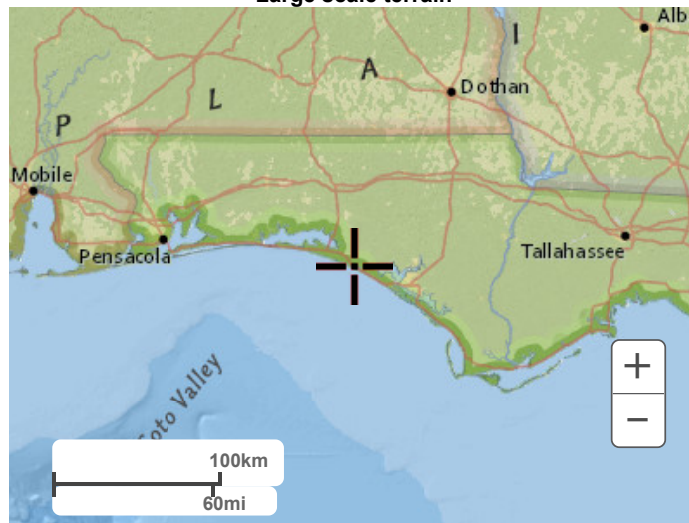
5-min 2-day
10-min 3-day
15-min 4-day
30-min 7-day
60-min 10-day
2-hr 20-day
3-hr 30-day
6-hr 45-day
12-hr 60-day
24-hr

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Large scale terrain



Large scale map



Large scale aerial

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